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SST 65-15 VOLUME 2

STRUCTURAL REACTION PROGRAM
NATIONAL SONIC BOOM STUDY PROJECT

APRIL 1965

SUPERSONIC TRANSPORT DEVELOPMENT
FEDERAL AVIATION AGENCY
WASHINGTON, D. C.

Prepared Under Contract FA-SS-65-12 by John A. Blume &
Associates Research Division, San Francisco, California.

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APPENDICES

Report on the National Sonic Boom Study

Structural Reaction Program

APRIL 1965

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Contract FA-SS-65-12

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I. Bibliography

Reference No.	
1	Soroka, W.W., SONIC BOOM PROBLEMS AND NOISE FROM HIGH PERFORMANCE PROPULSION SYSTEMS, Society of Automotive Engineers, National West Coast Meeting, Seattle, Washington, Paper 723 D (August 19-22, 1963).
2	Falco, M., SUPERSONIC TRANSPORT CLIMB PATH OPTIMIZATION INCLUDING A CONSTRAINT ON SONIC BOOM INTENSITY, AIAA Journal, Vol. 1 (December 1963).
3	Bird, G.A. and Wetherall, C.J., LIFT CONTRIBUTION TO THE SONIC BOOM, AIAA Journal, Vol. 2 (March 1964).
4	Sigalla, A., LIFT PRODUCED BY A SONIC BOOM, Journal, Royal Aeronautical Society, Vol. 67 (December 1963).
5	Randall, D.C., THE EFFECT OF INCIDENCE ON SONIC BAND INTFNSITIES, Tech. Note Structures 332, Royal Aircraft Establishment (Farnborough). Ministry of Aviation, London, W.C. 2 (April 1963).
6	Lansing,D.L., APPLICATION OF ACOUSTIC THEORY TO PREDICTION OF SONIC-BOOM GROUND PATTERNS FROM MANEUVERING AIRCRAFT, NASA TN D-1864 (October 1964).
7	Wilde, M.G., NOISE, in International Federation of Air Line Pilots Association (CFALPA), Symposium on Supersonic Transport, IFALPA, Vol. 2, London, England (November 12-14, 1963).
8	Guiraud, J.P., REMARQUES SUR LE BRUIT BALISTIQUE AU VOISINAGE D'UNE CAUSTIQUE (REMARKS ON THE SUPERSONIC BOOM IN THE NEIGHBORHOOD OF A CAUSTIC), La Recherche Aerospatiole (in French) (January-February 1964).

Appendix A

I. Bibliography (continued)

Reference No.	
9	Power, J.K., and Bates, G., SONIC BOOM AND COMMUNITY RELATIONS, Federal Aviation Agency, Washington, D.C. (prepared for National Aero-Nautical Meeting, Washington, D.C.) (April 8-11,1963).
10	Lienard, P., ETUDES DES DETONATIONS SUPERSONIQUES (STUDIES ON SUPERSONIC DETONATIONS). Congres International pour la Lutte contre le Bruit, 3rd, Paris, France (May 13-15, 1964).
11	Broadbent, G.E., and Robinson, D.W., SUBJECTIVE MEASUREMENTS OF THE RELATIVE ANNOYANCE OF SIMULATED SONIC BANGS AND AIRCRAFT NOISES, Journal of Sound and Vibration, Vol. 1 (April 1964).
12	Wilson, Jr., H.A., SONIC BOOM, Scientific American, Vol. 206, No. 1 (January 1962).
13	Lyster, H.N.C., THE NATURE OF THE SONIC BOOM, Materials Research and Standards, Vol. 4, No. 11 (November 1964).
14	Warren, C.H.E., THE PROPAGATION OF SONIC BANGS IN A HOMOGENEOUS STILL ATMOSPHERE, International Council of the Aeronautical Sciences, Congress, 4th, Paper 64-547, Paris, France (August 24-28, 1964).
15	Dressler, R., and Frecholm, N., ATMOSPHERIC SCATTERING OF SONIC-BOOM INTENSITIES, International Council of the Aeronautical Sciences, Congress, 4th, Paper 64-538, Paris, France (August 24-28, 1964).
16	Dressler, R.F., SONIC-BOOM WAVES IN STRONG WINDS, Aeronautical Research Institute of Sweden (October 1963).
17	Warren, C.H.E., THE EFFECT OF METEOROLOGICAL VARIATIONS ON THE STATISTICAL SPREAD IN THE INTENSITY OF BANGS AT LARGE DISTANCES FROM THE SOURCE, Royal Aircraft Establishment (Farnborough), Technical Note No. Structures 334, Ministry of Aviation, London, W.C. 2 (May 1963).

I. Bibliography (continued)

Reference No.	
18	Perkins, Jr., B., Lorrain, Pilt, and Townsend, W.H., FORECASTING THE FOCUS OF AIR BLASTS DUE TO METEOROLOGICAL CONDITIONS IN THE LOWER ATMOSPHERE, Report No. 1118, Ballistic Research Laboratories, Aberdeen Proving Ground, Maryland (October 1960).
19	Wilton, C., Wallace, N.R., and Kaplan, K., STUDY OF CHANNELING OF AIR BLAST WAVES, prepared for Defense Atomic Support Agency by United Research Services, Burlingame, Calif. (June 26, 1963).
20	U.S. Navy Department, HANDBOOK OF SUPERSONIC AERODYNAMICS, Vol. 6, Washington, D.C. (1959).
21	Ridenour, L.M., MODERN PHYSICS FOR THE ENGINEER, McGraw-Hill Book Co., Inc., New York, N.Y. (1954).
22	Department of the Army, THE EFFECTS OF NUCLEAR WEAPONS, Department of the Army Pamphlet No. 39-3 (May 1957).
23	Kornhauser, M., STRUCTURAL EFFECTS OF IMPACT, Spartan Books, Inc., Baltimore, Maryland (1964).
24	UNITED STATES CENSUS OF HOUSING 1960; United States Summary, States and Small Areas, U.S. Dept. of Commerce, Bureau of Census, HC(1) No. 1, Summary, Washington, D.C. (1963).
25	NEW HOUSING AND ITS MATERIALS, 1940-56, U.S. Dept. of Labor, Bureau of Labor Statistics, Washington, D.C. (August 1953).
26	LABOR AND MATERIAL REQUIREMENTS FOR PRIVATE ONE-FAMILY HOUSE CONSTRUCTION, Bulletin No. 1404, U.S. Dept. of Labor Statistics, Washington, D.C. (June 1964).
27	Whittenmore, H.L., Cotter, J.B., Stang, A.H. and Rhelan, V.B., STRENGTH OF HOUSES; APPLICATION OF ENGINEERING PRINCIPLES TO STRUCTURAL DESIGN, U.S. Dept. of Commerce, National Bureau of Standards, B.M.S. Report B.M.S. 109, Washington, D.C. (April 1, 1948).

I. Bibliography (continued)

Reference No.	
28	Wiggins, J.H., EFFECT OF SITE CONDITIONS ON EARTHQUAKE INTENSITY, ASCE Structural Division Journal (April 1964).
29	Brekke, G.N., WIND PRESSURES IN VARIOUS AREAS OF THE UNITED STATES, BMS Report 152, National Bureau of Standards, Washington, D.C. (April 24, 1959).
30	Thom, H.C.S., DISTRIBUTION OF EXTREME WINDS IN THE UNITED STATES, Journ. Struct. Division, ASCE (April 1960).
31	AMERICAN STANDARD BUILDING CODE REQUIREMENTS FOR MINIMUM DESIGN LOADS IN BUILDINGS AND OTHER STRUCTURES, American Standards Association (September 30, 1955).
32	DESIGN MANUAL - STRUCTURAL ENGINEERING, Nav docks DM-2, Dept. of the Navy, Bureau of Yards and Docks, Washington 25, D.C. (February 12, 1962).
33	DWELLING HOUSE CONSTRUCTION UNDER THE UNIFORM BUILDING CODE (1958 Edition).

II. General Sources

a. Indexes and Abstracts

INTERNATIONAL AEROSPACE ABSTRACTS,
Technical Information Service, American Institute of Aeronautics and Astronautics, Inc., 750 Third Ave., New York, N.Y. (10017).

SCIENTIFIC AND TECHNICAL AEROSPACE REPORTS,
National Aeronautics and Space Administration, Washington, D.C.

INDEXES OF NACA TECHNICAL PUBLICATIONS,
National Advisory Committee for Aeronautics (Series from 1915 to June 1960), Washington, D.C.

SCIENCE ABSTRACTS,
Section A. Physics Abstracts, The Institution of Electrical Engineers, Savoy Place, London, W.C. 2, England.

RESEARCH SUMMARY,
Annual Series, Institute of Engineering Research, University of California, Berkeley.

THE ENGINEERING INDEX,
Engineering Index Inc., New York, N.Y. (Annual,

TECHNICAL ABSTRACT BULLETIN INDEXES,
Defense Documentation Center, Defense Supply Agency, Cameron Station, Alexandria, Va. (22314).

TECHNICAL ABSTRACT BULLETIN,
Defense Documentation Center, Defense Supply Agency, Cameron Station, Alexandria, Va. (22314).

INDUSTRIAL ARTS INDEX
The H. W. Wilson Company, New York, N.Y.

THE CUMULATIVE BOOK INDEX,
The H. W. Wilson Company, New York, N.Y.

GEOPHYSICAL ABSTRACTS,
U.S. Geological Survey, Washington, D.C.

II. General Sources (continued)

a. Indexes and Abstracts (continued)

53-YEAR INDEX OF THE BULLETIN OF THE SEISMOLOGICAL SOCIETY OF AMERICA, Baltimore 2, Maryland (October 1964).

RUSSIAN TECHNICAL LITERATURE,
European Productivity Agency, O.E.E.C., 3 Rue Andre-Pascal, Paris (Monthly).

UNCLASSIFIED LIST OF REPORTS,
David Taylor Model Basin, U.S. Navy Department, Washington, D.C.

CUMULATIVE INDEX TO ASCE PUBLICATIONS,
American Society of Civil Engineers; Proceedings, 1950-1959 (Vols. 76-85); Transactions, 1935-1959 (Vols. 100-124); Civil Engineering, 1930-1959 (Vols. 1-29); New York, N.Y. (1961).

APPLIED SCIENCE & TECHNOLOGY INDEX,
The H. W. Wilson Company, 950 University Ave., Bronx, N.Y., (10452) (1958 to date).

GUIDE TO THE SUBJECT INDEXES for Scientific and Technical Aerospace Reports, NASA, Issue No. 1, Washington, D.C. (April 1964).

CUMULATED INDEX, U.S. Government Research Reports, U.S. Dept. of Commerce Office of Technical Services, Washington, D.C.

METEOROLOGICAL & GEOASTROPHYSICAL ABSTRACTS,
American Meteorological Society, 45 Beacon Street, Boston 8, Mass.

SURVEYS OF SOVIET - BLOC SCIENTIFIC LITERATURE,
Compilation of Abstracts, Library of Congress, Aerospace Technology Division, Washington, D.C.

II. General Sources (continued)

b. Reports, Papers, Memorandums, Articles

Shock Phenomena and Related Material

Van Hulsteyn, D.B., THE ATMOSPHERIC PRESSURE WAVE GENERATED BY A NUCLEAR EXPLOSION, Journ. of Geophysical Research, Vol. 70, No. 2, Parts 1 and 2 (January 15, 1965).

Warren, C.M.E., A CORRECTION TO THE THEORY OF SONIC BANGS, Progress in Aeronautical Sciences, Vol. 5, The MacMillan Co., New York (1965).

Pack, D.C., THE REFLECTION AND DIFFRACTION OF SHOCK WAVES, Journ. of Fluid Mechanics, Vol. 18, Part 4 (1964).

SONIC BOOMS RATTLE GHOST TOWN, Engineering News-Record (December 10, 1964).

Mayes, W.H., and Edge, Jr., P.M., EFFECTS OF SONIC BOOM AND OTHER SHOCK WAVES ON BUILDINGS, Materials Research & Standards, Vol. 4, No. 11 (November 1964).

Power, J.K., SOME RESULTS OF THE OKLAHOMA CITY SONIC BOOM TESTS, Materials Research & Standards, Vol. 4, No. 11 (November 1964).

Huntoon, J., METEOROLOGICAL REQUIREMENTS FOR THE SUPERSONIC TRANSPORT, International Federation of Air Line Pilots Associations (IFALPA), Symposium on Supersonic Transport, London, Nov. 12-13, 1964 IFALPA, Vol. 2 (1964).

Wilde, M.G., NOISE, International Federation of Air Line Pilots Associations (IFALPA), Symposium on Supersonic Transport, London, Nov. 12-13, 1964 IFALPA, Vol. 2 (1964).

Lyster, H.N.C., THE NATURE OF THE SONIC BOOM, Materials Research & Standards, Vol. 4, No. 11 (November 1964).

Lansing, D.L., APPLICATION OF ACOUSTIC THEORY TO PREDICTION OF SONIC-BOOM GROUND PATTERNS FROM MANEUVERING AIRCRAFT, NASA Tech Note TN D-1860 (October 1964).

THE SONIC BOOM COMES HOME, Astronautics & Aeronautics, Vol. 2 (September 1964).

II. General Sources (continued)

b. Reports, Papers, Memorandums, Articles (continued)

Lundberg, B.K.O., PROS AND CONS OF SUPERSONIC AVIATION IN RELATION TO GAINS OR LOSSES IN COMBINED TIME/COMFORT CONSIDERATIONS, Royal Aeronautical Society Journal, Vol. 68 (September 1964).

Halaby, N.E. and Bain, G.M., THE SUPERSONIC TRANSPORT, Data Magazine, Vol. 9, No. 9 (September 1964).

Halaby, N.E., SST-THE RACE FOR SAFETY, Astronautics & Aeronautics, Vol. 2, No. 9 (September 1964).

Kane, E.J., and Palmer, T.Y., METEOROGICAL ASPECTS OF THE SONIC BOOM, Federal Aviation Agency, Washington, D.C. (September 1964).

SONIC BOOM BIBLIOGRAPHY, Federal Aviation Agency, Washington, D.C. (September 1964).

Chang, T.S., and Laport, O., REFLECTION OF STRONG BLAST WAVES, Physics of Fluids, Vol. 7, No. 8 (August 1964).

Oswatitsch, K., DER STOSSWELLENKNALL BEIM UBERSCHALLFLUG (SONIC BOOM IN SUPERSONIC FLIGHT), International Council of the Aeronautical Sciences, Congress 4th, Paper 64-546, Paris, France (August 24-28, 1964).

Warren, C.H.E., THE PROPAGATION OF SONIC BANGS IN A NONHOMOGENEOUS STILL ATMOSPHERE, International Council of the Aeronautical Sciences, Congress, 4th Paper 64-547, Paris, France (August 24-28, 1964).

Dressler, R., and Fredholm, N., ATMOSPHERIC SCATTERING OF SONIC-BOOM INTENSITIES, International Council of the Aeronautical Sciences, Congress, 4th, Paris, France (August 24-28, 1964).

SONIC BOOM EFFECTS ON LIGHT AIRCRAFT, HELICOPTERS AND GROUND STRUCTURES, Federal Aviation Agency, Washington, D.C. (prepared for meeting of American Society for Testing and Materials, Chicago, Illinois, June 25, 1964).

Lienard, P., ETUDES DES DETONATIONS SUPERSONIQUES (STUDIES ON SUPERSONIC DETONATIONS), Congres International pour la Lutte Contre le Bruit, 3rd, Paris, France (May 13-15, 1964).

II. General Sources (continued)

b. Reports, Papers, Memorandums, Articles (continued)

THE SUPERSONIC HOT SEAT, Look (May 5, 1964).

SONIC BOOM INFORMATION FOR THE PRESIDENT'S ADVISORY COMMITTEE ON SUPERSONIC TRANSPORT, Federal Aviation Agency, Washington, D.C. (April 27, 1964).

Broadbent, D.E., and Robinson, D.W., SUBJECTIVE MEASUREMENTS OF THE RELATIVE ANNOYANCE OF SIMULATED SONIC BANGS AND AIRCRAFT NOISE, Journal of Sound and Vibration, Vol. 1 (April 1964).

Warren, C.H.E., A NOTE ON THE REFRACTION OF SOUND IN A MOVING GAS, Journal of Sound and Vibration, Vol. 1 (April 1964).

THE SUPERSONIC TRANSPORT, Space and Aeronautics, Vol. 41 (April 1964).

Carlson, H.W., INFLUENCE OF AIRPLANE CONFIGURATION ON SONIC BOOM CHARACTERISTICS, Journ. of Aircraft, Vol. 1, No. 2 (March-April 1964).

Bird, G.A., and Wetherall, C.J., LIFT CONTRIBUTION TO THE SONIC BOOM, AIAA Journal, Vol. 2 (March 1964).

Bird, G.A., THE BEHAVIOR OF SHOCK WAVES IN A GRAVITATIONAL ATMOSPHERE, The Astrophysical Journal, Vol. 139, No. 2 (February 15, 1964).

Edwards, E., PROGRESS WITH THE CONCORD SUPERSONIC TRANSPORT, Institute of Transport Brancker Memorial Lecture, 21st, London, England (February 10, 1964).

Perkins, B. Jr., and Jackson, W.F., HANDBOOK FOR PREDICTION OF AIR BLAST FOCUSSING, Ballistic Research Laboratory, Rept. 1240, Aberdeen Proving Ground, Maryland (February 1964).

Barger, R.L., SOME EFFECTS OF FLIGHT PATH AND ATMOSPHERIC VARIATIONS ON THE BOOM PROPAGATED FROM A SUPERSONIC AIRCRAFT, NASA, TRR-191 (February 1964).

Hannifin, J., and Murphy, C.J.V., WE'RE LOSING THE SUPERSONIC TRANSPORT RACE, Fortune (February 1964).

II. General Sources (continued)

b. Reports, Papers, Memorandums, Articles (continued)

Holtje, G., SOME THOUGHTS ABOUT THE DEVELOPMENT AND ECONOMICAL PROBLEMS OF SUPERSONIC TRANSPORTS, Esso Air World, Vol. 16 (January-February 1964).

Guiraud, J.P., REMARQUES SUR LE BRUIT BALISTIQUE AU VOISINAGE D'UNE CAUSTIQUE (REMARKS ON THE SUPERSONIC BOOM IN THE NEIGHBORHOOD OF A CAUSTIC), La Recherche Aerospatiale (January-February 1964).

Sigalla, A., LIFT PRODUCED BY A SONIC BOOM, Royal Aeronautical Society, Journal, Vol. 67 (December 1963).

Falco, M., SUPERSONIC TRANSPORT CLIMB PATH OPTIMIZATION INCLUDING A CONSTRAINT ON SONIC BOOM INTENSITY, AIAA Journal, Vol. 1 (December 1963).

Hutchinson, H.A., DEFINING THE SONIC BOOM PROBLEM, USAF, Wright-Patterson AFB, Vol. 1, Astronautics and Aerospace Engineering (December 1963).

LIST OF METEOROLOGICAL RESEARCH PAPERS (M.R.P.'S) OF THE BRITISH AIR MINISTRY METEOROLOGICAL RESEARCH COMMITTEE 1942-1958, RELEASED TO U.S. DEFENSE ACTIVITIES, Air Weather Service Pamphlet AWSP 0-1, U.S. Air Force (November 1, 1963).

Carlson, H.W., THE INFLUENCE OF AIRPLANE CONFIGURATION ON SONIC-BOOM CHARACTERISTICS, Proc. AIAA (Meeting at Dayton, Ohio, Nov. 4-6, 1963).

Dressler, R.F., SONIC-BOOM WAVES IN STRONG WINDS, Aeronautical Research Institute of Sweden, Stockholm (October 1963).

Maglieri, D.J., Parrott, T.L., Hilton, D.A., and Copeland, W.L., LATERAL SPREAD SONIC-BOOM GROUND-PRESSURE MEASUREMENTS FROM AIRPLANES AT ALTITUDES TO 75,000 FEET AND AT MACH NUMBERS TO 2.0, NASA, TN D-2021, Washington, D.C. (November 1963).

Polhemus, W.L., QUELQUES PROBLEMES DE NAVIGATION RELATIFS A L'AVION DE TRANSPORT SUPERSONIQUE (SOME NAVIGATION PROBLEMS OF SUPERSONIC TRANSPORT AIRCRAFT), Deutsche Gessellschaft fur Ortung und Navigation, International Congress, Berlin (April 24, 1963), Inst. Navg. Jour., Paris, Vol. 16 (Oct. 1963).

II. General Sources (continued)

b. Reports, Papers, Memorandums, Articles (continued)

Miles, J.W., NOTES ON THE DIFFRACTION OF BLASTS BY FLYING VEHICLES, Commander Space Systems Division, U.S. Air Force, Inglewood, California (26 August 1963).

Sovoka, W.W., SONIC BOOM PROBLEMS AND NOISE FROM HIGH PERFORMANCE PROPULSION SYSTEMS, University of California, Berkeley, Paper 723 D, Soc. of Automotive Engineers, National West Coast Meeting, Seattle, Washington (August 19-22, 1963).

Shepherd, E.C., THE BOOM OF SUPERSONIC AIR LINERS AND THE FREEDOM OF THE AIR, New Scientist, Vol. 19, No. 352 (August 15, 1963).

DEVELOPMENT OF EXPECTED NOISE SPECTRA, SIREN PROGRAMMING TECHNIQUES, AND EXPERIMENT PLANS FOR THE ASD SONIC FATIGUE FACILITY, Tech. Doc. Rept. No. ASD-TDR-63-674, Wright-Patterson AFB, Ohio (August 1963).

Maglieri, D.J., and Morris, G.J., MEASUREMENTS OF THE RESPONSE OF TWO LIGHT AIRPLANES TO SONIC BOOMS, NACA TN D-1941 (August 1963).

Wilton, C., Wallace, N.R., and Kaplan, K., STUDY OF CHANNELING OF AIR BLAST WAVES, prepared for Defense Atomic Support Agency by United Research Services, Burlingame, California (June 26, 1963).

Hutchinson, H.A., FURTHER DEFINITION OF THE SONIC BOOM PROBLEM AND ITS INFLUENCE ON SUPERSONIC TRANSPORT DESIGN, PROPULSION AND PERFORMANCE REQUIREMENTS, AIAA Summer Meeting, Los Angeles, Calif. (June 17-20, 1963).

Bradley, N.N., SHOCK WAVES AND HIGH TEMPERATURE CHEMISTRY, New Scientist, Vol. 18, No. 343, London, England (June 1963).

Friedman, M.P., Kane, E.J., and Sigalla, A., EFFECTS OF ATMOSPHERE AND AIRCRAFT MOTION ON THE LOCATION AND INTENSITY OF A SONIC BOOM, ACAA Journal, Vol. 1, No.6 (June 1963).

Tedrick, R.N., and Polly, R.C., A PRELIMINARY INVESTIGATION OF THE MEASURED ATMOSPHERIC EFFECTS UPON SOUND PROPAGATION, SASA, MTP-Test-63-6 (May 24, 1963).

II. General Sources (continued)

b. Reports, Papers, Memorandums, Articles (continued)

Warren, C.H.E., THE EFFECT OF METEOROLOGICAL VARIATIONS ON THE STATISTICAL SPREAD IN THE INTENSITY OF BANGS AT LARGE DISTANCES FROM THE SOURCE, Royal Aircraft Establishment, Tech. Note No. 334 (Structures), Farnborough, England (May 1963).

Randall, D.G., THE EFFECT OF INCIDENCE ON SONIC BANG INTENSITIES, Royal Aircraft Establishment, Tech. Note No. 332 (Structures), Farnborough, England (April 1963).

Power, J.K., and Bates, G., SONIC BOOM & COMMUNITY RELATIONS, Federal Aviation Agency, Washington, D.C. (prepared for National Aero-Nautical Meeting, Washington, D.C., April 8-11, 1963).

Tymczyszyn, J.J., and Spiess, P.C., THE EFFECTS OF SUPERSONIC FLIGHT CHARACTERISTICS ON PERFORMANCE REQUIREMENTS, Society of Automotive Engineers - American Society of Naval Engineers, Aero-Nautical Meeting, Washington, D.C. (April 8-11, 1963).

Cox, E.F., ATOMIC BOMB BLAST WAVES, Scientific American, Vol. 188, No. 4 (April 1963).

Maglieri, D.J., and Lansing, D.L., SONIC BOOMS FROM AIRCRAFT IN MANEUVERS, Sound, Vol. 2, No. 2 (March-April 1963).

TABLES FOR CALCULATION OF REYNOLDS NUMBER AS A FUNCTION OF MACH NUMBER, STAGNATION PRESSURE, AND STAGNATION TEMPERATURE, Rept. No. RF-TR-63-3, U.S. Army Missile Command, Redstone Arsenal, Alabama (February 18, 1963).

Guiraud, J.P., SUR LA VALEUR DE L'INTENSITE, AU VOISINAGE D'UNE CAUSTIQUE, DU BRUIT BALISTIQUE PRODUIT PAR LE VOL SUPERSONIQUE (ON THE INTENSITY VALUE OF A SONIC BOOM IN THE NEIGHBORHOOD OF A CAUSTIC), Academie des Sciences (Paris), Comptes Rendus, Vol. 256, No. 8 (February 18, 1963).

Warren, C.H.E., and Webb, D.R.B., AN EXPLORATORY INVESTIGATION OF THE EFFECTS OF BANGS ON THE SUBJECTIVE REACTION OF A COMMUNITY, Royal Aircraft Establishment, Farnborough, Tech. Note 324 (Structures), Ministry of Aviation, London (January 1963).

II. General Sources (continued)

b. Reports, Papers, Memorandums, Articles (continued)

Von Rues, D., and Bottger, P., EINE NAHERUNGSLOSNG FUR MACHREFLEXIONEIN, Zeitschrift Fur Angewante Math. und Mech., Vol. 43 (1963).

Andryankin, E.I., Koga, A.M., Kompanects, A.S., and Krainov, V.P., PROPAGATION OF STRONG EXPLOSION IN NON-HOMOGENEOUS ATMOSPHERE (Russian), Trans. by Wright-Patterson AFB, Ohio (1963).

Ioan, C.S., IN 1973 YOU WILL TRAVEL AT 2330 KM/HOUR (Rumania), Trans. by Wright-Patterson AFB, Ohio (1963).

Shepherd, E.C., EVOLUTION OF THE CONCORD SUPERSONIC AIR-LINER, New Scientist, Vol. 16, No. 316, London, England (December 6, 1962).

Guiraud, J.P., STRUCTURE ASYMOTIQUE DES ONDES SONORES NON LINEAIRES EMISES PAR UN AVION SUPERSONIQUE ET THEORIE DU BRUIT BALISTIQUE (THE ASYPTOTIC STRUCTURE OF NONLINEAR SOUND WAVES PRODUCED BY SUPERSONIC AIRCRAFT, AND THE BALLISTIC NOISE THEORY), International Council of the Aeronautical Sciences, International Congress, 3rd, Stockholm, Sweden (August 27-31, 1962).

Nowak, M.J., SOME FUNDAMENTAL PROPERTIES OF SHOCK WAVES, Air Force Special Weapons Center, U.S. Atomic Energy Commission (May 1962).

Maglieri, D.J., and Parrott, T.L., ATMOSPHERIC EFFECTS ON SONIC BOOM SIGNATURES, Paper presented to 63rd Meeting of Acoustical Society of America, New York (May 1962).

Wilson, Jr. H.A., SONIC BOOM, Scientific American, Vol. 26, No. 1 (January 1962).

Reed, J.W., MICROBAROGRAPH MEASUREMENTS OF B-58 SONIC BOOMS, Project Big Boom, Sandia Corporation (December 1961).

Hamilton, J., FREE-FLIGHT MODELS IN AERODYNAMIC RESEARCH, New Scientist, No. 262, London, England (November 23, 1961).

II. General Sources (continued)

b. Reports, Papers, Memorandums, Articles (continued)

Shepherd, E.C., SUPERSONIC AIRLINERS: SOME OF THE PROBLEMS, New Scientist, Vol. 12, No. 261, London, England (November 16, 1961).

Strahle, W.C., THE COMPUTATION OF OBLIQUE SHOCK WAVE CHARACTERISTICS FOR REAL CASES, The Rand Corporation, Santa Monica, California (August 1961).

Maglieri, D.J., and Hubbard, H.H., GROUND MEASUREMENTS OF THE SHOCK-WAVE NOISE FROM SUPERSONIC BOMBER AIRPLANES IN THE ALTITUDE RANGE FROM 30,000 TO 50,000 FEET NASA TN-880 (July 1961).

McChesney, M., THE SHOCK TUBE'S MANY USES, New Scientist, Vol. 10, No. 239, London, England (June 15, 1961).

Lansing, D.L., SOME EFFECTS OF FLIGHT MANEUVERS ON THE DISTRIBUTION OF SONIC BOOMS, Paper presented to Symposium on Atmospheric Acoustic Propagation, El Paso, Texas (June 1961).

SOME CONSIDERATIONS OF SONIC BOOM, Federal Aviation Agency, Washington, D.C. (May 1961).

Lundberg, B., SHOULD SUPERSON[illegible]IRLINERS BE PERMITTED, New Scientist, Vol. 9, No. 2[illegible], London, England (February 31, 1961).

Dosanjh, D.S., INTERACTION OF TRAVELING SHOCK WAVE WITH TURBULENT FLOW FIELDS, Office of Ordnance Research (July 1959 and January 1961).

Perkins, Jr., B., Lorrain, P.H., Townsend, W.H., FORECASTING THE FOCUS OF AIR BLASTS DUE TO METEOROLOGICAL CONDITIONS IN THE LOWER ATMOSPHERE, Rept. No. 1118, Ballistic Research Laboratories, Aberdeen Proving Ground, Maryland (October 1960).

Lighthill, M.J., HIGHER APPROXIMATIONS IN AERODYNAMIC THEORY, Princeton Aeronautical Paperbacks No. 5, Princeton University Press, New Jersey (1960).

Jones, R.T., and Cohen, D., HIGH SPEED WING THEORY, Princeton Aeronautical Paperbacks No. 6, Princeton University Press, New Jersey (1960).

II. General Sources (continued)

b. Reports, Papers, Memorandums, Articles (continued)

Anderson, Jr., F.E., BLAST PHENOMENA FROM A NUCLEAR BURST, Trans., ASCE, Vol. 125, Pt. 1 (1960).

Warren, C.M.E., and Randall, D.G., THE THEORY OF SONIC BANGS, Progress in Aeronautical Sciences, Vol. 1, The MacMillan Co., New York (1960).

Magileri, D.J., Hubbard, H.H., and Lansing, D.L., GROUND MEASUREMENTS OF THE SHOCK-WAVE NOISE FROM AIRPLANES IN LEVEL FLIGHT AT MACH NUMBERS TO 1, 4 AND AT ALTITUDES TO 45,000 FEET, NASA, TN D-48, Langley Research Center, Va. (September 1959).

Stanykovich, K.P., and Golitsyn, G.S., SHOCK WAVES, Translation from Russian, Technical Library, Air Force Ballistic Missile Division (May 21, 1959).

Randall, D.G., METHODS FOR ESTIMATING DISTRIBUTIONS AND INTENSITIES OF SONIC BANGS, R&M No. 3133, British A.R.C. (1959).

Walkden, F., THE SHOCK PATTERN OF A WING-BODY COMBINATION, FAR FROM THE FLIGHT PATH, Aero. Quart., Vol. 9, Part 2 (May 1958).

Whitham, G.B., A NEW APPROACH TO THE PROBLEMS OF SHOCK DYNAMICS, and TWO DIMENSIONAL PROBLEMS, Parts 1 and 2, Journ. of Fluid Mechanics (March 1957).

Whitham, G.B., ON THE PROPAGATION OF WEAK SHOCK WAVES, Journ. of Fluid Mechanics, Vol. 1 (September 1956).

Rao, R.S., SUPERSONIC BANGS, Part II, Aeronaut. Quart., Vol. VII (May 1956).

Rao, P.S., SUPERSONIC BANGS, Part I, Aeronaut. Quart., Vol. VII (February 1956).

Lilley, G.M., Westley, R., Yates, A.H., and Busing, J.R., ON SOME ASPECTS OF THE NOISE PROPAGATION FROM SUPERSONIC AIRCRAFT, Rept. No. 71, The College of Aeronautics, Cranfield, England (February 1955).

THE SHOCK WAVE, Translation of a Russian article, The Rand Corporation, Santa Monica, California (May 6, 1954).

II. General Sources (continued)

b. Reports, Papers, Memorandums, Articles (continued)

Warren, C.H.E., NOISE ASSOCIATED WITH SUPERSONIC FLIGHT, Journ. Royal Aeronaut. Society (London), Vol. 58 (April 1954).

Cox, E.F., Plagge, H.J., and Reed, J.W., METEOROLOGY DIRECTS WHERE BLAST WILL STRIKE, Bull. American Meteorol. Soc., Vol. 35, No. 3 (March 1954).

Bleakney, W., TRANSIENT PHENOMENA IN SUPERSONIC FLOW, Chapter 14 of Modern Physics for the Engineer, McGraw-Hill Book Co., Inc., New York, N.Y. (1954).

Supino, G., AIR-WATER ANALOGY AND THE STUDY OF HYDRAULIC MODELS, NACA, TM 1359 (July 1953).

Lilley, G.M., Westley, R., Yates, A.H., and Busing, J.R., SOME ASPECTS OF NOISE FROM SUPERSONIC AIRCRAFT, Journ. Royal Aeronaut. Soc. (London), Vol. 57 (June 1953).

EQUATIONS, TABLES, AND CHARTS FOR COMPRESSIBLE FLOW, NACA Tech. Rept. No. 1135 (1953).

Lighthill, M.J., ON THE ENERGY SCATTERED FROM THE INTERACTION OF TURBULENCE WITH SOUND OR SHOCK WAVES, Proc. Cambridge Society, Vol. 49 (1953).

Lighthill, M.J., ON THE ENERGY SCATTERED FROM THE INTERACTION OF TURBULENCE WITH SOUND OR SHOCK WAVES, Proc. Cambridge Phil. Soc., Vol. 49 (1953).

Whitham, G.B., THE FLOW PATTERN OF A SUPERSONIC PROJECTILE, Communications on Pure and Applied Mathematics, Vol. V, No. 3 (August 1952).

Lighthill, M.J., ON SOUND GENERATED AERODYNAMICALLY, General Theory, Proc. Royal Society (London), A 211 (1952).

HIGH-VELOCITY FLOW IN OPEN CHANNELS, A Symposium, Transactions ASCE, Vol. 116, Paper No. 2434 (1951).

Whitham, G.B., THE BEHAVIOR OF SUPERSONIC FLOW PAST A BODY OF REVOLUTION FAR FROM THE AXIS, Proc. of Royal Society, London, A201 (1950).

Von Karman, T., THE SIMILARITY LAW OF TRANSONIC FLOW, Journal of Mathematics and Physics, Vol. 26, No. 3 (1947).

II. General Sources (continued)

b. Reports, Papers, Memorandums, Articles (continued)

Bethe, H.A., THE THEORY OF SHOCK WAVES FROM AN ARBITRARY EQUATION OF STATE, Office of Scientific Research and Development, Rept. No. 545 (1942).

Preiswerk, E., APPLICATION OF THE METHOD OF GAS DYNAMICS TO WATER FLOWS WITH FREE SURFACE, NACA Tech. Memoranda Nos. 934 and 935, Washington, D.C. (March 1940).

Riabouchinsky, D., SUR L'ANALOGIE HYDRAULIQUE DES MOUVEMENTS D'UN FLUIDE COMPRESSIBLE, Comptes Rendus de l' Academie des Sciences, Vol. 195, and Vol. 199 (1932 and 1934).

Prandtl, L., ABRISS DER STRÖMUNGSLEHRE, Braunschweig, Vieweg (1931).

Shuman, E.C., GIANT SONIC BOOM CAUSES ONLY MINOR DAMAGE TO HOUSES, Materials Research & Standards, Vol. 5, No. 2 (February 1965).

Schriever, W.R., EFFECTS OF SONIC BOOM ON BUILDINGS, Materials Research & Standards, Vol. 4, No. 11 (November 1964).

Newberry, C.W., MEASURING THE SONIC BOOM AND ITS EFFECT ON BUILDINGS, Materials Research & Standards, Vol. 4, No. 11 (November 1964).

McKinley, R.W., RESPONSE OF GLASS IN WINDOWS TO SONIC BOOMS, Materials Research & Standards, Vol. 4, No. 11 (November 1964).

Ramsay, W.A., DAMAGE TO OTTAWA AIR TERMINAL BUILDING PRODUCED BY A SONIC BOOM, Materials Research & Standards, Vol. 4, No. 11 (November 1964).

SIMULATION OF THE RESPONSE OF EQUIPMENT LOCATED IN UNDERGROUND INSTALLATIONS TO BLAST INDUCED GROUND MOTIONS, Rept. No. 102, Barry Research and Development, Watertown, Mass. (November 30, 1964).

Warner, S.E., and Cherry, J.T., PROJECT SEDAN STRUCTURE RESPONSE, U.S. Atomic Energy Commission, Plowshare Program (November 27, 1964).

II. General Sources (continued)

b. Reports, Papers, Memorandums, Articles (continued)

Allgood, J.R., and Gill, H.L., STATIC AND BLAST LOADING OF SMALL BURIED CYLINDERS, Tech. Rept. R 332, U.S. Naval Civil Engineering Laboratory, Port Hueneme, California (November 10, 1964).

Vortman, L.J., CLOSE-IN AIR BLAST FROM A NUCLEAR EVENT IN NTS DESERT ALLUVIUM, Plowshare Program, U.S. Atomic Energy Commission, Washington, D.C. (October 2, 1964).

STRUCTURAL RESPONSE TEST-NATIONAL SONIC BOOM STUDY PROGRAM, Federal Aviation Agency, Washington, D.C. (October 1, 1964).

Hampton, D., A STUDY OF PORE AIR PRESSURES GENERATED IN SOIL SUBJECTED TO AIR SHOCK WAVES, Tech. Doc. Rept. No. WL TDR-64-3, Air Force Weapons Laboratory, Kirkland Air Force Base, New Mexico (October 1964).

SONIC BOOM IS NO THREAT TO BUILDINGS, Engineering News-Record (July 2, 1964).

Webb, D.R.B., CURRENT ACOUSTIC FATIGUE PROBLEMS, Commonwealth Advisory Aeronautical Committee, Royal Aircraft Establishment, Farnborough (Prepared for Structures Coordinators of C.A.A.R.O. in Canada April 27-May 2, 1964).

Andrews Associates and Hudgins, Thompson, Bell and Assoc., SECOND INTERIM REPORT ON STUDIES OF STRUCTURAL RESPONSE TO SONIC BOOMS, Federal Aviation Agency, Washington, D.C. (April 8, 1964).

GLASS PRODUCT RECOMMENDATIONS-STRUCTURAL, Technical Service Report No. 101, Pittsburgh Plate Glass Co., Pittsburgh, Pa. (March 1964).

Kelly, J.W., CRACKS IN CONCRETE, THE CAUSE AND CURES, Concrete, Vol. 3, No. 1, Master Builders Company, Cleveland 18, Ohio (1964).

GLASSMAKER BREAKS BIG PANELS, SHATTERS AND OLD IDEA, Engineering News-Record (January 9, 1964).

Rosendorf, L., RESPONSE OF SIMPLE GEOMETRIC SHELLS TO IMPULSIVE LOADING, Picatinny Arsenal, Dover, New Jersey (July 1963).

II. General Sources (continued)

b. Reports, Papers, Memorandums, Articles (continued)

Scruton, C., RESEARCH AGAINST WIND DAMAGE, New Scientist, Vol. 18, No. 345, London, England (June 27, 1963).

Lyackhov, G.M., and Polyackova, N.I., INTERACTION BETWEEN A SHOCK WAVE IN AN ELASTO-PLASTIC MEDIUM AND A NONRIGID WALL, Translation of a Russian paper, Foreign Technology Division, Wright-Patterson A.F.B., Ohio (June 26, 1963).

BLASTING VIBRATIONS AND BUILDING DAMAGE, The Engineer (May 31, 1963).

Leonards, G.A., LABORATORY EXPERIMENTS ON THE RESPONSE OF SOILS TO SHOCK LOADINGS, Tech. Doc. Rept. No. AFSWC-TDR-62-90, Air Force Special Weapons Center, Kirkland A.F.B., New Mexico (January 1963).

Hoover, J.W. and Ross, C.A., SONIC BOOMS AND LARGE GLASS WINDOWS, The American Registered Architect, Convention Issue (1963).

Wilson, S.D., and Sibley, E.A., GROUND DISPLACEMENT FROM AIR-BLAST LOADING, Journal ASCE, Soil Mechanics and Foundations Division (December 1962).

Muirhead, J.C., Jones, W.A., and McMurtry, W.M., ON THE HAZARD OF SHOCK WAVE DAMAGE TO WINDOW GLASS, Suffield Tech. Paper No. 268, Suffield Experiment Station, Ralston, Alberta, Canada (October 19, 1962).

Bowles, R., and Sugerman, B., THE STRENGTH AND DEFLECTION CHARACTERISTICS OF LARGE GLASS PANELS UNDER UNIFORM PRESSURE, Glass Technology (October 1962).

Parrott, T.L., EXPERIMENTAL STUDIES OF GLASS BREAKAGE DUE TO SONIC BOOMS, Sound (May-June 1962).

Parrott, T.L., EXPERIMENTAL STUDIES OF GLASS BREAKAGE DUE TO SONIC BOOMS, Sound-its Uses and Control (May-June 1962).

GLASS PERFORMANCE UNDER WIND LOAD, Pittsburgh Plate Glass Co., Pittsburgh, Pa. (February 1962).

Bouwkamp, J.G., BEHAVIOR OF WINDOW PANELS UNDER IN-PLANE FORCES, Bulletin of the Seismological Society of America, Vol. 51, No. 1 (January 1961).

II. General Sources (continued)

b. Reports, Papers, Memorandums, Articles (continued)

Pilkington, L., RESEARCH ON GLASS, New Scientist, Vol. 10, No. 236 (May 25, 1961).

Edwards, A.T., and Northwood, T.D., EXPERIMENTAL STUDIES OF THE EFFECTS OF BLASTING ON STRUCTURES, The Engineer (English) (September 30, 1960).

Hutton, R.E., GROUND MOTIONS RESULTING FROM NUCLEAR SURFACE DETONATIONS, Space Technology Laboratories, Inc., Los Angeles, California (February 1960).

Arde Associates, RESPONSE OF STRUCTURES TO AIRCRAFT GENERATED SHOCK WAVES, WADC Tech. Rept. 58-169, U.S. Air Force, Wright-Patterson A.F. Base, Ohio (April 1959).

Teichman, G.A., and Westwater, R., BLASTING AND ASSOCIATED VIBRATIONS, Engineering, London (April 12, 1957).

Whitney, C.S., Anderson, B.G., and Cohen, E., DESIGN OF BLAST RESISTANT CONSTRUCTION FOR ATOMIC EXPLOSIONS, Journal Amer. Concrete Inst., Vol. 26, No. 1 (March 1955).

Newmark, M.N., AN ENGINEERING APPROACH TO BLAST-RESISTANT DESIGN, ASCE Transaction, Vol. 121, Paper 2786 (1955).

Noble, V.H., CAUSES AND REMEDIES OF PLASTER CRACKS, Progressive Architecture (November 1951).

Crandell, F.J., GROUND VIBRATION DUE TO BLASTING AND ITS EFFECTS ON STRUCTURES, Journ. Boston Soc. of Civil Engineers (April 1949).

Birkenhower, H.F., A STUDY OF HOUSE VIBRATIONS FROM QUARRY BLASTS, Bull. Seismological Soc. of America, Vol. 35, No. 3 (July 1945).

II. General Sources (continued)

b. Reports, Papers, Memorandums, Articles (continued)

Loading Conditions and Housing

WIND EFFECTS ON BUILDINGS AND STRUCTURES, The Engineer (July 5, 1963).

LAND USE IN 33 OREGON CITIES, Planning Bulletin No. 2, Bureau of Municipal Research and Service, University of Oregon, Eugene, Oregon (January 1961).

Lutesan & Amundson, COOS BAY LOOKS AHEAD--A COMPREHENSIVE DEVELOPMENT PLAN, City Planning Commission, Coos Bay, Oregon (November 1960).

Thom, H.C.S., DISTRIBUTION OF EXTREME WINDS IN THE UNITED STATES, Journ. Struct. Division, ASCE (April 1960).

Brekke, G.N., WIND PRESSURES IN VARIOUS AREAS IN THE UNITED STATES, B.M.S. Report 152, U.S. Dept. of Commerce, National Bureau of Standards (April 24, 1959).

Murphy, H.L., BLAST LOADING ON STRUCTURES, Journ. ASCE, Struct. Division, Paper 1837 (November 1958).

Merritt, Mil., BLAST LOADING ON IDEALIZED STRUCTURES USING HIGH EXPLOSIVES, Proc. of Symposium on Earthquake and Glast Effects on Structures, University of California, Los Angeles (June 1952).

Chien, N., and others, WIND TUNNEL STUDIES OF PRESSURE DISTRIBUTION ON ELEMENTARY BUILDING FORMS, Institute of Hydraulic Research, State University of Iowa, Iowa City (1951).

II. General Sources (continued)

b. Reports, Papers, Memorandums, Articles (continued)

Building Codes

UNIFORM BUILDING CODE, International Conference of Building Officials, Pasadena, California (1937 to 1964 editions).

DWELLING HOUSE CONSTRUCTION UNDER THE UNIFORM BUILDING CODE, International Conference of Building Officials, Pasadena, California (1952 to 1964 editions).

Note

Building codes examined in this investigation included available codes for the following locations.

Los Angeles, California	Baltimore, Maryland
Seattle, Washington	New York, New York
Dallas, Texas	Boston, Massachusetts
Atlanta, Georgia	Chicago, Illinois
New Orleans, Louisiana	Denver, Colorado

II. General Sources (continued)

c. Books and Pamphlets

Shapiro, A.H., THE DYNAMICS AND THERMODYNAMICS OF COMPRESSIBLE FLUID FLOW, Vols. I and II, The Ronald Press Company, New York (1954).

Courant, R., and Friedrichs, K.O., SUPERSONIC FLOW AND SHOCK WAVES, Interscience Publishers, Inc., New York, N.Y. (1948).

Miles, E.R.C., SUPERSONIC AERODYNAMICS, Dover Publications, Inc., New York, N.Y. (1950).

Bradley, J.N., SHOCK WAVES IN CHEMISTRY AND PHYSICS, Methuen & Co., Ltd., London (1962).

Von Karman, T., AERODYNAMICS, Cornell University Press, McGraw-Hill Book Co., Inc. (1954).

Von Karman, T., FROM LOW-SPEED AERODYNAMICS TO ASTRONAUTICS, The MacMillan Company, New York, N.Y. (1963).

Bradshaw, P., EXPERIMENTAL FLUID MECHANICS, The MacMillan Company, New York, N.Y. (1964).

Prandt, L., ESSENTIALS OF FLUID DYNAMICS, Hafner Publishing Co., New York, N.Y. (1952).

Condon, E.U., and Odishaw, H., HANDBOOK OF PHYSICS, McGraw-Hill Book Co., Inc. (1958).

Bonney, E.A., ENGINEERING SUPERSONIC AERODYNAMICS, McGraw-Hill Book Co., Inc., New York, N.Y. (1950).

Ridenour, L.N., MODERN PHYSICS FOR THE ENGINEER, McGraw-Hill Book Co., Inc., New York, N.Y. (1954).

Binder, R.C., FLUID MECHANICS, Prentice-Hall, Inc., New York, N.Y. (1950).

Rouse, H., FLUID MECHANICS FOR HYDRAULIC ENGINEERS, Dover Publications, Inc., New York, N.Y. (1961).

U.S. Navy Departments, HAND BOOK OF SUPERSONIC AERODYNAMICS, Vols. 1 to 6, Washington, D.C. (1959).

II. General Sources (continued)

c. Books and Pamphlets (continued)

Stoker, J.J., WATER WAVES: THE MATHEMATICAL THEORY WITH APPLICATIONS, Interscience Publishers, New York (1957).

Menzel, D.H., FUNDAMENTAL FORMULAS OF PHYSICS, Vol. 1, Dover Publications, Inc., New York, N.Y. (1960).

Scorer, R.S., NATURAL AERODYNAMICS, The MacMillan Company, New York, N.Y. (1958).

Kinney, G.F., EXPLOSIVE SHOCKS IN AIR, The MacMillan Company, New York, N.Y. (1962).

Kornhauser, M., STRUCTURAL EFFECTS OF IMPACT, Spartan Books, Inc., Baltimore, Maryland (1964).

University of Arizona, PROCEEDINGS OF THE SYMPOSIUM ON SOIL-STRUCTURE INTERACTION, Engineering Research Laboratory, Tucson, Ariz. (September 1964).

Sibert, H.W., HIGH-SPEED AERODYNAMICS, Prentice-Hall, Inc., New York, N.Y. (1948).

Ferri, A., ELEMENTS OF AERODYNAMICS OF SUPERSONIC FLOWS, The MacMillan Company, New York, N.Y. (1949).

McLeod, Jr., E.B., INTRODUCTION TO FLUID DYNAMICS, The MacMillan Company, New York, N.Y. (1963).

BLASTER'S HANDBOOK, E.C. Du Pont De Nemours & Co., Wilmington, Delaware (1963).

Rockwell, E.H., VIBRATIONS CAUSED BY BLASTING AND THEIR EFFECT ON STRUCTURES, Hercules Powder Co., Wilmington, Delaware (1934).

Mantell, C.L., ENGINEERING MATERIALS HANDBOOK, McGraw-Hill Book Co., New York, N.Y. (1958).

Hayes, W.D., GASDYNAMIC DISCONTINUITIES, Princeton Aeronautical Paperbacks No. 3, Princeton University Press, Princeton, N.J. (1960).

Department of the Army, THE EFFECTS OF NUCLEAR WEAPONS, Department of the Army Pamphlet No. 39-3 (May 1957).

II. General Sources (continued)

c. Books and Pamphlets (continued)

Windes, S.L., DAMAGE FROM AIR BLAST, Progress Reports 1 and 2, U.S. Department of the Interior, Bureau of Mines, Washington, D.C. (1943).

Tschebotarioff, G.P., SOIL MECHANICS, FOUNDATIONS, AND EARTH STRUCTURES, McGraw-Hill Book Co., New York, N.Y. (1951).

U.S. Department of Interior, SEISMIC EFFECTS OF QUARRY BLASTING, Bureau of Mines Bulletin 442, Washington, D.C. (1942).

Norris, C.H., Hansen, R.J., Holley, Jr., M.J., Biggs, J.M., Mamyet, S., Minami, J.K., STRUCTURAL DESIGN FOR DYNAMIC LOADS, McGraw-Hill Book Co., Inc., New York, N.Y. (1959).

BLASTING CLAIMS: A GUIDE FOR ADJUSTERS, National Board of Fire Underwriters-Association of Casualty and Surety Companies.

Ackeret, J., AKUSTISCHE PHANOMENE BEI HOHEN FLUGGESH-WINDIGKEITEN, Neue Zurcher Zeitung (September 18, 1952).

Liepmann, H.W., and Puckett, A.E., AERODYNAMICS OF A COMPRESSIBLE FLUID, John Wiley & Sons, New York, N.Y. (1954).

Henshaw (editor), SUPERSONIC ENGINEERING, John Wiley and Sons, Inc., New York, N.Y. (1962).

Lighthill, M.J., HIGHER APPROXIMATIONS IN AERODYNAMIC THEORY, Princeton Aeronautical Paperbacks No. 5, Princeton University Press (1960).

Whittenmore, H.L., Cotter, J.B., Stang, A.H., and Rhelan, V.B., STRENGTH OF HOUSES; APPLICATION OF ENGINEERING PRINCIPLES TO STRUCTURAL DESIGN, U.S. Dept. of Commerce, National Bureau of Standards, B.M.S. Report B.M.S. 109, Washington, D.C. (April 1, 1948).

NEW HOUSING AND ITS MATERIALS, 1940-56, U.S. Dept. of Labor, Bureau of Labor Statistics, Washington, D.C. (August 1958).

II. General Sources (continued)

c. Books and Pamphlets (continued)

UNITED STATES CENSUS OF HOUSING 1960; United States Summary, States and Small Areas, U.S. Dept. of Commerce, Bureau of Census, HC(1) No. 1, Summary, Washington, D.C. (1963).

LABOR AND MATERIAL REQUIREMENTS FOR PRIVATE ONE-FAMILY HOUSE CONSTRUCTION, Bulletin No. 1404,U.S. Dept. of Labor Statistics, Washington, D.C. (June 1964).

CONSTRUCTION REPORTS, HOUSING STARTS, U.S. Dept. of Commerce, Bureau of the Census, Washington, D.C. (December 1964).

Priestly, C.H.B., TURBULENT TRANSFER IN THE LOWER ATMOSPHERE, University of Chicago Press (1959).

Streeter, V.L., FLUID MECHANICS, McGraw-Hill Book Co., New York (Third Edition, 1962).

Taft, R.J., SNOW LOAD DESIGN DATA FOR THE LAKE TAHOE AREA, Structural Engineers Association of Northern California (December 1964).

White, H.H., THE EFFECT OF VIBRATION FROM COMMERCIAL BLASTING, Lusher & Lusher, Hazleton, Penn. (April 1953).

Wood, W.F. and Snell, J.B., PREDICTIVE METHODS IN TOPOGRAPHIC ANALYSIS; I. RELIEF, SLOPE, AND DIRECTION ON INCH-TO-THE-MILE MAPS IN THE UNITED STATES, Technical Report EP-112, Quartermaster Research & Engineering Center, U.S. Army, Natick, Mass. (April 1959).

Barkan, D.D., DYNAMICS OF BASES AND FOUNDATIONS, McGraw-Hill Book Co., Inc., New York, N.Y. (1962).

UNIFORM BUILDING CODE, International Conference of Building Officials, Pasadena, California (1937 to 1964 editions).

DWELLING HOUSE CONSTRUCTION UNDER THE UNIFORM BUILDING CODE, International Conference of Building Officials, Pasadena, California (1952 to 1964 editions).

Cheers, F., ELEMENTS OF COMPRESSIBLE FLOW, John Wiley and Sons, Ltd., London (1963).

THE EFFECTS OF ATOMIC WEAPONS, The Combat Forces Press, Washington, D.C. (August 1950).

II. General Sources (continued)

c. Books and Pamphlets (continued)

Thewlis, J., ENCYCLOPAEDIC DICTIONARY OF PHYSICS, Vol. 6, Pergamon Press, New York, N.Y. (1962).

Llowarch, W., RIPPLE TANK STUDIES OF WAVE MOTION, Oxford University Press, (1961).

Anderson, L.O., and Heyer, O.C., WOOD-FRAME HOUSE CONSTRUCTION, Agriculture Handbook No. 73, U.S. Dept. of Agric., Washington, D.C. (February 1955).

... R.J., SMITHSONIAN METEOROLOGICAL TABLES, Smithsonian Institution, Washington, D.C. (1951).

... MANUAL - STRUCTURAL ENGINEERING, Nav docks DM-2, ... of the Navy, Bureau of Yards and Docks, Washington 25, D.C. (February 12, 1962).

Table A-1

Selected Characteristics of New Non farm 1-Family Houses

1940, 1950, 1954, 1955, 1956
(Percent distribution of houses according to characteristic)

Characteristics	1940	1950	1954	1955	1956
Average floor area (sq. ft.)	1,177	983	1,140	1,170	1,230
TYPE OF HOUSE	(1)	(1)	*	*	100
Detached	(1)	(1)	*	*	97
Semidetached	(1)	(1)	*	*	1
Row	(1)	(1)	*	*	1
Unknown			*	*	1
NUMBER OF STORIES	100	100	*	*	100
1 story	67	86	*	*	87
Split level	*	*	*	*	6
Other	33	14	*	*	6
Unknown			*	*	1
FLOOR AREA (SQ. FT.)	*	*	100	100	100
Less than 800	*	*	18	7	5
800 to 999	*	*	20	22	17
1,000 to 1,199	*	*	24	30	31
1,200 to 1,499	*	*	19	26	26
1,500 to 1,799	*	*	10	7	10
1,800 and over	*	*	7	5	9
Unknown	*	*	2	3	2
NUMBER OF BEDROOMS	*	100	100	100	100
2 bedrooms or less	*	66	34	23	21
3 bedrooms	*	33	58	68	70
4 bedrooms or more	*	1	5	6	8
Unknown	*		3	3	1
NUMBER OF BATHROOMS	100	100	*	*	100
1 bathroom	80	92	*	*	49
1 complete, 1 partial bathroom	12	4	*	*	20
2 complete bathrooms	7	3	*	*	21
More than 2 complete bathrooms	1	1	*	*	7
No bathroom	*	*	*	*	1
Unknown			*	*	2
BASEMENT	100	100	100	100	100
Full or partial basement	69	39	41	42	43
No basement	31	61	58	55	55
On slab	(2)	4	*	16	16
With crawl space	31	57	*	39	39
Unknown			1	3	2
UTILITY ROOM	*	100	*	100	100
With utility room	*	20	*	33	37
No basement	*	20	*	27	30
With basement	*	*	*	6	7
No utility room	*	20	*	27	30
Unknown	*		*	3	5
GARAGE FACILITIES	100	100	*	*	100
Garage	80	41	*	*	50
Carport only	(2)	6	*	*	17
No garage or carport	20	53	*	*	31
Unknown			*	*	2

Table A-1 (continued)

Characteristics	1940	1950	1954	1955	1956
EXTERIOR WALL CONSTRUCTION	100	100	100	100	100
Masonry	11	11	13	20	16
Brick	10	6	9	15	12
Other masonry	1	5	4	5	4
Frame	89	89	82	77	83
Brick facing	20	12	20	18	26
Brick and wood facing			5	8	7
Wood facing	43	43	31	29	24
Asbestos shingle facing	4	21	14	8	9
Stucco	15	11	12	14	14
Other facing	7	2			3
All other construction	*	*	3	1	(2)
Unknown			2	2	1
SHEATHING (FRAME HOUSES ONLY)	100	100	*	*	100
Sheathed	69	80	*	*	83
Wood plank	49	40	*	*	31
Plywood	1	4	*	*	7
Insulation board	14	23	*	*	32
Gypsum board	5	12	*	*	9
Other	(2)	1	*	*	4
Unsheathed	31	20	*	*	17
INTERIOR WALL CONSTRUCTION	100	100	*	*	100
Plaster	90	50	*	*	44
On gypsum lath	56	49	*	*	40
On metal or wood lath	34	1	*	*	4
Dry wall	10	50	*	*	55
Gypsum board	*	48	*	*	48
Other	*	2	*	*	7
Unknown			*	*	1
ROOFING	100	100	*	*	100
Shingles	83	92	*	*	84
Asbestos	*	*	*	*	7
Asphalt	47	82	*	*	66
Wood	36	10	*	*	11
Built-up	5	6	*	*	11
Other	12	2	*	*	3
Unknown			*	*	2
INSULATION: PERCENT OF ALL HOUSES WITH INSULATION IN:					
Ceiling	25	83	*	*	81
Walls	10	34	*	*	33
Perimeter	*	1	*	*	5
WINDOWS ABOVE BASEMENT, PREDOMINANT FRAME MATERIAL	100	100	100	100	100
Wood	91	69	63	57	57
Steel	9	22	18	16	11
Aluminum	*	5	17	24	29
Unknown			2	3	3
WINDOW SCREENS	100	100	*	*	100
With screens	89	62	*	*	77
Aluminum	1	8	*	*	56
Bronze	27	12	*	*	3
Copper	10	5	*	*	6
Galvanized steel	50	36	*	*	10
Other	1	1	*	*	(2)
Unknown material			*	*	2
No screens	11	38	*	*	23

Table A-1 (continued)

Characteristics	1940	1950	1954	1955	1956
DOOR SCREENS	100	100	*	*	100
With screens	89	45	*	*	70
Aluminum	1	2	*	*	46
Bronze	27	9	*	*	3
Copper	10	2	*	*	4
Galvanized steel	50	31	*	*	13
Other	1	1	*	*	1
Unknown material			*	*	3
No screens	11	55	*	*	30

* No data available
(1) Only single-family detached houses survey
(2) No cases reported, or less than 0.5%

APPENDIX B - TEST STRUCTURES

1. New Structures

Seven new test structures were built at the Oscura Range Camp (C-1 - Blockhouse; W-2 - Metal Lath; W-3 - Drywall; W-4 - Jackhouse; 2S-5 - Doubledeck; PF-6 - Prefab; and Greenhouse). In addition, various types of storefront glass were installed along the complete 60 foot north wall of an existing structure called Storefront.

a. Design of the structures was carried out to agree with minimum provisions in the 1958 edition of the Uniform Building Code. While some slight departures from the original drawings were made during construction by the workmen, these departures were carefully noted by the inspector on site and incorporated into the drawings to reflect the as-built condition. It is stressed that this inspector was continuously present on the site during the construction period. He was instructed to note each phase of construction for inclusion in as-built drawings and to periodically take typical samples of all materials for later laboratory testing.

PF-6 was purchased in prefabricated panels from a Fort Worth, Texas manufacturer and erected on the

site. The house model is known as Sportsman I and was purchased complete except for plumbing and electrical fixtures and connections.

The greenhouse was purchased as a package unit complete with glass of foreign manufacture. During the glazing of the greenhouse the glass was installed and secured in place by small wire brads located at two points along the bearing edges much as glass is installed in older greenhouses across the country. This procedure causes a stress concentration point where each of the nails bears on the glass to restrain movement.

The storefront was built in an existing metal building on the site (40 x 60 feet)modified by removing 60 lineal feet of side wall and installing 60 lineal feet of plate glass storefront construction. The plate glass, of various sizes, was mounted in fixed, flexible and resilient mountings.

Refer to the attached "as-built" drawings for detail of structures.

b. Description and photos of new construction:

C-1 - Blockhouse

Foundation:	Concrete slab on grade, 2500 psi concrete with 6" x 6"/#10 x #10 welded wire fabric reinforcement.

Exterior Walls:	8" x 8" x 16" Grade A, Concrete Blocks with Duro-wall reinforcement.
Interior Walls:	6" x 8" x 16" Grade A, Concrete Blocks with Duro-wall reinforcement.
Mortar:	Lime rich mix and silica sand (1950 psi average compressive strength).
Roof Joists:	2 x 10 Douglas Fir at 24" ctrs.
Interior Finish:	2 coats gypsum plaster applied to expanded metal lath on ceiling. Base coat: extra fibered gypsum and washed silica sand 1:1-1/2 by volume, Finish coats: unfibered gypsum and washed silica sand.
Roof:	3/8 Plywood with 15-lb. mineral coated asphalt cap sheet.
Glass:	Picture window 60" x 120" x 1/4" Solargray; casement windows 1/8" DSB; double hung windows 8 light and 2 light, 1/8" SSB; sliding door 7/32" B crystal sheet; doorlight 1/8" SSB; hermetically sealed 3' x 3' windows with 2 sheets 1/8" DSA.

W-2 - Metal Lath

Foundation:	Concrete slab on grade, 2500 psi concrete with 6" x 6"/#10 x #10 welded wire fabric reinforcement.
Walls:	2 x 4 studs at 16" ctrs. Metal lath and 3 coat gypsum plaster on interior wall surfaces. Paper backed welded wire fabric (2" x 2"/#12 x #12) with stucco on exterior wall surfaces.

Trusses:	Roof trusses are gang nailed with 2 x 6 top chord, 2 x 4 bottom chord and 2 x 4 king post. Trusses were placed at 24" ctrs. Roof slope 2:12.
Ceiling:	Metal lath and 3 coat gypsum plaster. Metal lath is attached to 1" x 4" furring strips at 16" ctrs which are nailed to underside of trusses.
Roof:	3/8 plywood with 15-lb. felt and 90-lb. mineral coated asphalt cap sheet.
Glass:	Picture window 60" x 120" x 1/4" clear plate; casement windows 1/8" DSB; double hung windows 8 light and 2 light, 1/8" SSB; sliding door 7/32" B crystal sheet; doorlight 1/8" SSB; hermetically sealed 3' x 3' window with 2 sheets 1/8" DSA.

W-3 - Drywall

Foundation:	Raised footing with interior concrete footings. 2500 psi concrete with #4 reinforcing bars.
Floor:	2 x 8 DF joists at 16" ctrs. with 5/8" CD plywood floor.
Walls:	2 x 4 DF studs at 16" ctrs. 1/2" thick gypsum sheetrock with taped joints on interior surfaces. Paper backed welded wire fabric (2" x 2"/ #12 x #12) with stucco on exterior surfaces.
Trusses:	Roof trusses are gang nailed with 2 x 6 top chord, 2 x 4 bottom chord and 2 x 4 king post. Trusses placed at 24" ctrs. Roof slope 2:12.
Roof:	3/8" plywood with 15-lb. felt and 90-lb. mineral coated asphalt cap sheet.

Glass:	Picture Window 60" x 120" x 1/4" Solargray; casement windows 1/8" DSB; double hung windows 8 light and 2 light, 1/8" SSB; sliding door 7/32" B crystal sheet; doorlight 1/8" SSB; hermetically sealed 3' x 3' windows with 2 sheets 1/8" DSA.

W-4 - Jackhouse

Foundation:	Raised footing with interior concrete footings. 2500 psi concrete with #4 reinforcing bars. Two diagonal corners of the footing were omitted to allow for placement of a screw jack to simulate settlement.
Floor:	2 x 8 DF joists at 16" ctrs. supported on footings and girders with 5/8" CD plywood floor.
Walls:	2 x 4 DF studs at 16" ctrs., 3/8" thick wood lath with two coat gypsum plaster on interior surfaces during Part "A". Wood lath and plaster removed and 3/8" thick perforated gypsum plasterbase with two coat gypsum plaster installed for Part "B". Exterior wall surfaces were 1 x 8 redwood bevel edge siding throughout the tests.
Trusses:	Roof trusses are gang nailed with 2 x 6 top chord, 2 x 4 bottom chord and 2 x 4 king post. Trusses placed at 24" ctrs. Roof slope 2:12.
Roof:	3/8" plywood with 15-lb. felt and red cedar shingles, clear and better, 16" x 3/8" butt, 6" to weather.
Glass:	Picture window 60" x 120" x 1/4" clear plate; casement windows 1/8" DSB; double hung windows 8 light and 2 light, 1/8" SSB; sliding door 7/32" B crystal sheet; doorlight 1/8" SSB; hermetically sealed 3' x 3' windows with 2 sheets 1/8" DSA.

2S- - Doubledeck

Foundation:	Raised footing with interior concrete footings and continuous raised concrete footing under interior bearing wall. 2500 psi concrete with #4 reinforcing bars.
Floor:	1st Floor - 2 x 8 DF joists at 16" ctrs. with 5/8" CD plywood flooring. 2nd Floor - 2 x 12 DF joists at 24" ctrs. with 5/8" CD plywood flooring.
Walls:	2 x 4 DF studs at 16" ctrs. 3/8" thick wood lath with two coat gypsum plaster on interior surfaces. During Part "A" tests the exterior surfaces had brick veneer to the first floor top plate line and 1" x 8" redwood bevel edge siding on the second floor exterior surface. For Part "B" tests the brick veneer was removed and replaced with the 1" x 8" redwood bevel siding and a brick fireplace with chimney was built into the opening formerly used for the sliding glass door.
Trusses:	Roof trusses are gangnailed with 2 x 6 top chord, 2 x 4 bottom chord and 2 x 4 king posts. Trusses placed at 24" ctrs. Roof slope 2:12.
Roof:	3/8" plywood with 15-lb. felt and red cedar shingles, clear and better, 16" x 3/8" butt, 6" to weather.
Glass:	Picture windows 60" x 120" x 1/4" Solargray on 1st Floor and clear plate on 2nd Floor; casement windows 1/8" DSB; double hung windows 8 light and 2 light, 1/8" SSB; sliding door 7/32" B crystal sheet; doorlight 1/8" SSB; hermetically sealed 3' x 3' windows with 2 sheets 1/8" DSA; sliding window 1/8" DSB.

PF-6 - Prefab

Foundation:	Concrete slab on grade. 2500 psi concrete with 6" x 6"/#10 x #10 welded wire fabric reinforcement.
Walls:	Prefabricated panels with 2 x 4 hemlock studs at 16" ctrs. 1/2" gypsum sheetrock applied to interior surfaces for Part "A" test. Sheetrock was removed and replaced with 3/8" thick perforated gypsum plasterbase with two coat gypsum plaster for Part "B" tests. Exterior wall surfaces were covered with 3/8" unfinished cedar plywood, staple gun applied.
Trusses:	Prefabricated wood Fink-type trusses with glued and nailed plywood gussets. Chords and web members are 2 x 4 Douglas Fir with the trusses placed at 24" ctrs.
Roof:	1/2" plywood, 15-lb. felt and 210-lb. grade C asphalt square tab shingles.
Glass:	Factory glazed sash 1/8" SSA and DSB.

G-7 - Greenhouse

Foundation:	9' x 12' Concrete strip footing on grade. Normally this structure would be placed on a concrete slab but the slab was not thought necessary for test purposes.
Frame:	Precut mortised and rabbetted redwood.
Glazing:	1/8" single strength and double strength glass held in place with wire brad finishing nails.

S-8 - Storefront

Foundation:	Existing slab on grade.
Structure:	Existing on site. Parkersburg prefabricated metal building 40 x 60 foot in plan.
Modification:	Remove metal panels on north wall and install various types of storefront construction utilizing 1/4" plate glass in various sizes and three types of glass mountings: fixed, flexible and resilient.
Glass:	Storefront windows A, B, C are 5'3" x 10'8" clear 1/4" plate except for B which is Solargray plate; windows D and E are 7'6" x 10' clear 1/4" plate; windows F, G, H are 5' x 9'6" clear 1/4" plate; window I is 5' x 9'6"clear 3/8" plate. Four windows (4'2" x 6'10") with 6 panes of wiremesh glass in each and 11 windows (4' x 3'6") with 4 panes of wire mesh glass in each window remained during tests.

2. Old Structures (existing)

a) Pump House - located 100 feet north of W-4 is a wood frame building on concrete slab 8'4" x 10'5". Exterior finish is asbestos shingles with no interior finish and has a gable roof with mineral surfaced asphalt roll roofing. The west wall has one 3'3" x 3'3" window with 12 panes, two of which were broken. This structure houses a deep well pump and a well reported to be 600 feet deep.

b) Wash House - located 100 feet north of W-4 on centerline of site is a wood frame structure 6'3" x 8'4" on a concrete slab. Exterior finish is asbestos shingle with no interior finish. There are two windows

2'2" x 2'2" with 6 panes in each. One of the windows was boarded up.

c) Radar Building - located 800 feet southwest of 2S-5 is a concrete frame structure with 8" concrete block filler walls. It has a raised concrete slab floor and an 8" concrete slab roof with added concrete beams to support radar antennae loads. The interior walls are plastered and are non-load bearing. Windows are: 1 window 5' x 1'3" with 2 panes glass; 2 windows 5' x 3' with 1 pane glass; 1 window 4'6" x 2'6" with 2 panes glass; 1 window 5' x 2'6" with 2 panes glass; 2 windows 5' x 3' with 1 pane of hermetically sealed glass (2 panes separated by air space) 1 double door with 3 panes of glass each door; 1 single door with 3 panes glass each door; 1 single door with 3 panes of glass 1'3" x 2'10" each, and 2 double doors with 2 panes of 1' x 2'3" wire mesh reinforced glass in each door.

d) Pump House - located next to Radar Building is 10' x 10'7" with 8 inch concrete block walls and a flat wood roof. The house has 1 window 4'6" x 1'3" with 2 panes of glass.

e) Radar Shop - located 500 feet west of W-4 is a prefabricated metal building 40' x 24' with a concrete slab floor and the interior finished with sheetrock. There are seven windows 3'6" x 2'6" with 4 panes each window.

f) Barracks Building (H-Building) - located 500 feet northwest of W-4 is an "H" shaped metal building made by Butler Manufacturing Co. with wings 20' x 100' and a cross wing 20' x 40' housing the latrine and boiler room. The structure is placed on a concrete slab and is finished on the interior with sheetrock walls and suspended sheetrock ceiling. The shower room has ceramic tile floor and walls with the wall tile attached by adhesive. There are 49 windows 2'6" x 3'2" with four panes each, some of which are wire

mesh reinforced glass. There are four double doors with two 2'1" x 2'8" panes in each door and one single door with a 2'1" x 2'8" window divided into two panes. See drawings.

g) Communications Building - located 4000 feet west of W-4 is a concrete frame structure with concrete block filler walls and concrete slab floor. The structure has a reinforced concrete slab roof to support microwave antennae. There are three windows 4'8" x 3'6" with three panes, two windows 4'8" x 4'8" with 4 panes, one window 4'8" x 2'4" with two panes and two doors with three panes 1'3" x 3'. All glass is wire mesh reinforced. This structure is active and houses telephone switchgear for the Range.

h) 366th TAC Building and Towers - located 5 miles northwest of the site is a prefabricated 30' x 60' metal (Mestex) building erected on a concrete slab. The north half of the building is set aside for office use and is finished on the interior with sheetrock on the walls and a suspended sheetrock ceiling. There are eight windows 5' x 4' with four panes each, four windows 2' x 2' with two panes each, and three doors with two each 1'6" x 2' wire mesh reinforced glass panes. The structure also has a 250-gallon butane tank and a 3-ton air conditioner mounted on exterior concrete slabs. In addition there are two 40-foot wood pole towers nearby with glass-enclosed cabs used by the 366th Range control officers. The 9' x 9' cabs are glazed with heat-absorbing plate glass.

i) Phillips Hill Radar - located approximately 3-1/2 miles southwest of the site is a 29' x 66' reinforced concrete building having concrete block filler walls, floor slab on grade, and a concrete slab roof. It is similar to the Communications Building noted above.

j) Abandoned Ranch House - located 2-1/2 miles east of the site is a 30' x 34' wood frame house with stucco exterior, interior sheetrock walls and ceiling, raised wood floor, wood frame gabled roof with corrugated iron roofing and a 6' x 16'4" screen-covered porch. Windows are: five 2' x 4'7", 8 panes, screen covered, double hung, wood frame; five 2' x 4'7", 2 pane, screen covered, double hung, wood frame; four 2'8" x 2'9", 2 pane, double hung wood frame; and one double window with 21" x 24" panes. The house in in a general state of extreme disrepair having been abandoned for many years.

Outbuildings with the abandoned ranch are:

1) Storage House and Storm Cellar - 8'7" x 12'6" made of concrete block with wood frame floor and corrugated iron roofing.

2) Chicken House and Feed Storage - 22' x 7'8" made of concrete block with stucco exterior and interior with concrete slab floor and corrugated iron roofing.

3) Garage - 22' x 7'8" with room at rear of building has a wood frame structure with stucco on exterior and on the interior of the room. Stucco is unpainted.

k) Withers' Ranch - located 4 miles east of the site is occupied by Mr. and Mrs. Withers. The house is part of the ranch headquarters complex with seven outbuildings and a large trailer home, however, the ranch house was the only structure observed. The ranch house is about 33' x 45' in plan with exterior walls of 8" concrete block. Interior walls are wood stud with sheetrock and a thin coat of plaster finish. Concrete block walls appear to be finished on the interior and exterior with a dash coat of

plaster and stucco respectively. The floor is wood and the ceiling is sheetrock with rough-taped joints and a dash coat of plaster. The roof is corrugated metal as on many other structures in the area. Windows are steel casement type with muntins.

1) Helm's Ranch - located 6-1/2 miles east of the site is an occupied structure constructed of concrete with an addition of concrete block and with concrete slab floors. The roof is corrugated metal with interior stud walls and ceilings presumably plastered. The house has 12 double hung windows and 3 steel casement windows with a total glass area of approximately 115 square feet. The Helm's Ranch House had two original wood lath and plaster ceilings and plaster over the formed concrete and block walls. This house is basically two structures, one old (circa 1920), and one new (1960). The original section combines formed concrete walls (stucco exterior and plaster interior), wood lath and plaster ceilings, wood floors, wood sash and a corrugated steel roof. A living room with fireplace, kitchen, pantry and small bedroom comprise the rooms in this section. The new area includes two bedrooms and a bath. The construction is light weight concrete block exterior walls, wood stud and drywall interior partitions and drywall ceilings. The block is stuccoed on the exterior and plastered on the interior. Windows are steel framed.

m) Other structures and equipment subjected to test sonic booms include:

1) Communications Building area:

8' x 10" metal building with 9' walls; 3 windows 3' x 3', 4 panes in each. 5-KVA pole-mounted transformer. 1,000 feet northwest of Communications Building.

10' x 14' metal building on skids, 9'

walls. Evaporative cooler mounted on side. 200 feet west of Communications Building.

100 pairs of telephone lines on pole terminating underground 300 feet northwest of Communications Building.

Approximately 50 pairs of telephone lines on poles terminating underground 400 feet west of Communications Building.

One 10-KVA and one 15-KVA transformer mounted on 25' poles in area.

5,000-gallon upright water tank on concrete foundation in area. 1,000-gallo LP gas tank horizontal on concrete foundation in area.

Two fuel tanks 200 and 400 gallons on angle-iron frames in area.

Emergency generator on angle-iron frame in area.

One 6' x 8' and one 8' x 10' Butler Building on skids in area.

4-wheel trailer 8' x 20', electronic equipment with 5' parabolic dish antenna, operated by AVCO Corporation in area.

Two 7-1/2-ton air conditioners on angle-iron frames (mounted on Communications Building).

Seven VHF antennas of various types mounted on Communications Building.

2) Test Structure area:

One 25' and one 30' x 8' van type, 4-wheel trailers. Tracking type antenna mounted atop 30' trailer. Trailers contain radar. Equipment mounted on jacks on concrete pad. Trailers cable guyed.

One portable air cooling device, electric motor with compressor, mounted on wood frame.

Air cooling device on wood frame with steel ducts.

One 5-gallon fuel tank on skids, one 200-gallon fuel tank on angle-iron frame.

Two 56.3-KVA generators and two 12-1/2-KVA generators on steel frames.

Galvanized water tank, vertical on 8' x 12' concrete slab.

Six-unit bank distributing transformer on concrete slab.

Air conditioner on concrete slab

Three 5-KVA pole-mounted transformers.

200-gallon LP tank on railroad crossties.

Evaporative cooler blower on angle tower and concrete piers.

One 10-KVA and two 5-KVA transformers and two 25-KVA and one 15-KVA transformers in general area of Operations Trailer, mounted on poles.

One 500-gallon LP tank on skids.

Three evaporative coolers on wooden frames.

Elevated tank 25' high mounted on a pipe frame and has an estimated 3,000-gallon capacity.

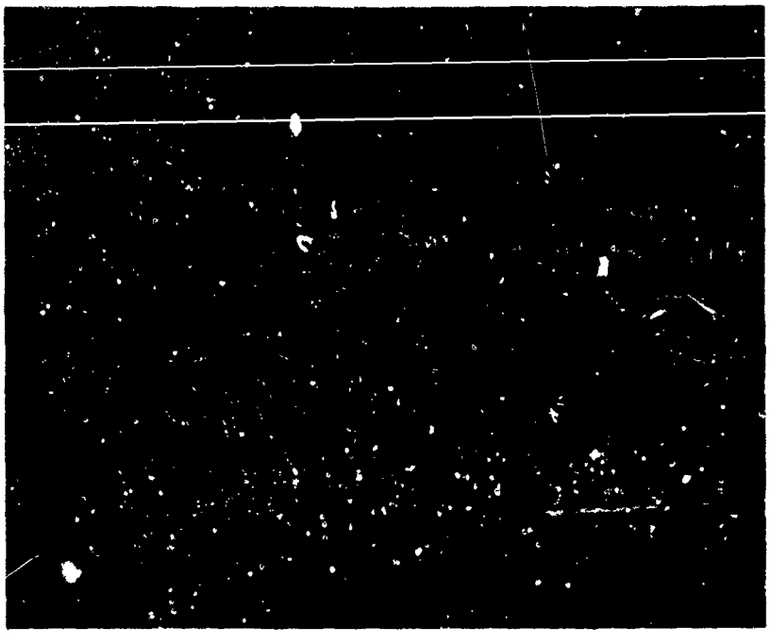


Fig. B1-1 Exterior View of Blockhouse, C-1

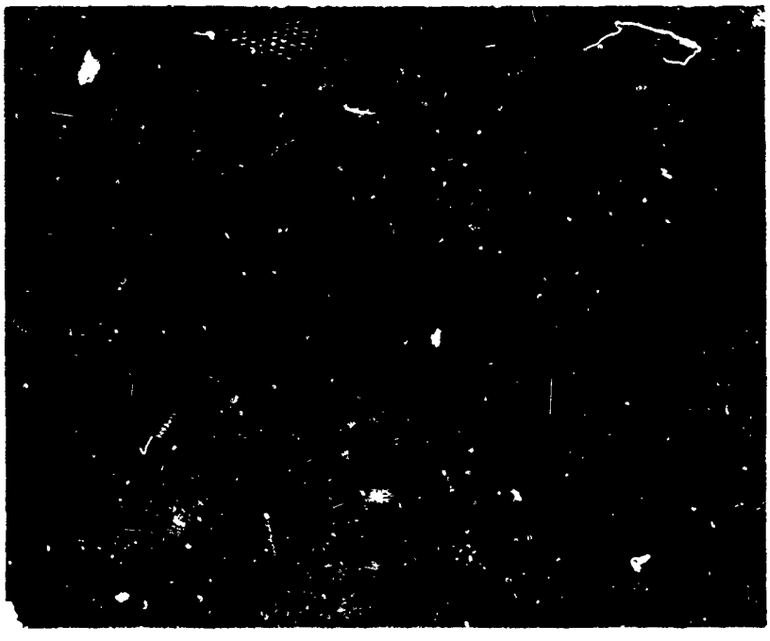


Fig. B1-2 Interior View of Blockhouse, C-1 Prior to Plastering. Note Use of Metal Lath Corner Reinforcement and 1" x 4" Furring Strips at 16" Ctrs.

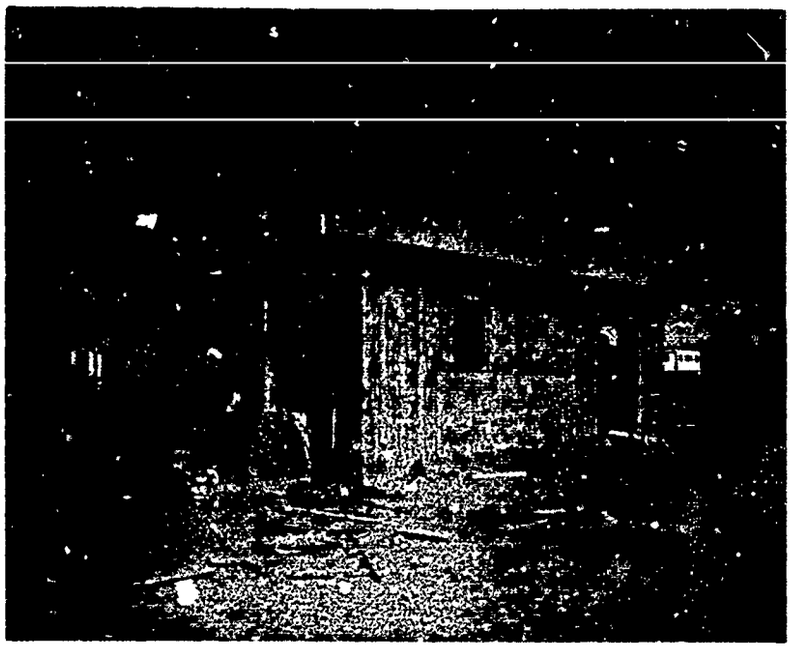


Fig. B1-3 Exterior View of Metal Lath, W-2. Note the Effect of Dry Winds on the Curing of the Basecoat of Stucco.

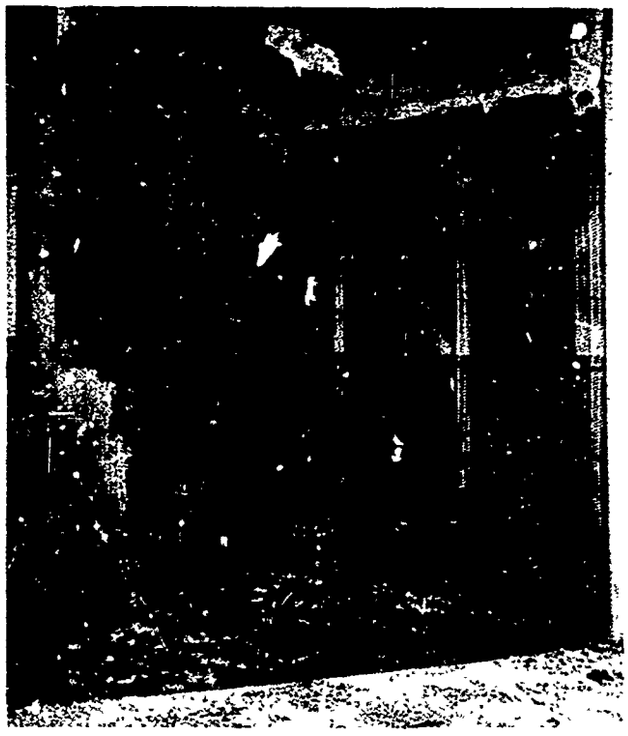


Fig. B1-4 Interior View of Metal Lath, W-2, Showing Lath and Plaster Application

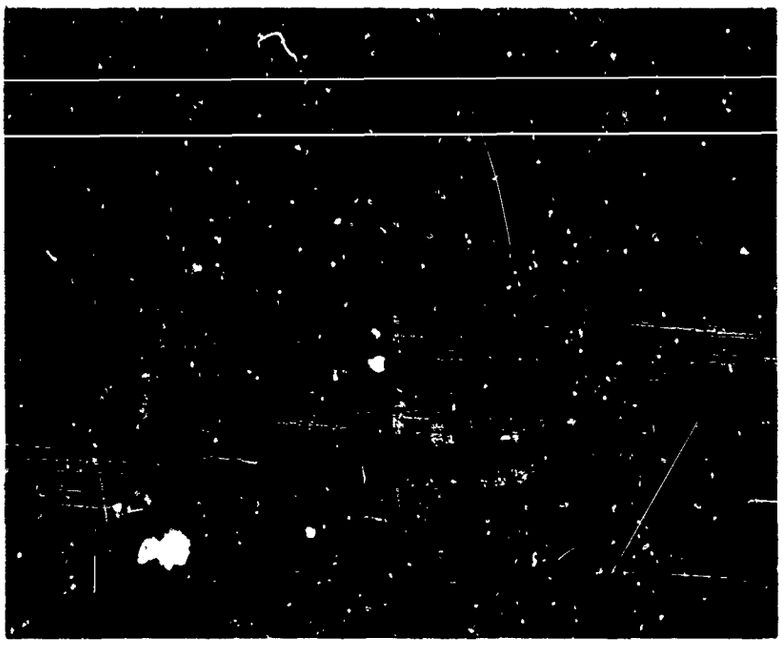


Fig. B1-5 Exterior View of Drywall, W-3 Prior to Application of Finish Coat of Stucco

Fig. B1-6 Interior View of Drywall, W-3 Prior to Application of 1/2" Thick Gypsum Sheetrock

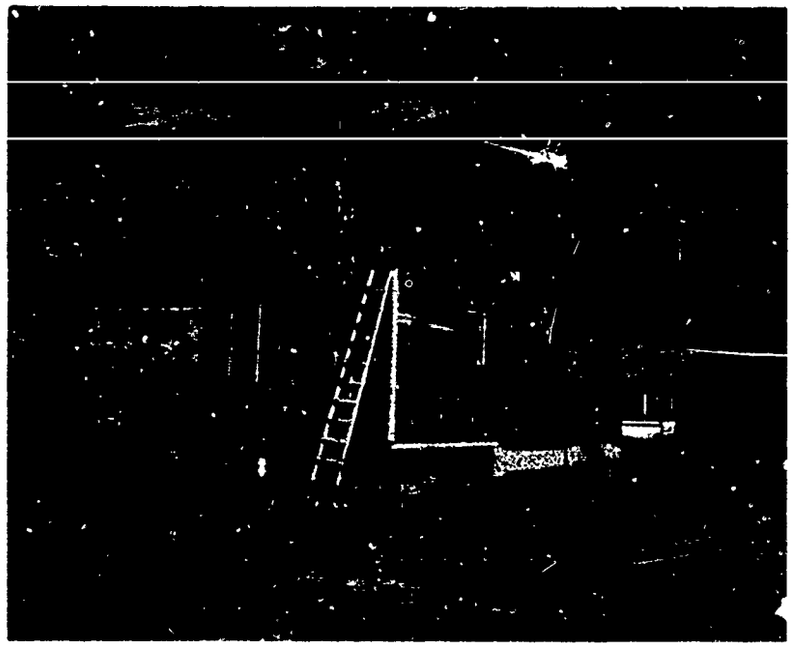


Fig. B1-7 Exterior View of Jackhouse, W-4. Note Post at Corner is Location of Future Screw Jack.

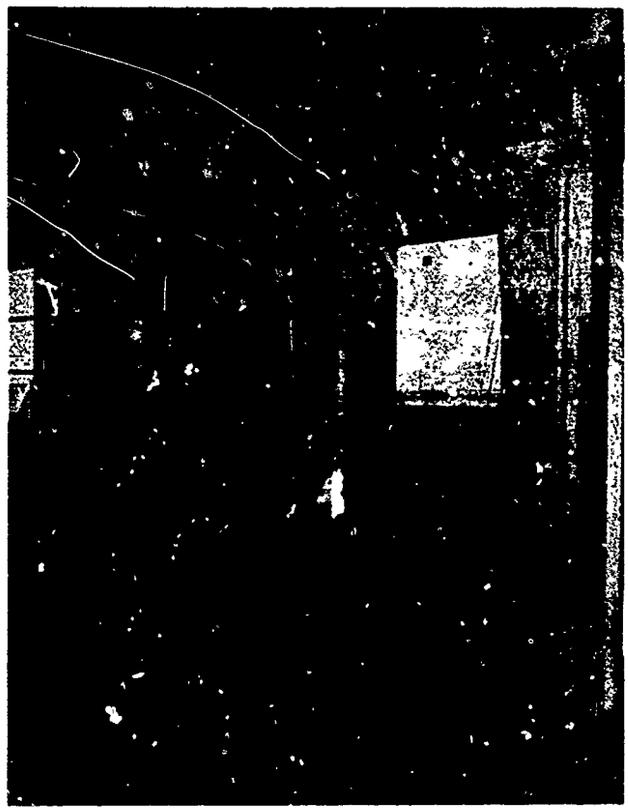


Fig. B1-8 Interior View of Jackhouse, W-4, Showing Application of Wood Lath

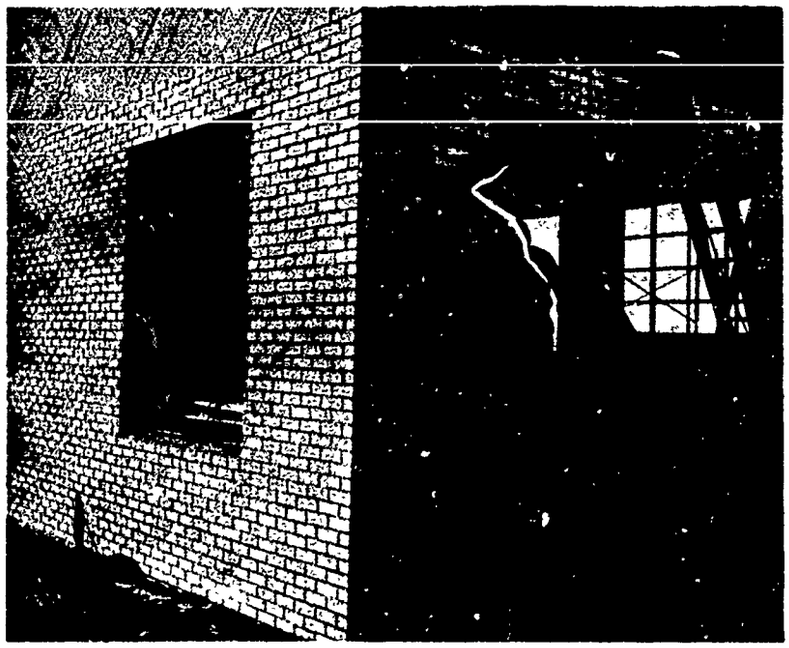


Fig. B1-9 Exterior View of Doubledeck, 2S-5, Showing Brick Veneer With Stacked Bond and Common Bond. Flemish Bond Section is Not Shown. Veneer is Tied to Sheathing With Ties at 12" Ctrs. Every Second Course

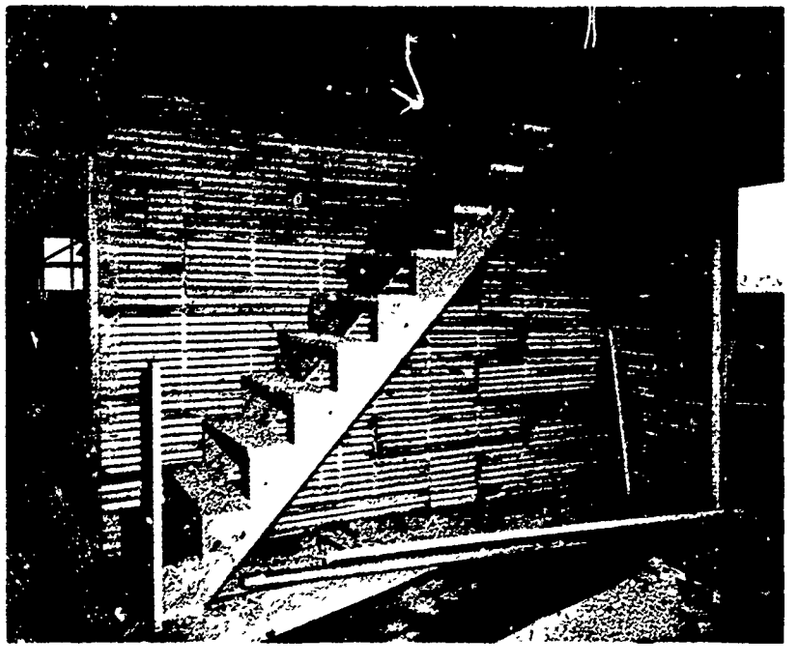


Fig. B1-10 Interior View of Stairs in 2S-5 and First Floor Lathing

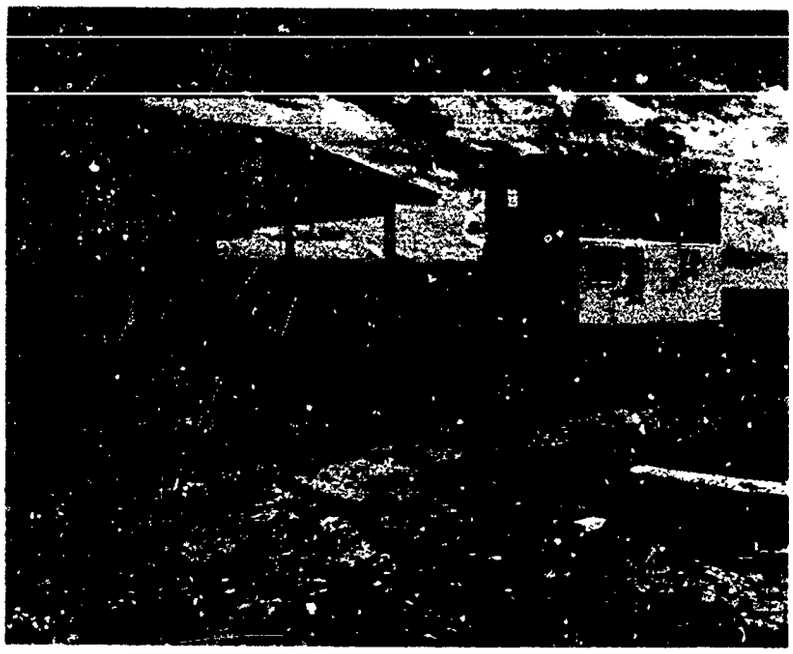


Fig. B1-11 Exterior View of Doubledeck, 2S-5, Prior to Part "A" Testing Showing the Brick Veneer

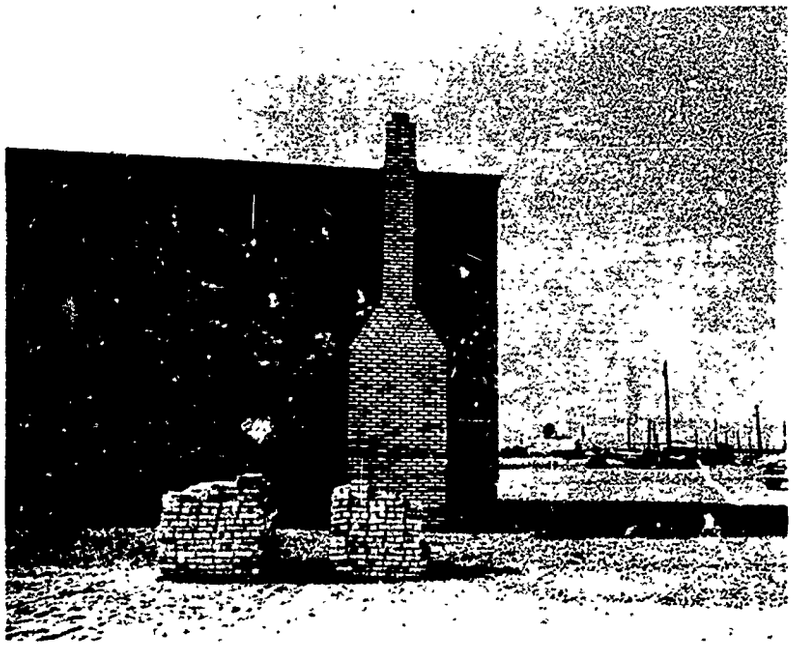


Fig. B1-12 Exterior View of Doubledeck, 2S-5, prior to Part "B" Testing. Note That Brick Veneer Has Been Removed and Replaced by Redwood Siding. Note Also the New Brick Fireplace and Chimney.

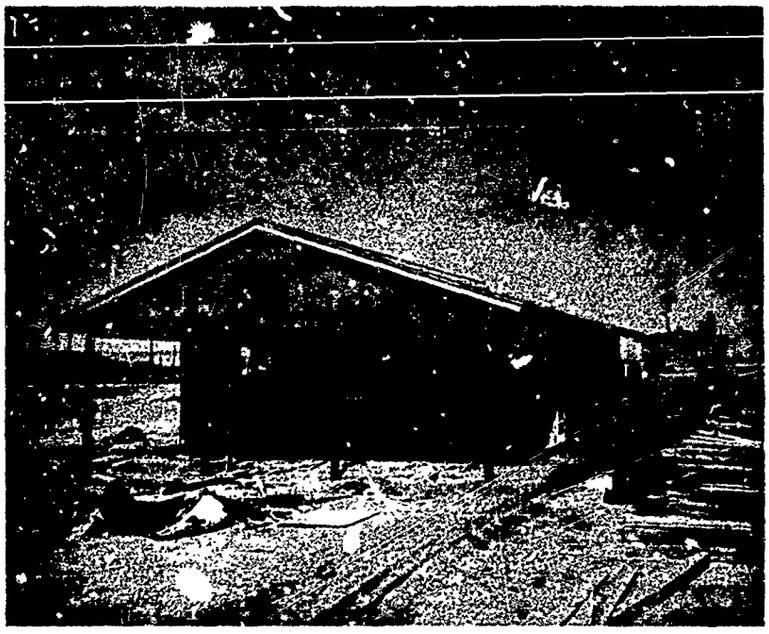


Fig. B1-13 Exterior View of Prefab, PF6. Note Use of Exterior Plywood Siding and Single Hung Aluminum Windows

Fig. B1-14 Interior View of PF-6 Showing the Sheetrock Application

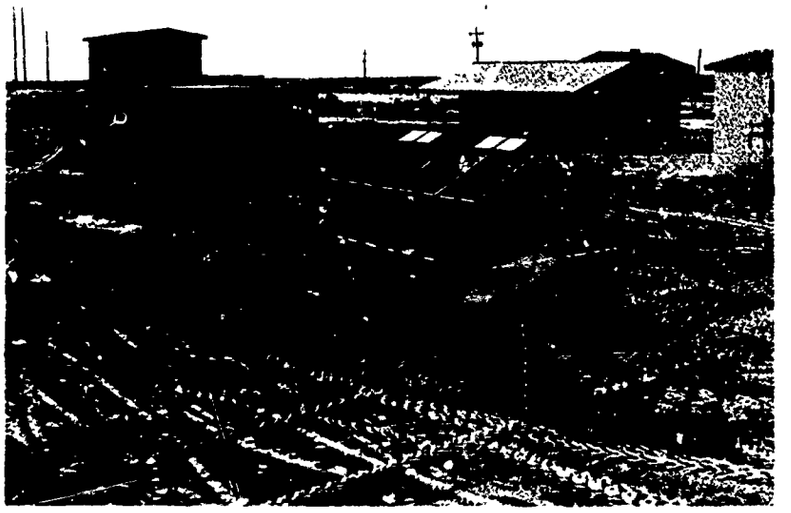


Fig. B1-15 Exterior View of Greenhouse Prior to Glazing

Fig. B1-16 View of Precut Members Before Glazing (Greenhouse)

Fig. B1-17 View After Glazing Greenhouse. Note Wire Brads Holding Glass

Fig. B1-18 View of Storefront With Glass in Place Prior to Sonic Boom Tests

Fig. B1-19 Aluminum Extrusions Used on the Storefr Note the Three Types of Mountings Used: Fixed, Flexible and Resilient.

Fig. B2-1 View of Withers' Ranch Headquarters Showing the Various Outbuildings

Fig. B2-2 Interior View of Withers' Living Room. Note Tape Joints on Ceiling Sheetrock.

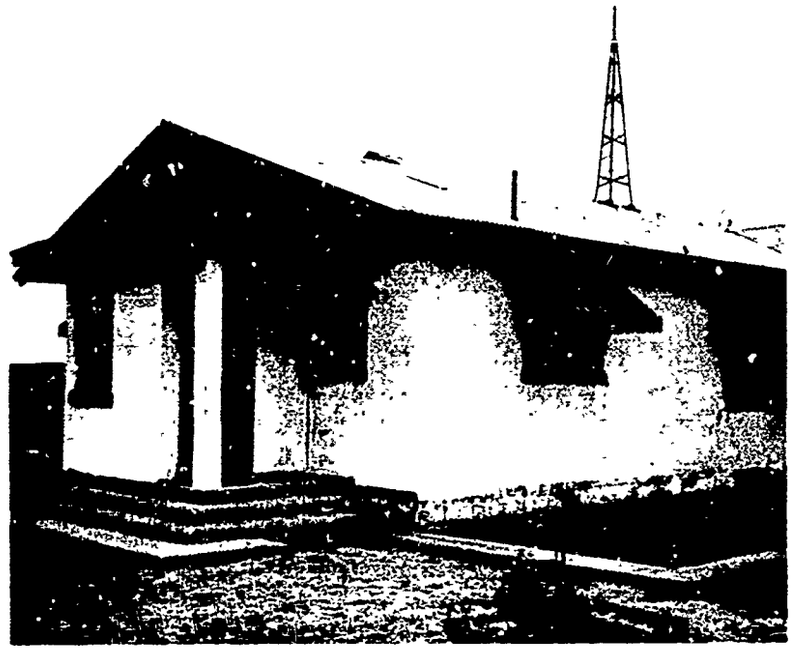


Fig. B2-3 Partial View of Exterior of Withers' Ranchhouse. Note Block Wall Construction With Evidence of Settlement.

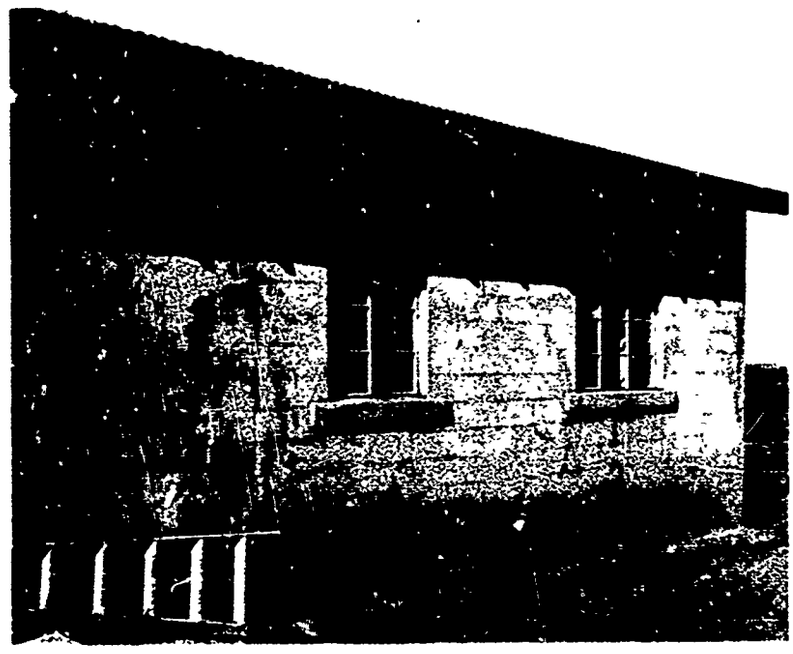
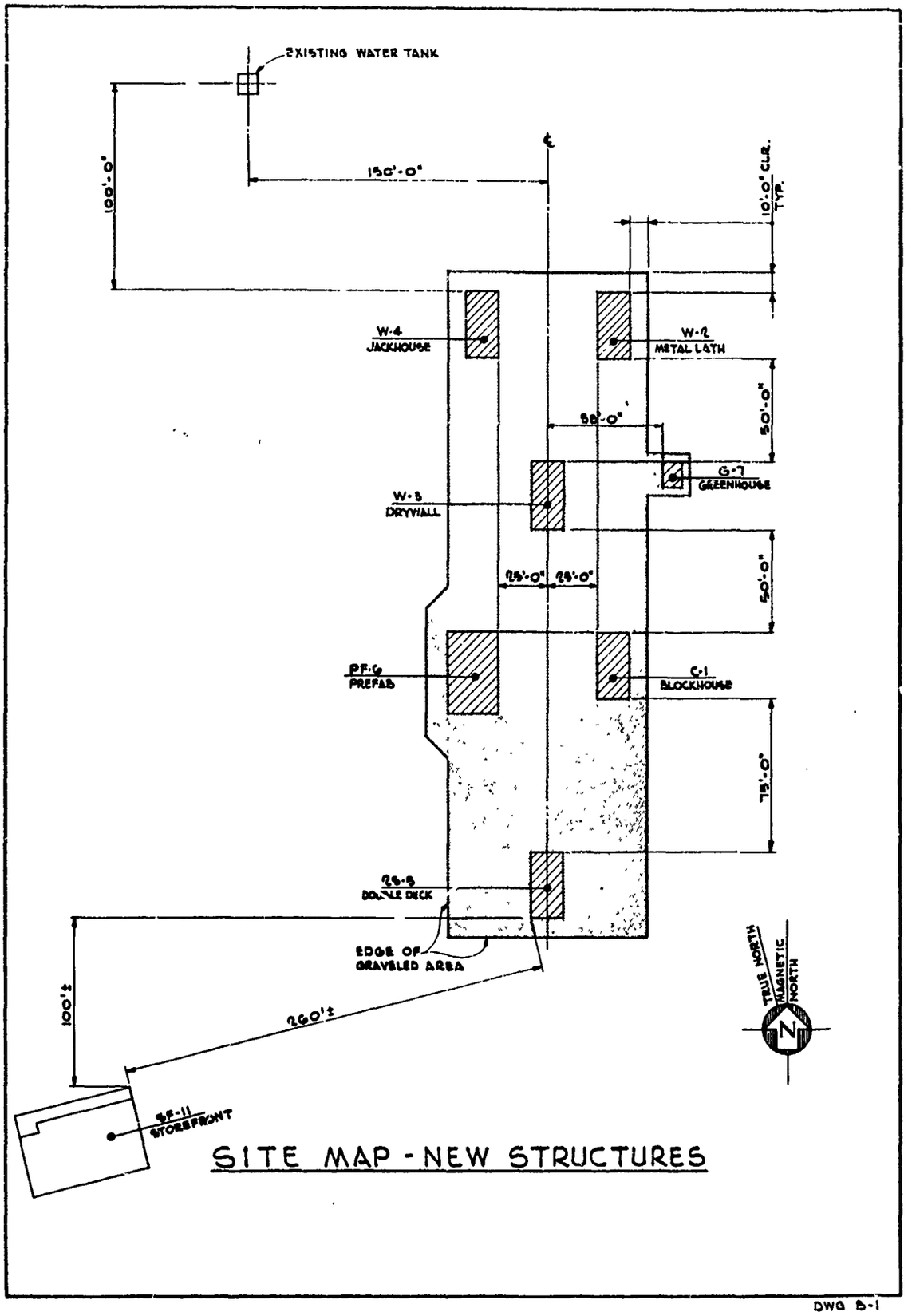
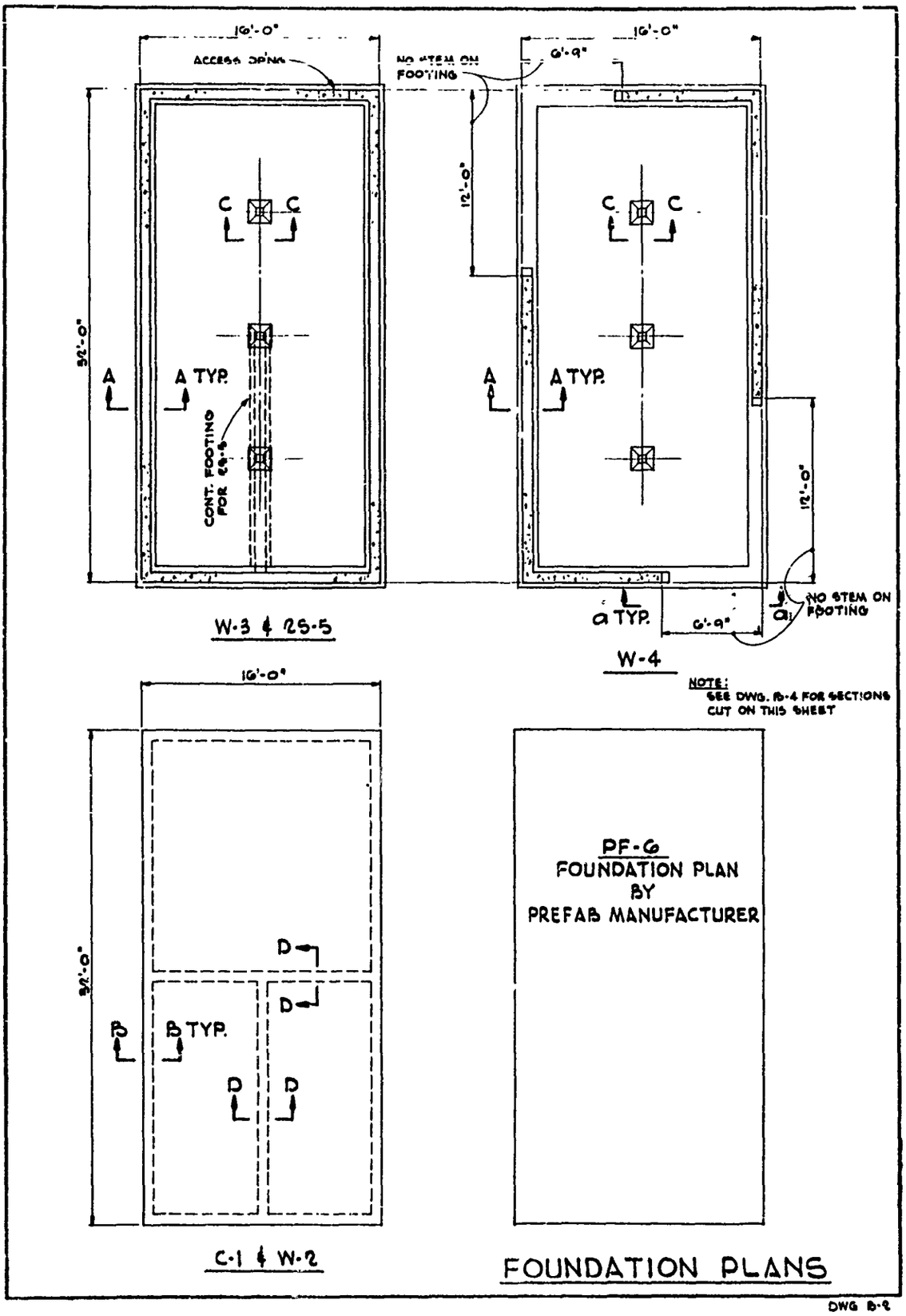


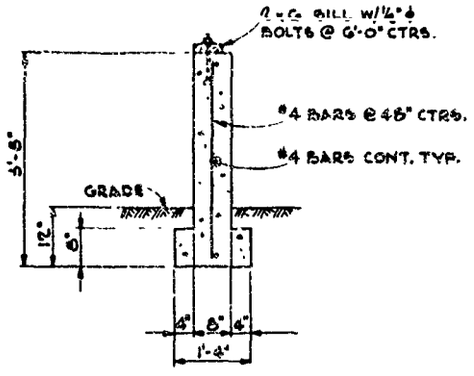
Fig. B2-4 Exterior View of Helms' Ranchhouse Showing the Older Concrete Portion to the Left With the Newer Concrete Block Addition to the Right



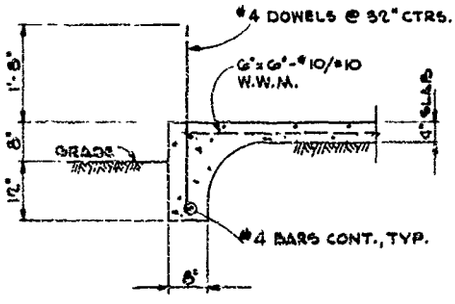
SITE MAP - NEW STRUCTURES

DWG B-1

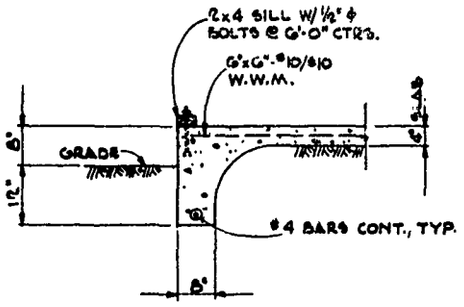

16'-0"
ACCESS OPNG
NO STEM ON FOOTING
6'-9"
16'-0"
12'-0"
32'-0"
C
C
A
A TYP.
CONT. FOOTING FOR C8-5
W-3 & C5-5
a TYP.
6'-9"
a
NO STEM ON FOOTING
W-4
NOTE:
SEE DWG. B-4 FOR SECTIONS CUT ON THIS SHEET
16'-0"
32'-0"
D
B
B TYP.
C-1 & W-2
PF-6
FOUNDATION PLAN
BY
PREFAB MANUFACTURER
FOUNDATION PLANS
DWG B-2



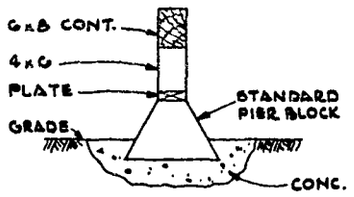
SECTION A-A



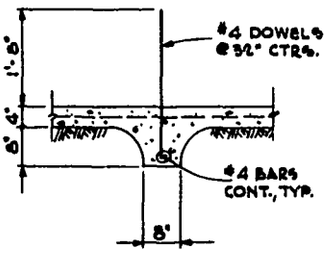
SECTION B-B FOR C-1



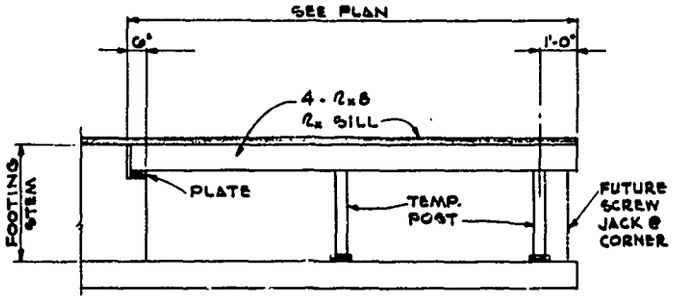
SECTION B-B FOR W-2



SECTION C-C



SECTION D-D

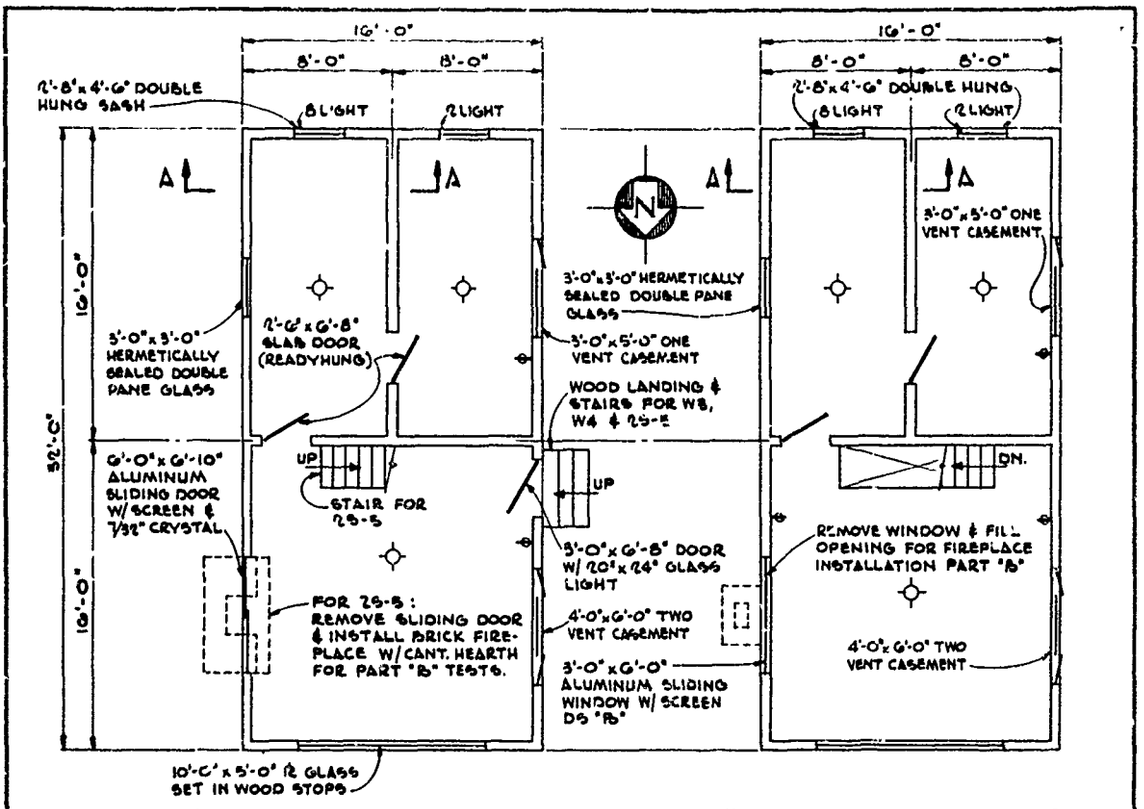


ELEVATION a-a

FOUNDATION DETAILS

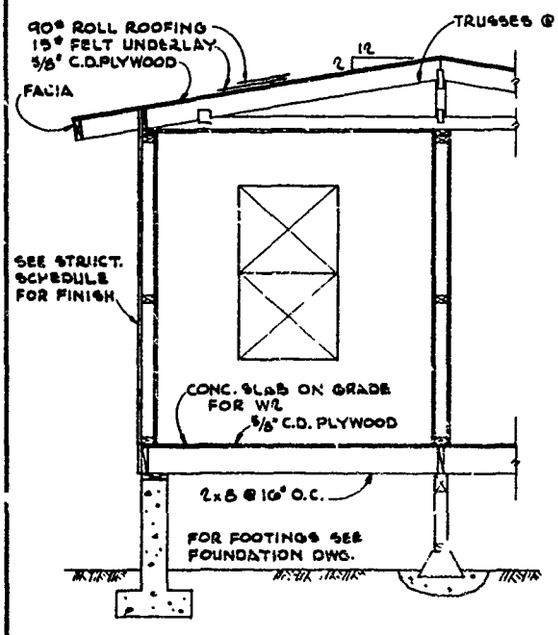
NO SCALE

DWG. B-3

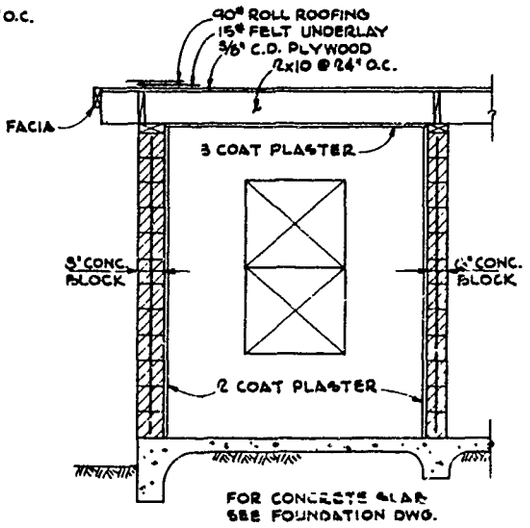


GROUND FLOOR PLAN
FOR C1, W2, W3, W4, & 25-5

2ND FLOOR PLAN FOR 25-5



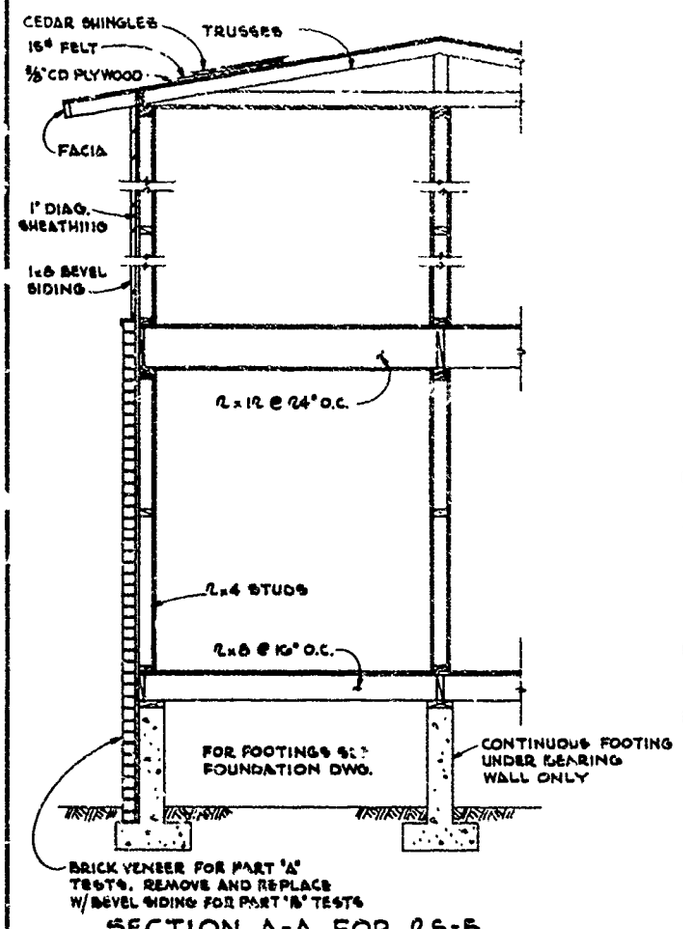
SECTION A-A FOR W2, W3 & W4



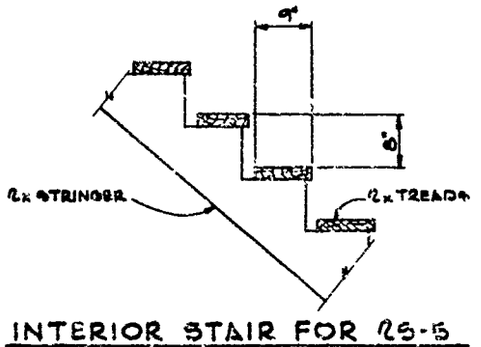
SECTION A-A FOR C1

FLOOR PLANS AND SECTIONS

DWG B-4



SECTION A-A FOR 25-5



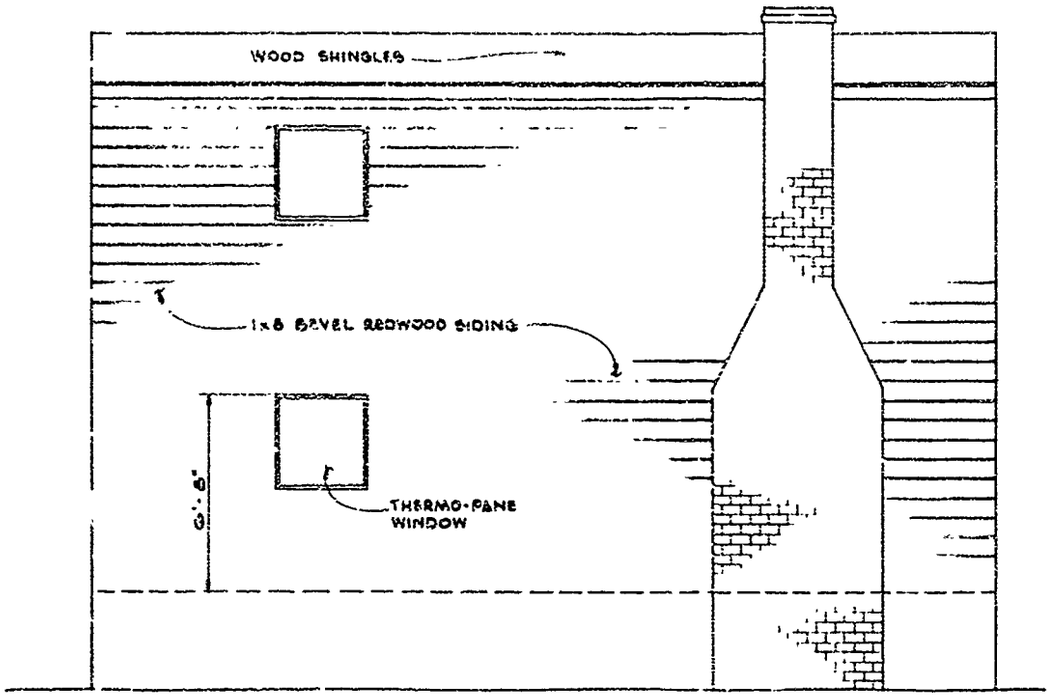
INTERIOR STAIR FOR 25-5

OUTLINE SPECIFICATIONS

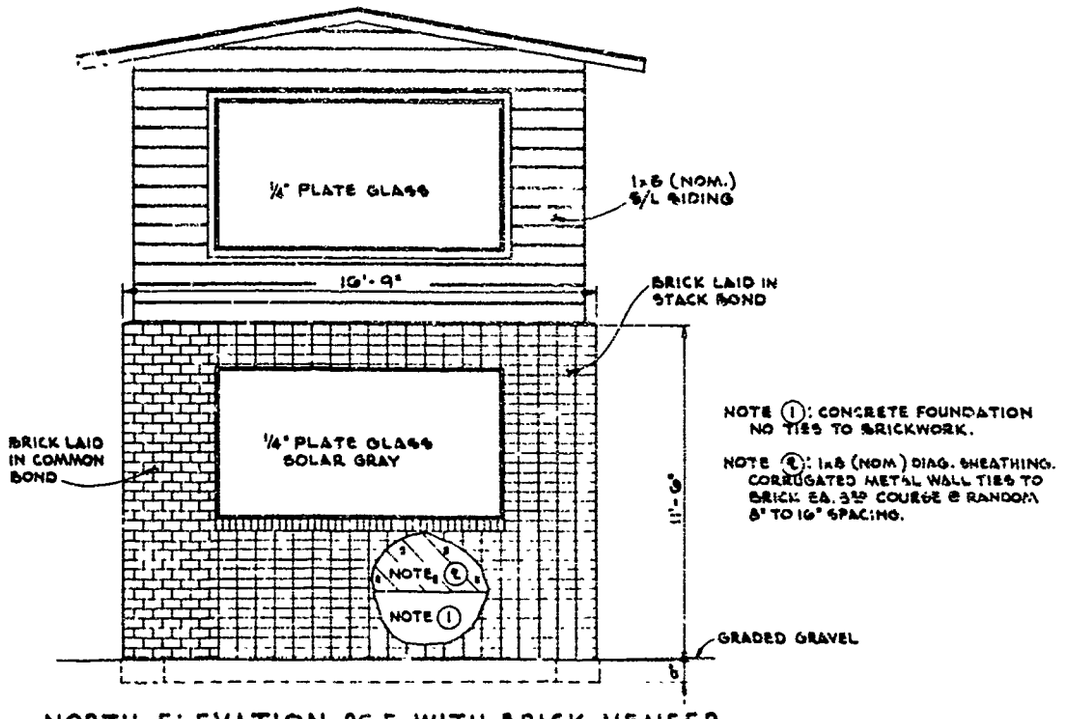
1. EXCAVATION & SITE WORK:
   CLEAR AREA OF VEGETATION AS SHOWN AND EXCAVATE FOR FOOTINGS TO FIRM SOIL AS INDICATED.
2. FOUNDATIONS:
   FORM FOOTINGS AND SLABS AS INDICATED. CONCRETE SHALL HAVE 2500 PSI STRENGTH AT 28 DAYS WITH #4 RE-BARS AS INDICATED.
3. PIERS:
   PRECAST CONCRETE PER DWGS.
4. FRAMING LUMBER:
   DOUGLAS FIR - STAND ARD OR BETTER.
5. NAILING:
   PER UNIFORM BUILDING CODE, 1958 EDITION.
6. VENTS:
   PROVIDE VENTS AND ACCESS DOOR PER UBC.
7. WALL FINISHES:
   PER SCHEDULE. EXTERIOR STUCCO PER UBC. INTERIOR PLASTER PER UBC.
8. PAINT:
   STUCCO - WASH COAT, WHITE; SIDING - SEAL & FINISH, WHITE; INT. PLASTER - ONE COAT, FLAT WHITE; DOORS - SEAL & FINISH, WHITE.
9. FLOOR:
   5/8" CD PLYWOOD ONLY, NO FINISH.
10. PLUMBING:
    NO PLUMBING REQUIRED, EXCEPT ROUGH-IN IN PFG.
11. ELECTRICAL:
    PROVIDE ONE (1) PULL CHAIN PORCELAIN LIGHT RECEPTACLE PER ROOM AND DUPLEX OUTLETS WHERE INDICATED. ROMEX WIRING - CONNECT ALL TO 60 AMP POWER POLE PROVIDED BY CONTRACTOR. 1500 WATTS/HOUSE.
12. ROOFING:
    15# FELT UNDERLAY
    90# ROLL ROOFING
    SEAL LAPS ON FLAT ROOF.
13. JACKS:
    CONTRACTOR TO PROVIDE 4 - 5 TON CAPACITY BELL BOTTOM JACK SCREWS - DUFF NORTON OR EQUAL FOR W4.

25-5 SECTION & OUTLINE SPECIFICATIONS

DWG B-5

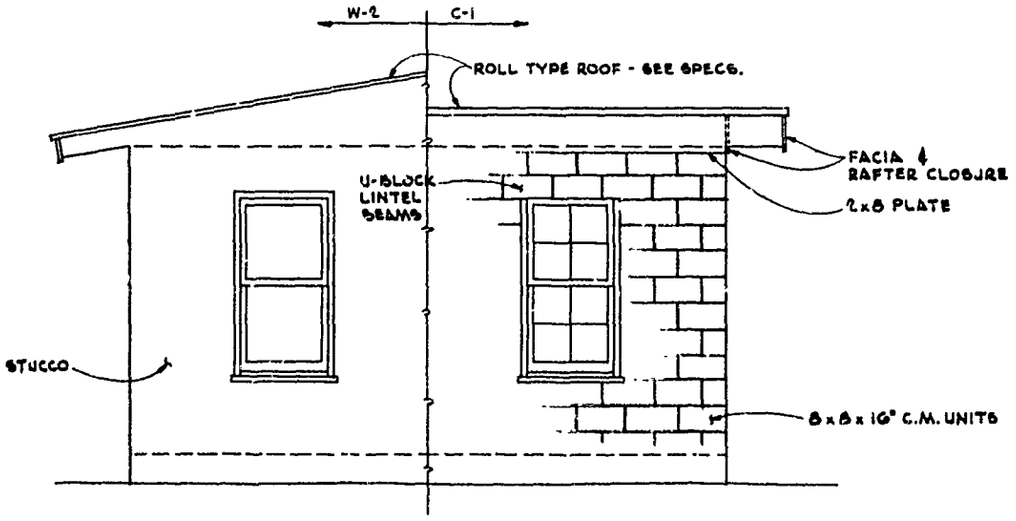


EAST ELEVATION 25-5 WITH CHIMNEY (AS USED DURING PART B)

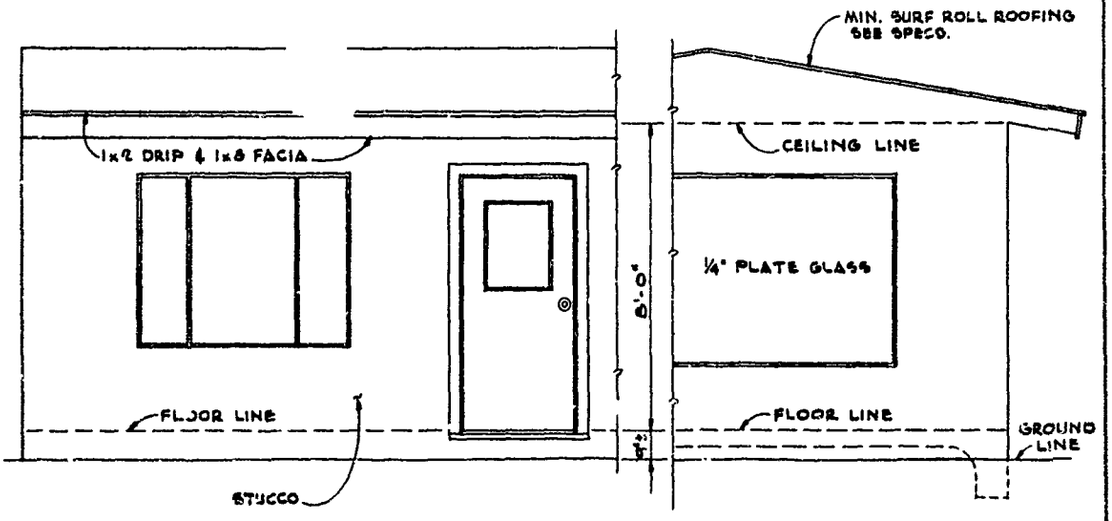


NORTH ELEVATION 25-5 WITH BRICK VENEER (PART A)

ELEVATIONS 25-5



TYPICAL SOUTH ELEV. SHOWING DOUBLE HUNG WINDOW UNITS



HALF WEST ELEV. @ ENTR. DOOR W2

HALF NORTH ELEV. W2

NOTE:
ELEVATIONS FOR W-3 AND W-4 ARE SIMILAR TO THOSE SHOWN FOR W-2. SEE SCHEDULE FOR EXTERIOR FINISH.

ELEVATIONS

DWG S-7

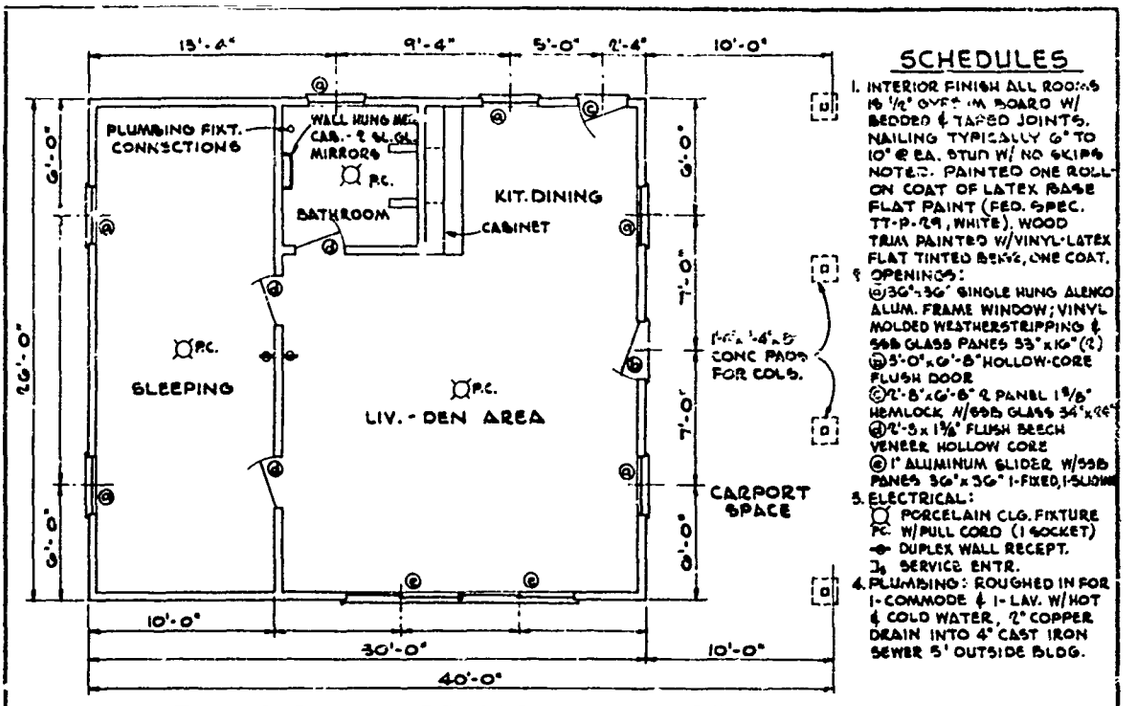
STRUCTURE SCHEDULE

STRUCTURE SCHEDULE

STRUCTURE NO.	FOUNDATION	WALLS	EXTERIOR WALL FINISH	INTERIOR WALL & CEILING FINISH	ROOF
C-1	CONCRETE SLAB ON GRADE. STEEL TROWEL FINISH	CONCRETE BLOCK 8" EXTERIOR 6" INTERIOR	PAINT ONLY	PLASTER ON BLOCK WALLS, METAL LATH AND PLASTER ON CEILING	FLAT - WOOD WITH ROLL ROOFING. 6" SL LAPS
W-2	CONCRETE SLAB ON GRADE. STEEL TROWEL FINISH	WOOD STUDS	STUCCO ON PAPER-BACKED WIRE FABRIC	METAL LATH AND PLASTER	PITCHED - WOOD WITH ROLL ROOFING
W-3	RAISED FOOTING	WOOD STUDS	STUCCO ON PAPER-BACKED WIRE FABRIC	½" SHEETROCK WITH TAPED JOINTS	PITCHED - WOOD WITH ROLL ROOFING
W-4	RAISED FOOTING WITH JACKS, SEE DETAIL	WOOD STUDS	WOOD BEVEL SIDING	PART 'A' - WOOD LATH & PLASTER PART 'B' - GYPSUM LATH & PLASTER	PITCHED - WOOD WITH CEDAR SHINGLES
29-5	RAISED FOOTING	WOOD STUDS	PART 'A' - BRICK VENEER ON FIRST FLOOR AND WOOD BEVEL SIDING ON SECOND FLOOR PART 'B' - BRICK VENEER REMOVED AND BEVEL SIDING INSTALLED	WOOD LATH AND PLASTER	PITCHED - WOOD WITH CEDAR SHINGLES
PF-6	CONCRETE SLAB ON GRADE. STEEL TROWEL FINISH	WOOD STUDS - PREFABRICATED	UNFINISHED - 5/8" CEDAR PLYWOOD	PART 'A' - ½" SHEET-ROCK W/TAPED JOINTS PART 'B' - GYPSUM LATH & PLASTER	PITCHED - WOOD WITH ASPHALT SHINGLES

NOTE:
PART 'A' - ALL INTERIOR SURFACES AND EXTERIOR STUCCO RECEIVED ONE COAT OF LATEX WHITE PAINT.
PART 'B' - ALL INTERIOR SURFACES AND EXTERIOR STUCCO RECEIVED TWO COATS OF LATEX WHITE PAINT.

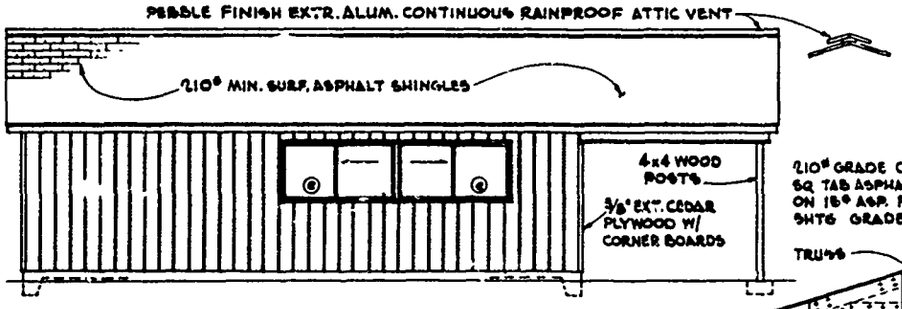
DWG B-6



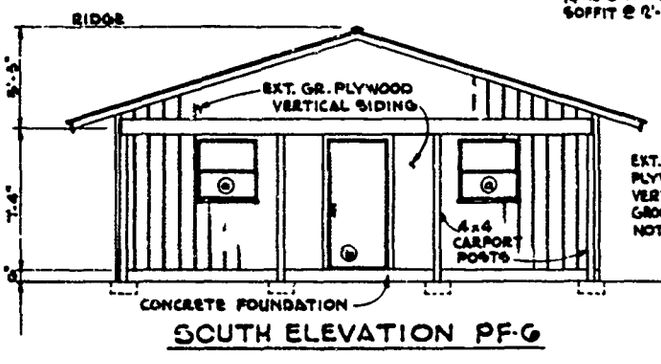
SCHEDULES

1. INTERIOR FINISH ALL ROOMS 1/2" GYPS. BD. W/ BEDDED & TAPED JOINTS, NAILING TYPICALLY 6" TO 10" @ EA. STUD W/ NO SKIPS NOTED. PAINTED ONE ROLLER COAT OF LATEX BASE FLAT PAINT (FED. SPEC. TT-P-29, WHITE), WOOD TRIM PAINTED W/ VINYL-LATEX FLAT TINTED BEIGE, ONE COAT.
2. OPENINGS:
   - (a) 36"x36" SINGLE HUNG ALENCO ALUM. FRAME WINDOW; VINYL MOLDED WEATHERSTRIPPING & SSB GLASS PANES 33"x16" (2)
   - (b) 3'-0"x6'-8" HOLLOW-CORE FLUSH DOOR
   - (c) 2'-8"x6'-8" 2 PANEL 1 3/8" HEMLOCK W/ SSB GLASS 34"x24"
   - (d) 2'-3"x1 3/8" FLUSH BEECH VENEER HOLLOW CORE
   - (e) 1" ALUMINUM SLIDER W/ SSB PANES 36"x36" 1-FIXED, 1-SLIDING
3. ELECTRICAL:
   - PORCELAIN CLG. FIXTURE
   - PC W/ PULL CORD (1 SOCKET)
   - DUPLEX WALL RECEPT.
   - SERVICE ENTR.
4. PLUMBING: ROUGHED IN FOR 1-COMMODE & 1-LAV. W/ HOT & COLD WATER, 2" COPPER DRAIN INTO 4" CAST IRON SEWER 5' OUTSIDE BLDG.

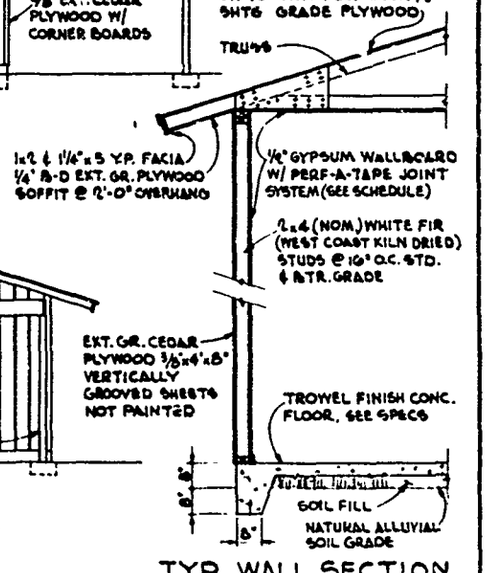
FLOOR PLAN PRE-FAB HOUSE PF-6



WEST ELEVATION PF-6



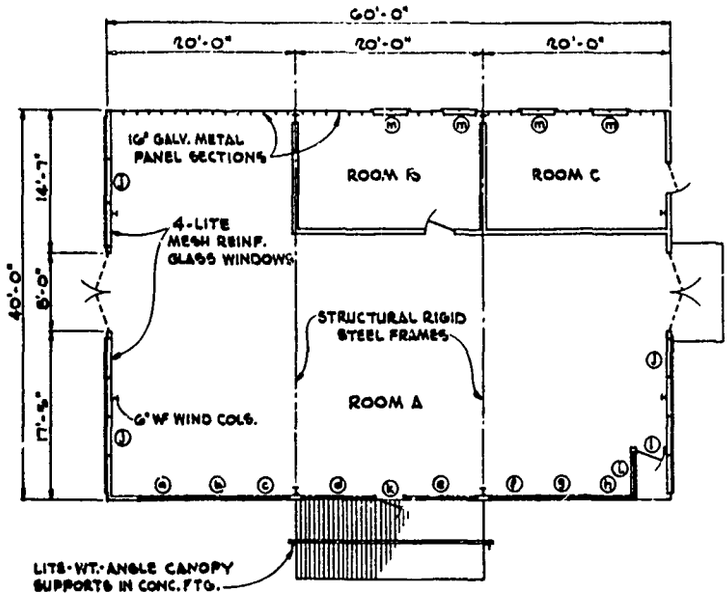
SOUTH ELEVATION PF-6



TYP. WALL SECTION

PREFAB HOUSE, PF-6

DWG B-9



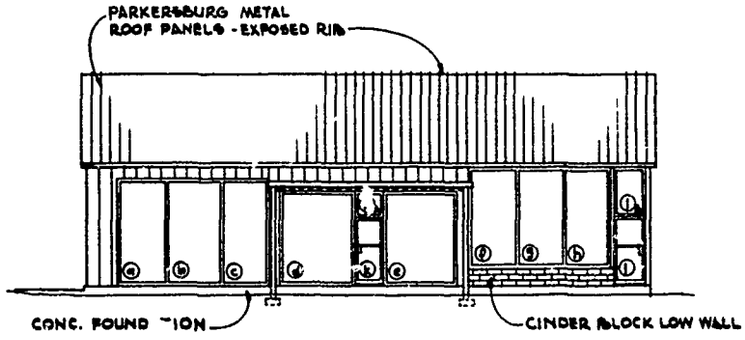
FLOOR PLAN STORE FRONT

SCHEDULES

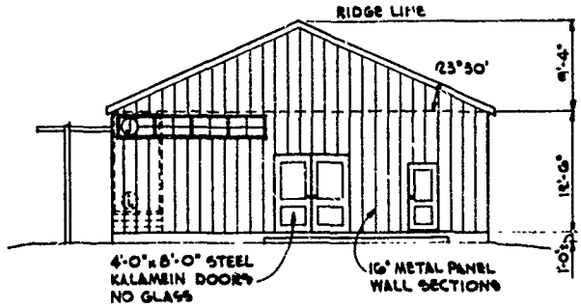
ROOM A:
1. INCANDESCENT (200 WATT) LITE BULBS IN PENDANT REFLECTORS
2. GLASS:
   - ⓐ 1/4" CLEAR PLATE
   - ⓑ 1/4" SOLEX GRAY
   - ⓒ 1/4" CLEAR PLATE
   - ⓓ do do do
   - ⓔ do do do
   - ⓕ do do do
   - ⓖ do do do
   - ⓗ do do do
   - ⓘ 5/8" do do
   - ⓙ 1/8" DS-B
   - ⓚ & ⓚA DOOR & TRANSOM (FIXED) WITH ⓙ & ⓙA 1/4" CLEAR PLATE GLASS
   - ⓜ
   - ⓝ INSULATED SECTIONAL WALL PANELS GAGE METAL OUTSIDE & 1/2" GYPSUM WALL BOARD INSIDE. ROOF PANELS SIMILAR. CEILING PANELS PERFORATED

ROOM B:
1. 8-2 TUBE FLUORESCENT FIXTURES (4') SURFACE MOUNTED
2. 2-ⓜ WINDOWS

ROOM C:
SIMILAR



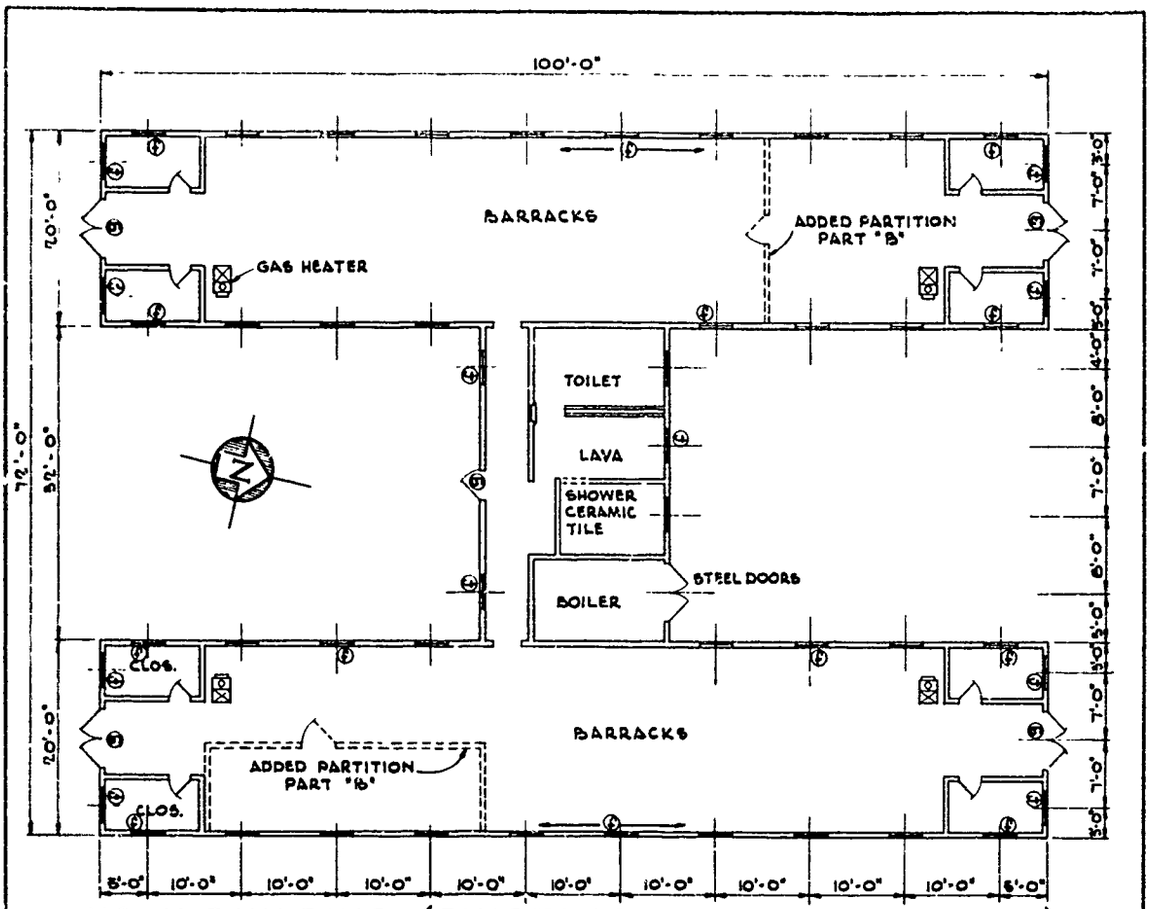
NORTH ELEVATION STORE FRONT



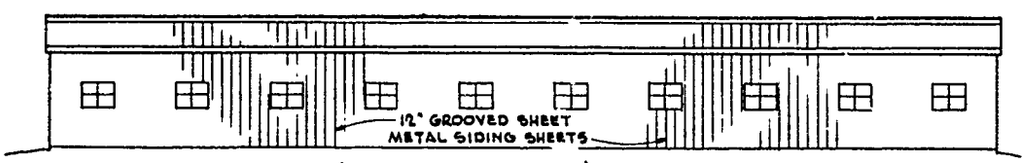
WEST ELEVATION STORE FRONT
EAST ELEVATION SIMILAR

STOREFRONT

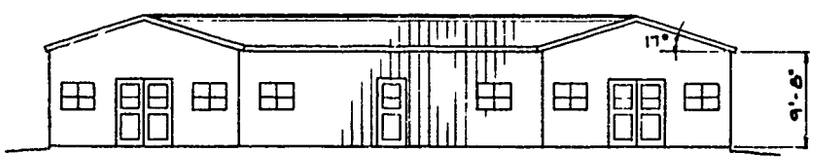
DWG B-10



H8-H BUILDING (EXISTING METAL BARRACKS)



EAST ELEVATION (WEST SIMILAR) H-8 BARRACKS BUILDING



SOUTH ELEVATION - H-8 (H BLDG.)

LITE WT. STEEL CHANNEL FRAMING, V-GR. GALV. SHEET METAL EXT. SIDING & ROOFING (SCREWED) & GYPSUM WALLBOARD INT. WALLS & CEILINGS

H-8, H BUILDING

DWG B-11

SCHEDULE OF GLAZED OPENINGS

TEST BLDG.	OPENING			INDIVIDUAL GLASS PANES							AREA IN SQ. FT.				
	MARK	SIZE	TYPE	MOUNTING	TYPE	THICKNESS NOM.	THICKNESS ACTUAL	W&H INCHES	AREA SF	NO. PANES	NORTH	EAST	SOUTH	WEST	TOTAL
C-1	A	5'-10"	PICTURE WINDOW	1⅝" WOOD FRAME 1"x1" NAILED T.D. STOP	SOLAR GREY POL PLATE	¼"	7/32"	118 x 58	47.5	1	47.5				
	B	5'-10"x6'-6"	SLIDING DOOR	1" ALUM. FRAME NEOPRENE STOPS	CRYSTAL SHEET	7/32"	3/16"	33x63	14.4	2		28.8			
	C	5'x5'	THERM-O-PANE	WOOD FRAME (1⅝") 1" NAILED WOOD STOPS	CLEAR DSB (2)	⅛"	.115	35x35	8.0	1		8.0			
	D	2'-6"x4'-6"	CONV. DBL HUNG	WOOD FRAME W/PUTTY & GLAZING CLIPS	CLEAR SSB	3/32"	.085	24x24	4	2			8		
	E	2'-6"x4'-6"	do	do do do	do	do	do	12x12	1	8			8		
	F	4'-2"x3'-2"	STEEL CASEM.	STEEL ANGLE FRAME, SPRING CLIPS & COMM. PUTTY	CLEAR DSB	⅛"	0.115	15x85 & 35x35	3.0 8.0	1 1				3.0 8.0	
	G	5'-2"x4'-2"	do	do do do	do	do	do	15x47 & 31x47	4.9 10.1	2 1				9.8 10.1	
	H	3'-0"x6'-8"	ENT. DOOR	WOOD STOPS NAILED	do	do	do	20x24	3.3	1				3.3	135.1
W-2	ALL OPENINGS SIMILAR & IDENTICAL IN ALL CHARACTERISTICS TO C1 (EXCEPT WINDOW "A" IS CLEAR PLATE)														135.1
W-3	ALL OPENINGS SIMILAR TO C1 EXCEPT FOR "F" & "G"														
	F	4'-2"x3'-2"	STEEL CASEM.	STEEL ANGLE FRAME, SPRING CLIPS & COMM. PUTTY	CLEAR DSB	⅛"	0.115	15x11	1.08	9				9.7	
	G	5'-2"x4'-8"	do	do do do	do	do	do	do	1.08	16				17.3	131.2
W-4	ALL OPENINGS SIMILAR & IDENTICAL IN ALL CHARACTERISTICS TO C1 (EXCEPT WINDOW "A" IS CLEAR PLATE)														135.1
255	1ST FLOOR OPENINGS SIMILAR & IDENTICAL TO C1														135.1
	2ND FLOOR SIMILAR EXCEPT DELETE "B" & "H" AND SUBSTITUTE FOLLOWING:														
	1	3'-0"x6'-0"	SLIDING WINDOW	ALUM. CHANNEL FRAME NEOPR.	CLEAR SSB	3/32"	.085	34x35	7.8	2	47.5	8.0 15.0	16	30.9	118.0
PFG	Ⓐ	3'-0"x3'-0"	SGL. HG. WINDOW	do do	do	do	do	33x16	3.6	12	14.4	14.4	14.4		
	Ⓒ	2'-3"x6'-8"	INT. DOOR	WOOD STOPS NAILED	do	do	do	24x34	5.6	1		5.6			
	Ⓔ	3'-0"x6'-0"	SLIDING WINDOW	ALUM. CHANNEL FRAME NEOPR.	do	do	do	35x35	8.5	4				34.0	82.6
G-7		GLASS WALL & ROOF AREA		GLASS LAID IN 2x2 REDWOOD FRAME W/ NAILS @ 2 PT'S EA. SIDE	CLEAR SSB	3/32"	.085 & .078± PROB. FOREIGN	10x32 16x24 18x24 16x16 16x12	5.5 7.6 5.0 1.8 (OR LESS)	16 24 8 20	32.4	28 3.2 (ROOF) ↓ 50.4	32.4	28 3.2 (ROOF) ↓ 50.4	227.8
H-8	Ⓕ	5'-4"x2'-8"	STEEL AWNING	STEEL ANGLE FRAME, SPR. CLIPS & PUTTY	CLEAR SSB	3/32"	.085	18x14	1.75	4 EA. WDW. x 44 WDWS.	49.0	136.0	136.0	42	393.0
	Ⓖ	3'-0"x7'-0"	DOOR	do do	do	3/16"	.182	24x15	2.5	12	6.6				
I-9	DOOR LITE & 4 WINDOWS ALL CLEAR				SSB	3/32"	.085	35x23	5.2	9	10.4	10.4		23.8	44.2
F-10	9 LITE WOOD WINDOW SASH 3'-0"x5'-0"			do	do	do	8x10	0.55	12	6.6				6.6	
SF-11	Ⓐ Ⓑ & Ⓒ	5'-3"x10'-6"	STORE GLASS	SEE FIG. 81-19	Ⓐ Ⓒ CLR PLATE; Ⓑ SOLAR GRAY	¼"	13/64"	61x127	54.8	3	164.4				
	Ⓓ & Ⓔ	7'-6"x10'-6"	do	do do	do	do	do	90x117	73.1	2	146.2				
	Ⓕ, Ⓖ, Ⓗ, Ⓘ, Ⓙ & Ⓚ	5'-0"x9'-6"	do	do do	do	7/32" do	do	60x115	47.5	4	190.2				
	Ⓚ, Ⓛ	3'-0"x7'-0"	DOORS	ALUM. MEDIUM STYLE-T5 ALLOY	do	do	do	31x75	16.1	2	32.2				736.0
	Ⓚ, Ⓛ	3'-0"x4'-0"	TRANSOM		do	do	do	31x44	9.4	2	18.8				
	Ⓛ Ⓜ	5'-10"x2'-0"		STEEL ANGLE FRAME SPR. CLIPS & PUTTY	DSB do	⅛"	0.115	21x15 do	2.2 do	46 30		61.6	66.0	56.6	
0-12	2 DOOR LITES & 9 WINDOWS ALL CLEAR				SSB	3/32"	.085	24x42	7.0	9	7.0	24.5	7.0	24.5	63.0

SCHEDULE OF GLAZED OPENINGS

DWG A-12

APPENDIX C - INSTRUMENTATION

1. General

Instrumentation for the project was provided by three experienced firms in the field of data acquisition: DATACRAFT, INC.; THE BOEING COMPANY; and LOCKHEED - CALIFORNIA COMPANY. The first of these was under subcontract with Blume and the latter two were under contract with FAA, but all technical direction was Blume's responsibility. Lockheed participated in the maneuver phase only and their equipment is discussed in Chapter VII.

The data acquisition systems used during the test were: (a) Near-Field Overpressure; (b) Far-Field Overpressure; (c) Mechanical Displacement-Structural; (d) Mechanical Displacement-Glass; (e) Mechanical Vibration System; (f) Mechanical Strain-Glass; (g) Mechanical Strain-Plaster; (h) Timing System; (i) Temperature Measurement System; (j) Scratch Gages; and (k) Sprengnether Recorders.

2. Description of Data Systems

a. Near Field Overpressure System

(1) Datacraft provided a total of eighteen (18) channels of near field overpressure data during the test program. A block diagram of their system is

shown in Fig. C-1. The microphone pickups were placed at various specific locations within the immediate test site with the data recorded on magnetic tape and oscillographs. The frequency response of the microphones when used with signal conditioners ranged from 0.5 cps to 10 kc. Magnetic tape recorders were capable of recording this response over the entire range while the oscillographs were limited by the use of 0-3000 cps galvanometers.

(2) Boeing provided a near field overpressure system consisting of six (6) pressure transducers, six (6) signal conditioning networks and one (1) direct-write multichannel oscillograph (Fig. C-2). All components, except the transducers, are unmodified commercial equipment. The condenser microphones (Altec Lansing 21BR and Photocon Research Products 404) were modified to respond to approximately 0.5 cps by critically controlling "air-venting" across the microphone diaphragm.

The electrical response of the measurement system was essentially uniform from DC to 2,500 cps. The upper frequency limitation was determined by the recording galvanometer (CEC Model 7-362). The low frequency response below 20 cps was controlled by

the back venting of the microphone diaphragm. The acoustic calibration of the microphone from 10 cps to 5 KC was done in a pressure coupler using a certified Western Electric Model 640AA as a reference microphone. The back venting on each microphone was then adjusted to obtain the best compromise between good low frequency response below 10 cps and fast recovery time from static pressure variations. The back venting adjustment was done in a low frequency pistonphone which was referenced to the 640AA standard microphone at 10 cps. The acoustic calibrator used for field calibration was also calibrated using the 640AA microphone.

b. Far Field Overpressure System

The system consisted of two mobile tape recorders provided by Datacraft. The block diagram of this system is shown in Fig. C-3. Recordings were made at various far field locations such as Withers Ranch, Phillips, etc., on the 1/4 inch magnetic tape and later transcribed at the Datacraft office to oscillograph form for analysis.

c. Mechanical Displacement System - Structural

The system consisted of twelve (12) transducers

placed at various points on the structures. The transducers used were actually velocity pickups with an integrating amplifier as shown by the block diagram (Fig. C-4). All data was recorded on oscillograph by Datacraft.

d. Mechanical Displacement System - Glass

The system consisted of five (5) linear potentiometer transducers mounted as a group on various windows to record the response movement of the window during the sonic boom. The block diagram (Fig. C-5) illustrates Datacraft's equipment arrangements. Window arrangements are shown in Figs. III-12 and C-11.

e. Mechanical Vibration System (Acceleration)

With this system twelve (12) channels of acceleration data were recorded during the program. Location of accelerometers were changed as required for proper test coverage. Accelerometers were mounted generally on walls; however, in several instances they were mounted on the 5' x 10' plate glass windows. A block diagram is shown in Fig. C-6. During Part B of the test program certain changes were made to eliminate the loss of response

caused by varying temperatures at the test site. The changes included installation of heater jackets on the accelerometers as shown by Fig. C-7.

f. Mechanical Strain - Glass

Thirty (30) channels of strain gage information were recorded from ten (10) rosette type gages located on windows in C-1 and W-2. A photo of the strain gage is shown earlier in Chapter III, Fig. III-14. A block diagram of the system is shown in Fig. C-8.

g. Mechanical Strain - Plaster

Eighteen (18) channels of strain gage information were recorded from six (6) rosette type gages located variously throughout the test structures. A block diagram is shown in Fig. C-9.

h. Timing System

Datacraft utilized a 100 cps timing signal of 0.5 volts amplitude which was taken from the oscillator and fed into the remote control panel. Within the panel the signal leads were wired to a spring loaded switch which permitted the timing signal to be shorted out during each run thereby removing the

timing from all recorders simultaneously. This removal of timing served as a common event marker on the various recorders. A block diagram of the system is shown in Fig. C-10.

i. Temperature Measurement System

Datacraft recorded fourteen (14) channels of temperatures at locations determined by Blume personnel. The system consisted of a Leeds and Northrup Speedomax Type G, 16 point, Temperature Recorder and 14 copper constantan (T) thermocouples.

j. Scratch Gages

These gages were built on the job at various locations to record the displacement of specific walls and windows and the ceiling in PF-6. A typical scratch gage appears in Chapter III, Fig. II-11.

k. Sprengnether Recorders

Four (4) of these recorders were utilized to record the displacement in three orthogonal directions - vertical, longitudinal and transverse. These displacement meters had magnification factors of 50 and 65 and were placed so that their longitudinal axis was parallel to the north-south axis of the

test site.

3. Total Probable Error for the Systems

As a part of their report, Datacraft analysed the systems for probable errors. The analysis together with the calibration information serve as a guide for evaluating the data:

Overpressure Systems

Ampex Tape Recorder	+3.1db -- -4. 5db
CEC Tape Recorder	+3.2db -- -4. 3db
Oscillographs	+3.1db -- -4. 3db
Far Fields	+3.1db -- -4. 5db

Mechanical Displacement - Structural

±6.16%

Mechanical Vibration (Acceleration)

Original System	±5.24%
Heater Jacket System	±5.43%

Mechanical Displacement - Windows

0.50 inch Calibration	±3.56%
0.25 inch Calibration	±3.65%

Mechanical Strain - Glass

±4.27%

Mechanical Strain - Plaster

±3.87%

4. Instrument Locations

Figs. C-11 through C-50 show the instrument locations during the test program. For diagrammatic purposes the Datacraft instrument pickups utilize the following code:

M = Microphone location (Overpressure)

V = Displacement (Velocity transducers)

A = Accelerometer (Acceleration)

R = Rosette (Strain gages)

T = Temperature

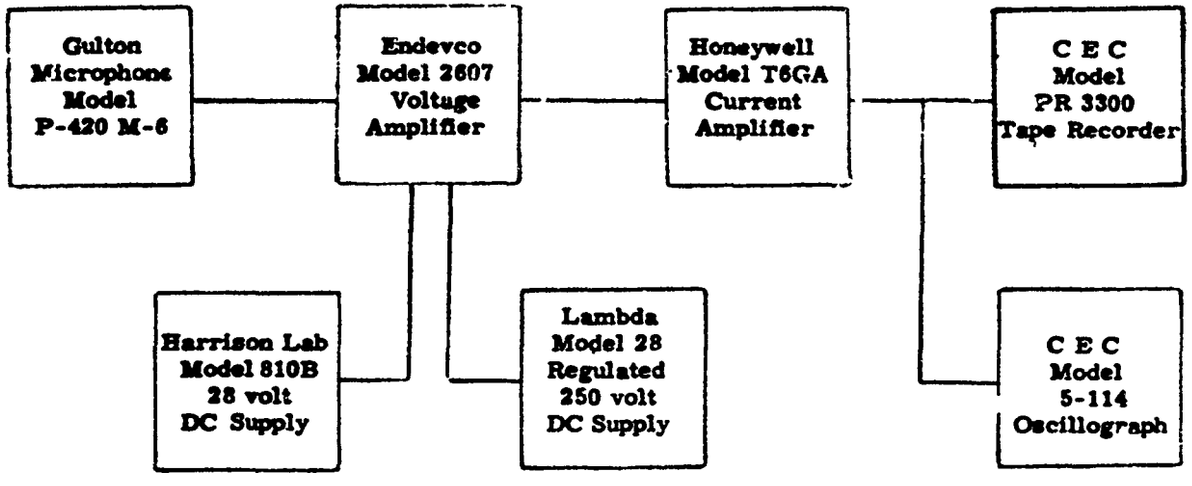


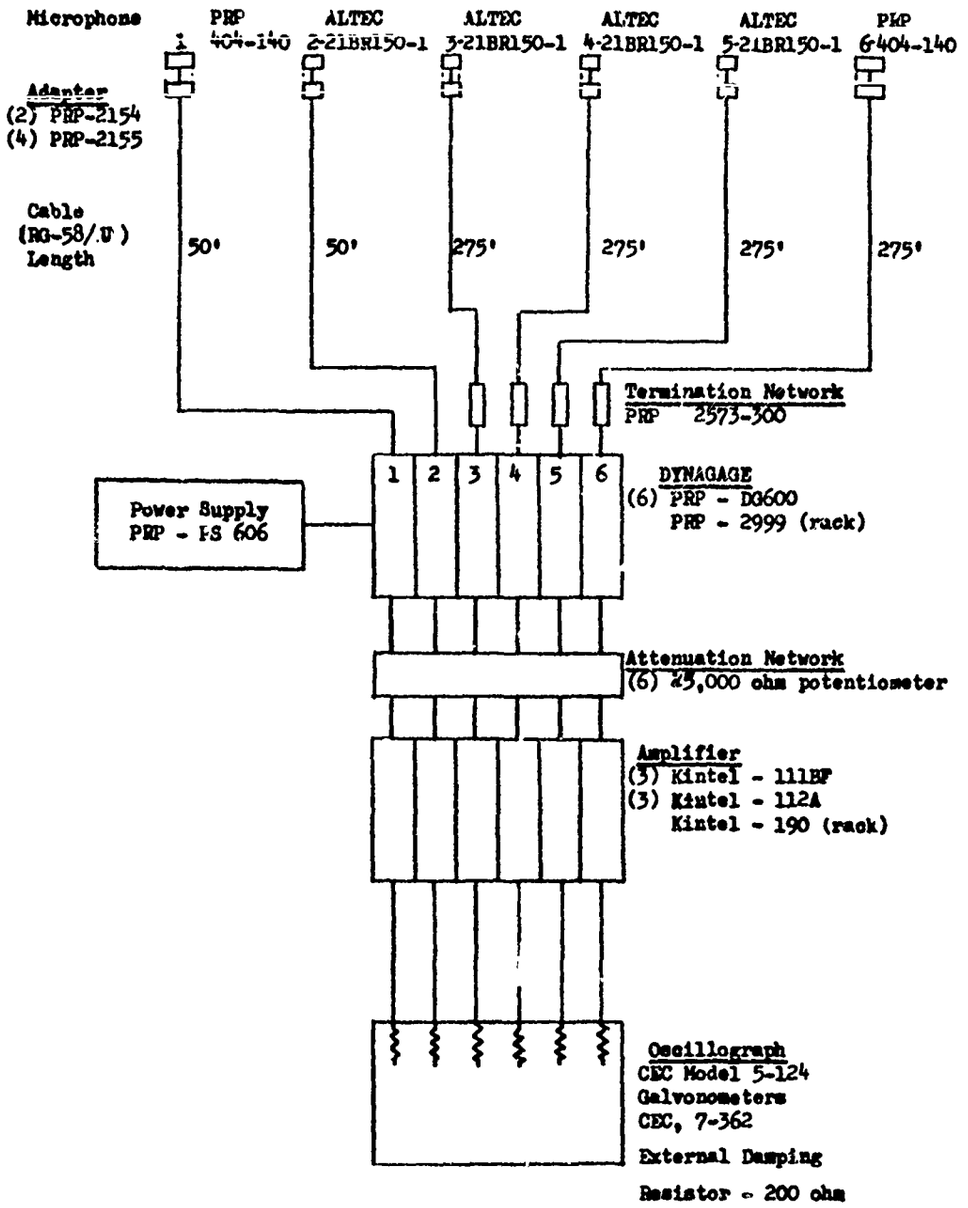
FIG. C-1

DATACRAFT INC

DRAWN	SCALE	REVISIONS	DATE
CHECKED			
APPROVED			
DATE 11-22-64			

TITLE BLOCK DIAGRAM
TYPICAL OVERPRESSURE CHANNEL

NO. ~~Fig. 1~~



PRP - Photocon Research Products Co.
CEC - Consolidated Electrodynamics Corporation

ENGR	REVISED	DATE	BLOCK DIAGRAM OF MEASUREMENT SYSTEM	~~FIG. 1~~
CHECK				D6-17485
APR			THE BOEING COMPANY	
APR			RENTON WASHINGTON	~~Page 12~~

TD 1012 R6

FIG. C-2

6 7800

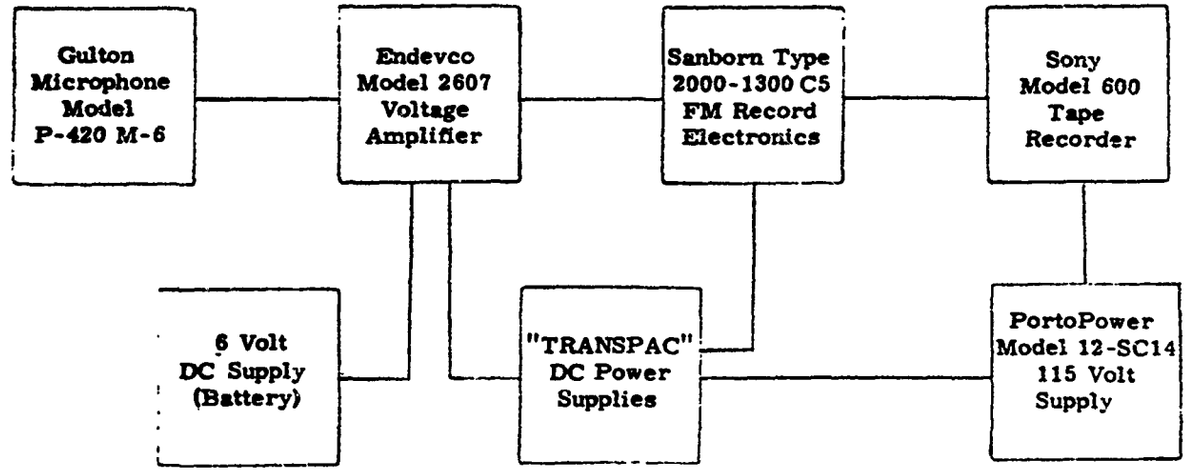


FIG. C-3

DATACRAFT INC.

DRAWN R. White	SCALE	REVISIONS	DATE
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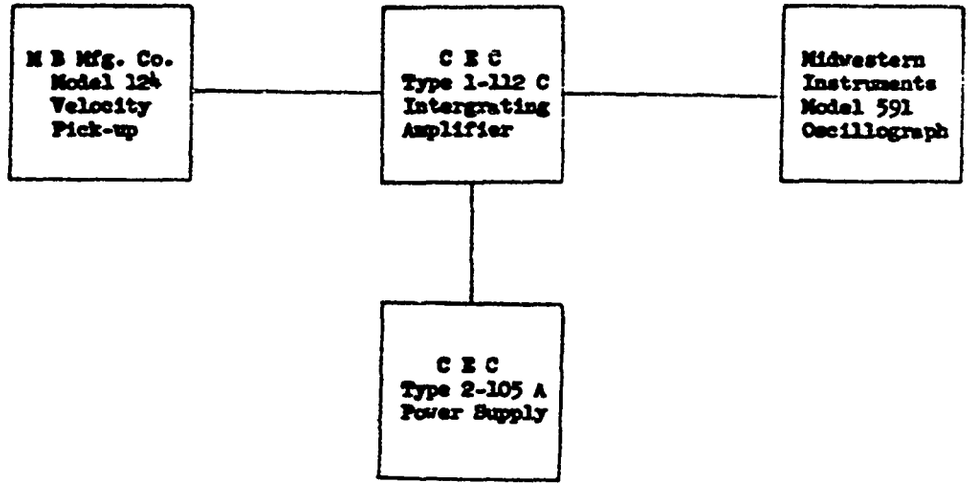
APPROVED			
DATE 11-22-64			

TITLE BLOCK DIAGRAM
FAR FIELD OVERPRESSURE SYSTEM

NO ~~Fig. 2~~



DATACRAFT INC.

DRAWN R. White	SCALE none	REVISIONS	DATE
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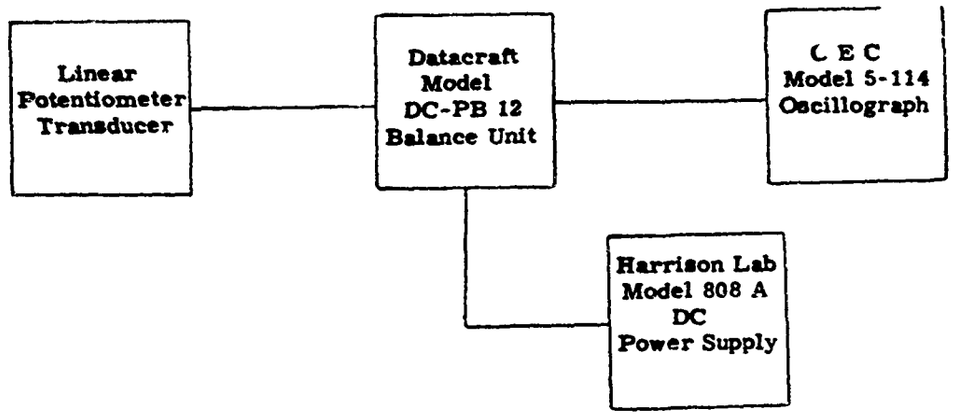
APPROVED			
DATE 11-22-64			

TITLE BLOCK DIAGRAM
MECHANICAL DISPLACEMENT SYSTEM

NO. ~~Fig 8~~

FIG. C-4



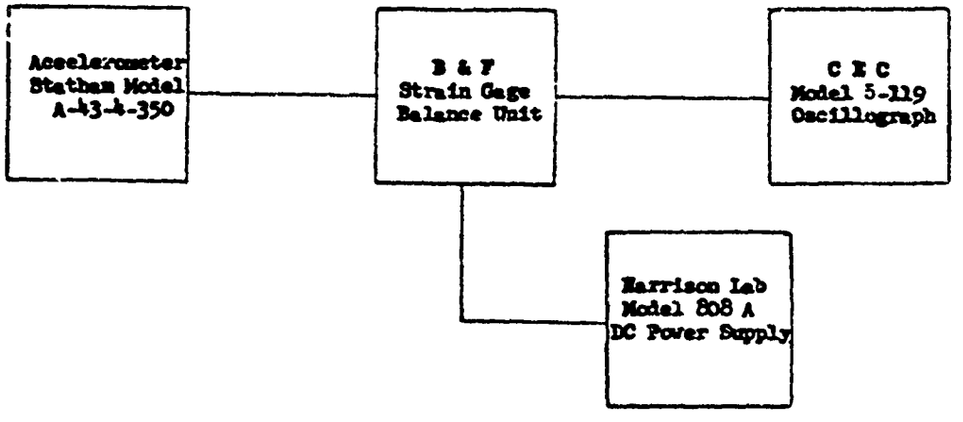
DATACRAFT INC.

DRAWN R. White	SCALE none	REVISIONS	DATE
CHECKED			
APPROVED			
DATE 1-30-65			

TITLE BLOCK DIAGRAM MECHANICAL DISPLACEMENT (windows)

NO. ~~Fig. 4~~

FIG. C-5



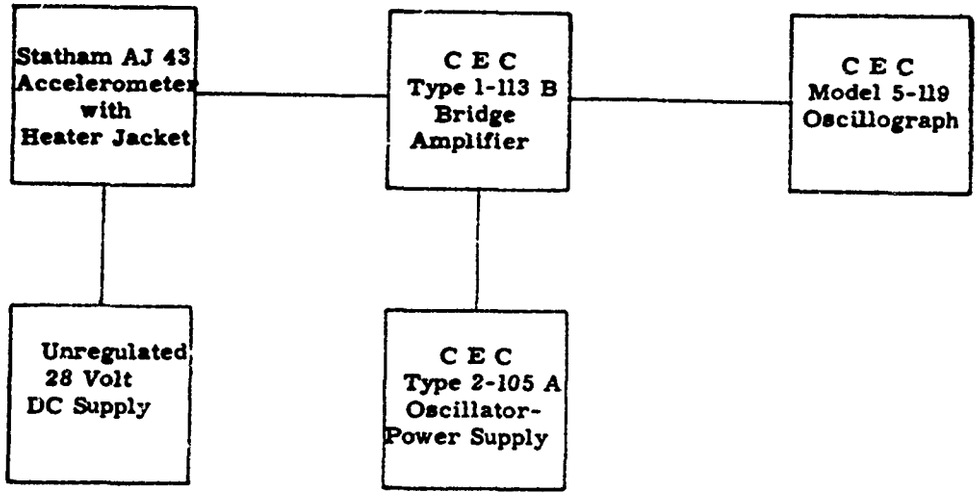
DATACRAFT INC.

DRAWN R. White	SCALE none	REVISIONS	DATE
CHECKED			
APPROVED			
DATE 11-22-64			

TITLE: BLOCK DIAGRAM ACCELEROMETER SYSTEM

NO. ~~Fig 6~~

FIG. C-6



DATACRAFT INC.

DRAWN R. White	SCALE none	REVISIONS	DATE
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APPROVED			
DATE 1-29-65			

TITLE BLOCK DIAGRAM
ACCELEROMETER SYSTEM

NO. ~~Fig 6~~

FIG. C-7

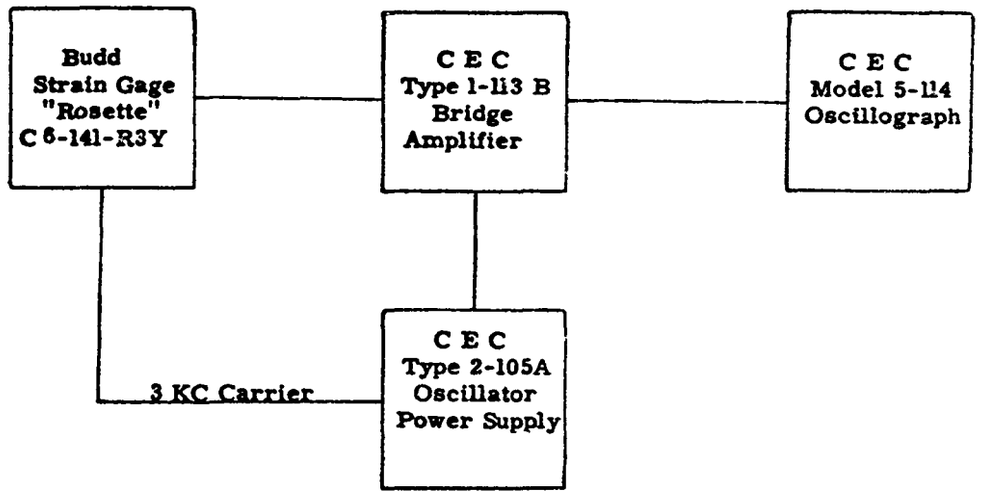


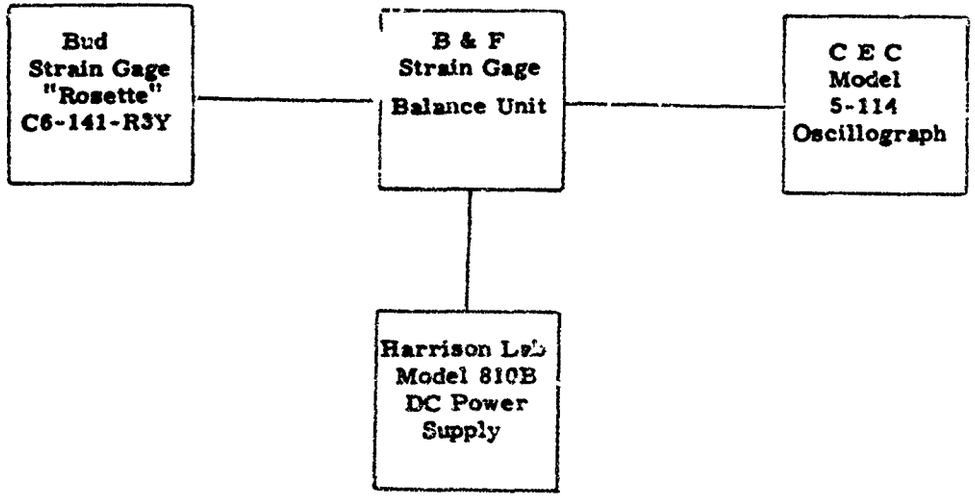
FIG. C-8

DATACRAFT INC.

DRAWN R. White	SCALE none	REVISIONS	DATE
CHECKED RH			
APPROVED			
DATE 11-22-64			

TITLE BLOCK DIAGRAM
MECHANICAL STRAIN, GLASS

NO ~~Fig 17~~



DATACRAFT INC.

DRAWN R. White	SCALE	REVISIONS	DATE
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APPROVED			
DATE 11-22-64			

TITLE: BLOCK DIAGRAM
MECHANICAL STRAIN, PLASTER

NO. ~~Fig. 9~~

FIG. C-9

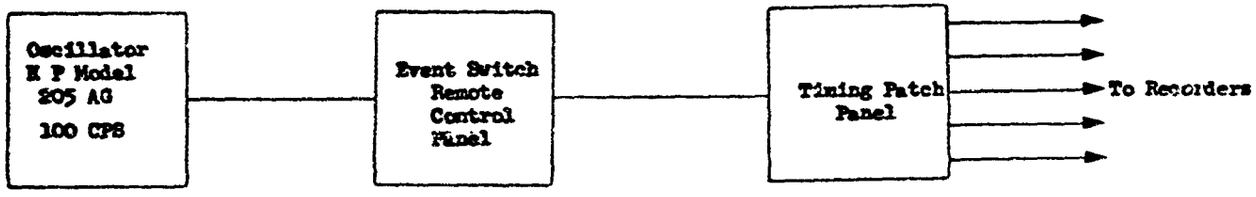

FIG. C-10

DATACRAFT INC.

DRAWN R. White	SCALE none	REVISIONS	DATE
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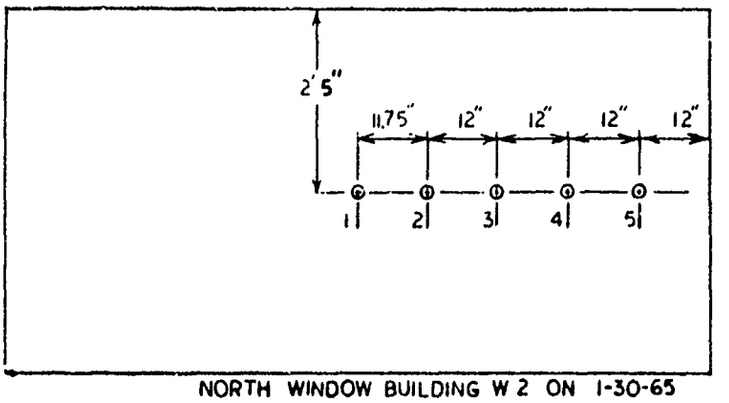
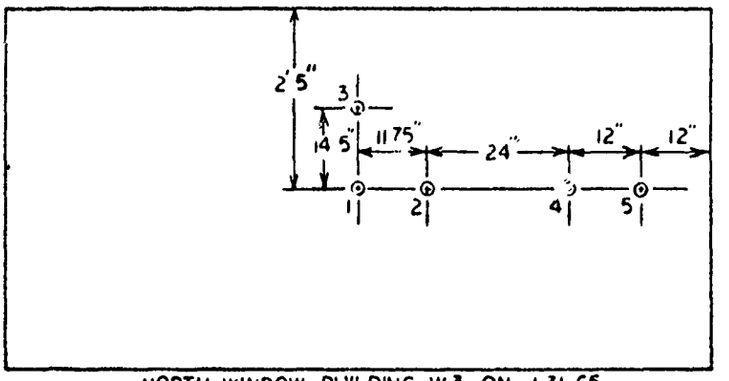
APPROVED			
DATE 11-15-65			

TITLE: BLOCK DIAGRAM TIMING CIRCUIT

NO. ~~Fig 8~~

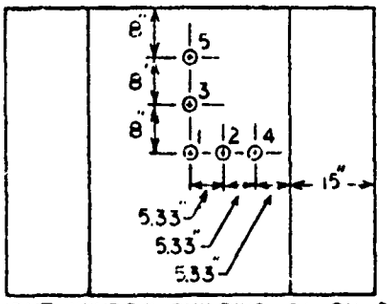


NORTH WINDOW BUILDING W 2 ON 1-30-65



NORTH WINDOW BUILDING W 3 ON 1-31-65
NORTH WINDOW BUILDING C 1 ON 1-2-65 AND 2-2-65

2-1



CASEMENT WINDOW BUILDING C 1 ON 2-3-65 THROUGH 2-6-65

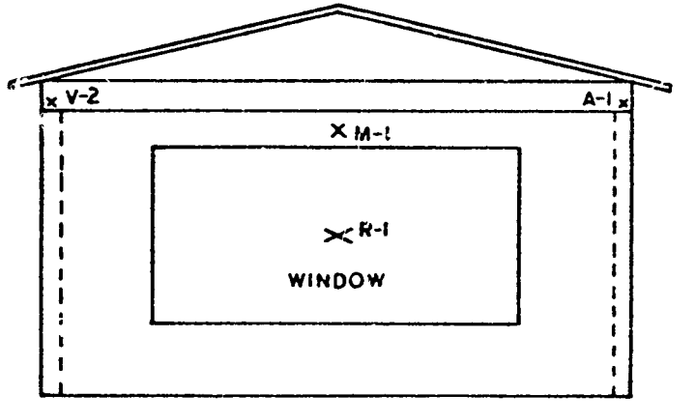
FIG. C-11

DATACRAFT INC.

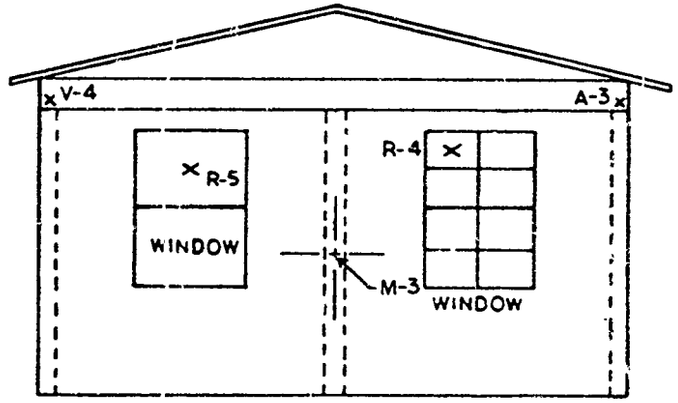
DRAWN R. WHITE	SCALE 1/4" = 1'0"	REVISIONS	DATE
CHECKED			
APPROVED			
DATE 2-27-65			

TITLE POTENTIOMETER LOCATIONS

NO ~~FIG 4~~



NORTH WALL



SOUTH WALL

W 4

FIG. C-12

DATACRAFT INC.			
DRAWN R. WHITE	SCALE NONE	REVISIONS	DAT.
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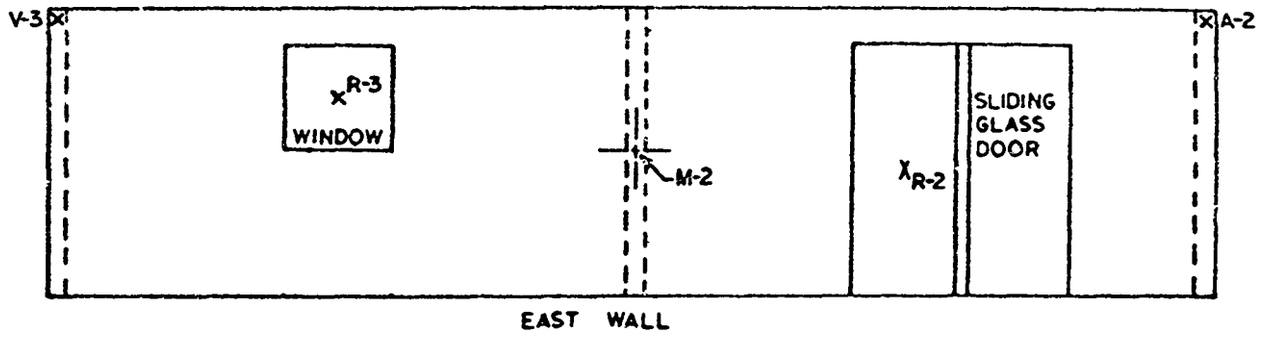
APPROVED			
DATE 11-22-64			
TITLE INSTRUMENT LOCATIONS		NO. ~~FIG. 7~~	



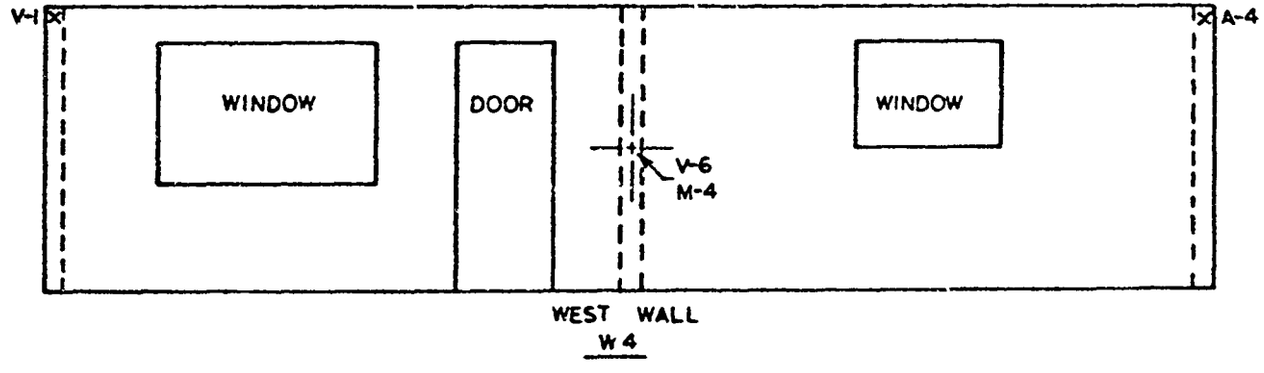


FIG. C-13

DATACRAFT INC.			
DRAWN R. WHITE	SCALE NONE	REVISIONS	DATE
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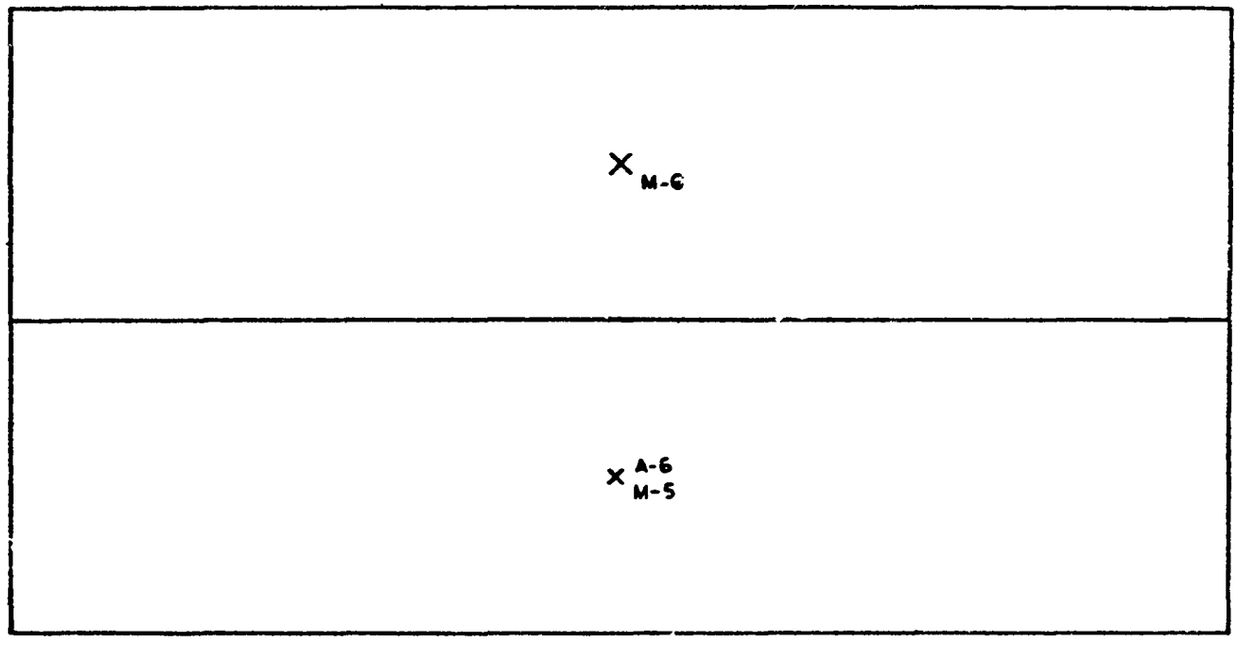
APPROVED			
DATE 11-22-64			
TITLE INSTRUMENT LOCATIONS		NO ~~FIG. C~~	



ROOF TOP
W 4

DATACRAFT INC.			
DRAWN R. WHITE	SCALE NONE	REVISIONS	DATE
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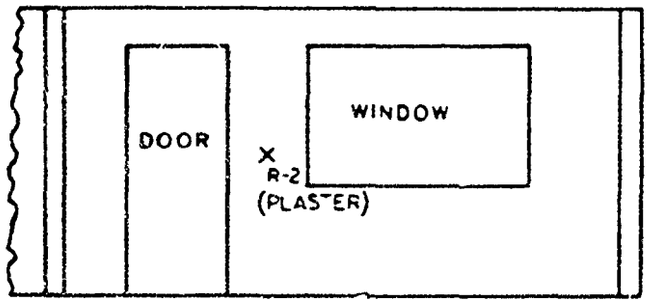
APPROVED			
DATE 11-22-64			
TITLE INSTRUMENT LOCATIONS		NO. ~~FIG. 9~~	

FIG. C-14



WEST WALL LIVINGROOM

W 4

FIG. C-15

DATACRAFT INC			
DRAWN R. WHITE	SCALE NONE	REVISIONS	DATE
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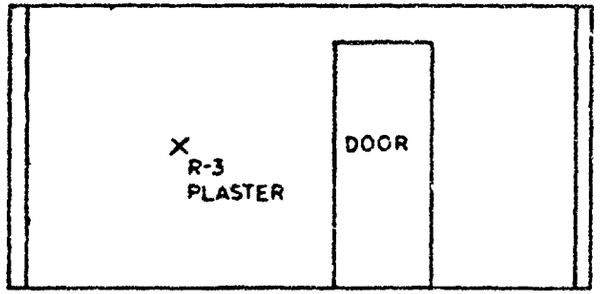
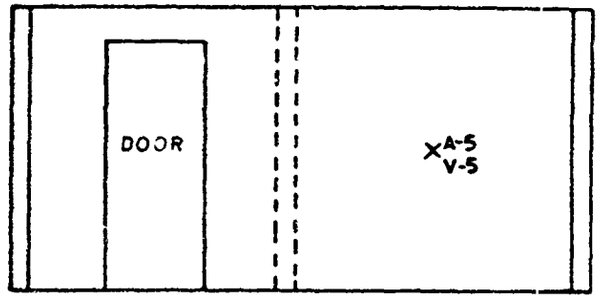
APPROVED			
DATE 11-22-64			
TITLE INSTRUMENT LOCATIONS		NO ~~FIG. 10~~	



WEST WALL BEDROOM NO. 1



SOUTH WALL LIVINGROOM

W 4

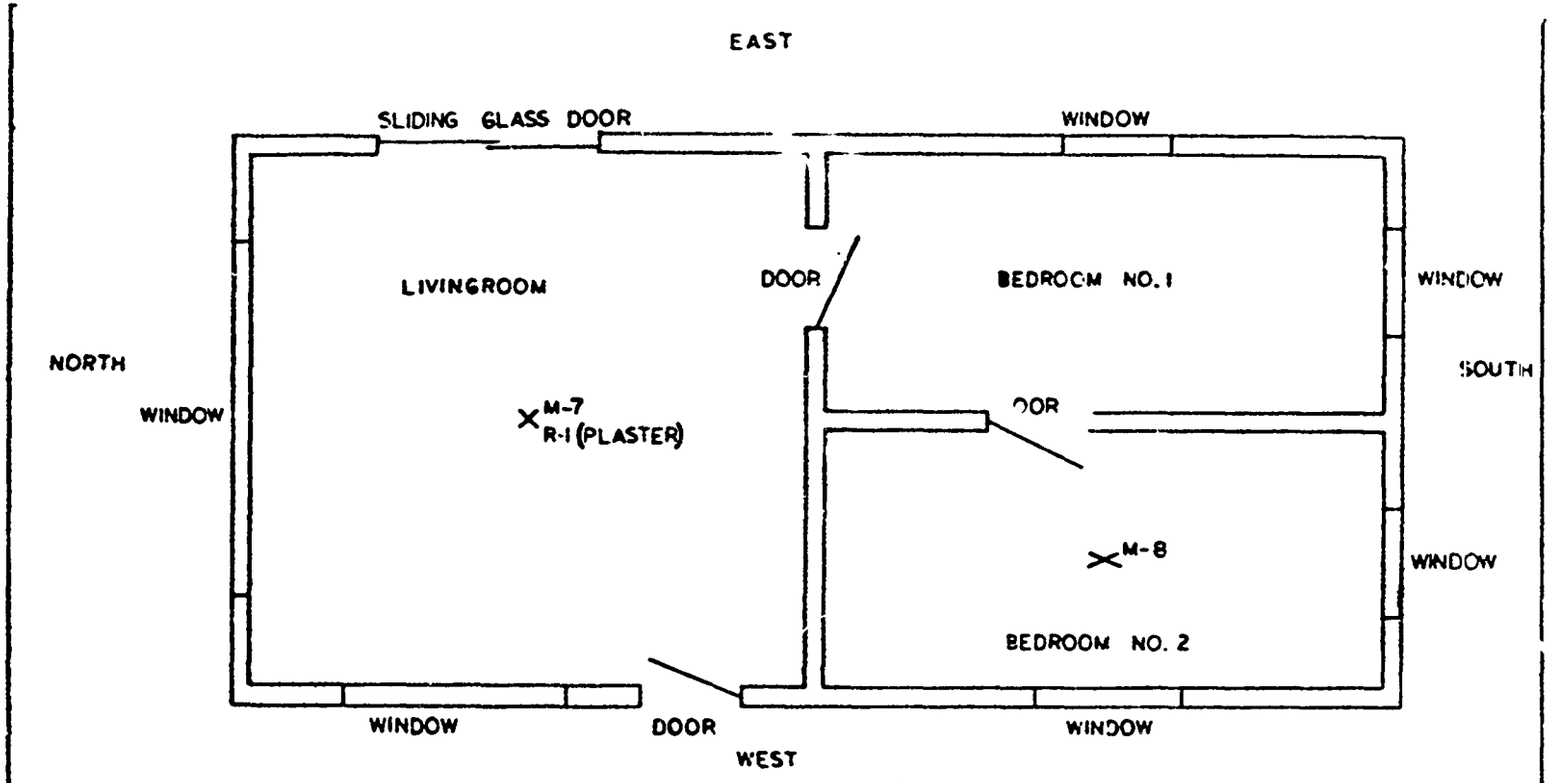
FIG. C-16

DATACRAFT INC.

DRAWN R. WHITE	SCALE NONE	REVISIONS	DATE
CHECKED R.R.			
APPROVED			
DATE 11-22-6~~4~~			

TITLE INSTRUMENT LOCATIONS

NO ~~FIG. 14~~



NOTE: MIKES 4' OFF FLOOR
ROSETTE STRAIN GUAGE R-1
LOCATED ON PLASTER CEILING

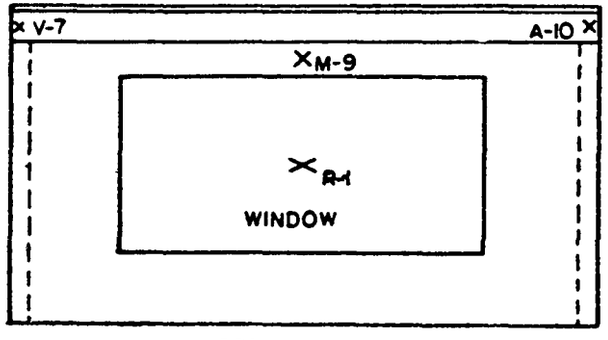
DATACRAFT INC.

DRAWN R WHITE	SCALE NONE	REVISIONS	DATE
CHECKED RH			
APPROVED			
DATE 11-22-64			

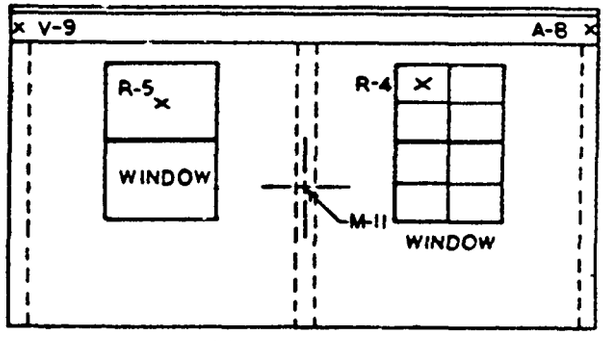
TITLE: INSTRUMENT LOCATIONS

NO ~~FIG. 12~~

FIG. C-17



NORTH WALL

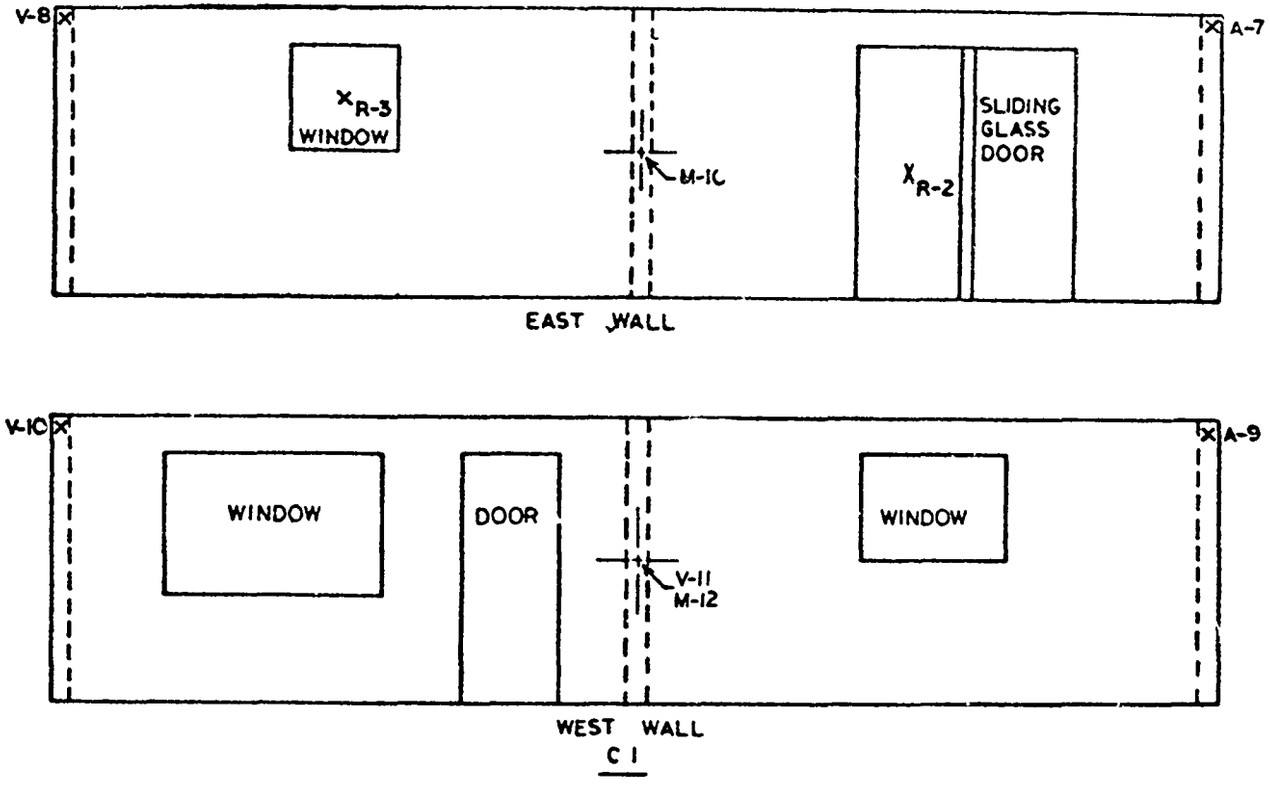


SOUTH WALL

C 1

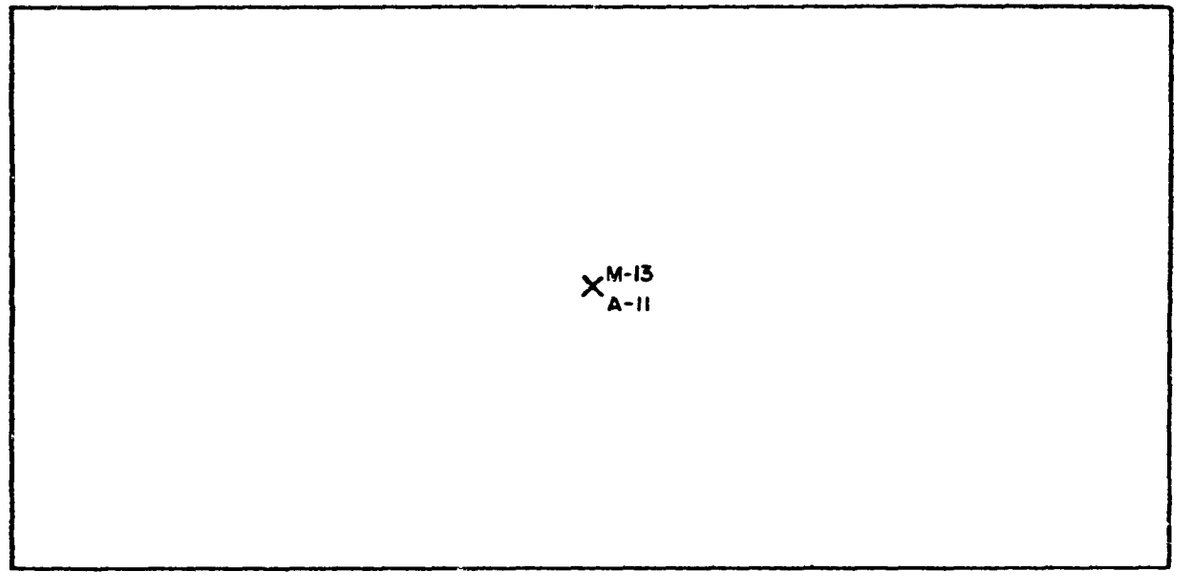
FIG. C-18

DATACRAFT INC.			
DRAWN R. WHITE	SCALE NONE	REVISIONS	DATE
CHECKED			
APPROVED			
DATE 11-22-64			
TITLE INSTRUMENT LOCATIONS		NO. ~~FIG. 13~~	



DATACRAFT INC.			
DRAWN R. WHITE	SCALE NONE	REVISIONS	DATE
CHECKED			
APPROVED			
DATE 11-22-64			
TITLE INSTRUMENT LOCATIONS		NO. ~~FIG. 14~~	

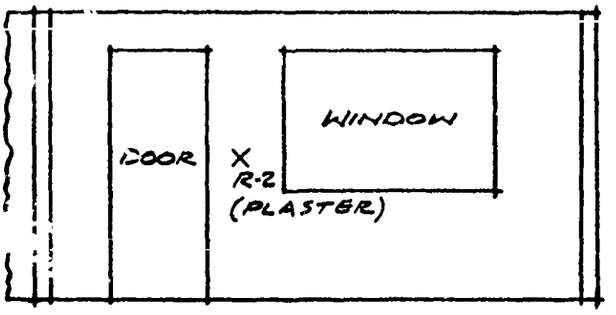
FIG. C-19



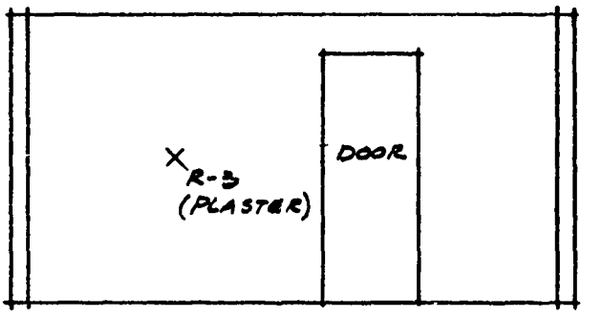
ROOF TOP
C 1

FIG. C-20

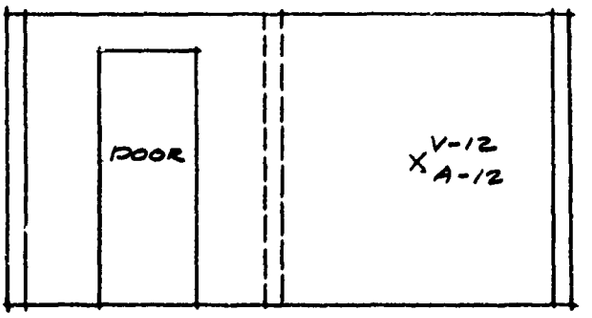
DATACRAFT INC.			
DRAWN R. WHITE	SCALE NONE	REVISIONS	DATE
CHECKED RG.			
APPROVED			
DATE 11-22-64			
TITLE INSTRUMENT LOCATIONS		NO. ~~FIG. 15~~	



WEST WALL LIVINGROOM
C1

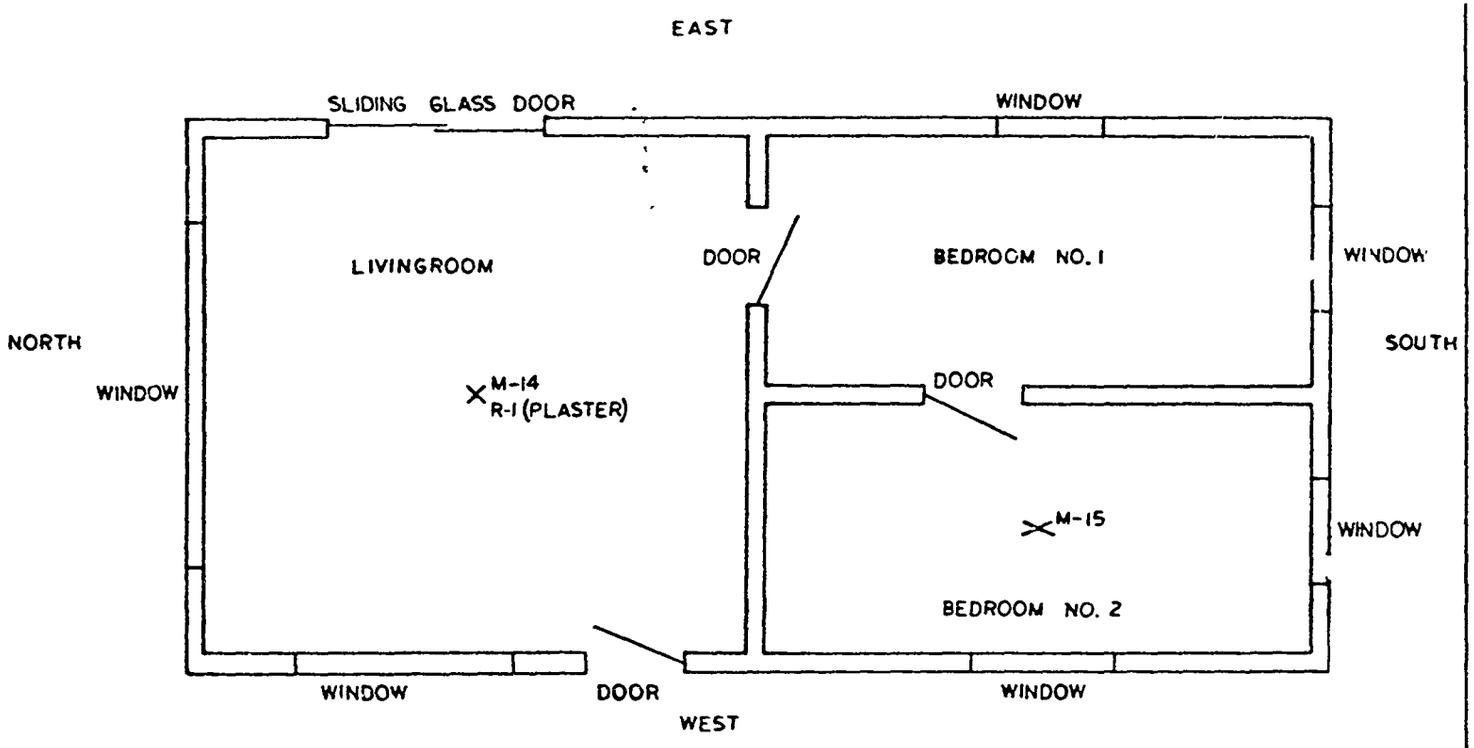


WEST WALL BEDROOM NO.1
C1



SOUTH WALL LIVINGROOM
C1

11-22-64
FIG. C-21



C 1

NOTE: MIKES 4 OFF FLOOR
ROSETTE STRAIN GUAGE R-1
LOCATED ON PLASTER CEILING

DATACRAFT INC.

DRAWN R WHITE	SCALE NONE	REVISIONS	DATE
CHECKED			
APPROVED			
DATE 11-22-64			

TITLE: INSTRUMENT LOCATIONS

NO. ~~FIG. 18~~

FIG. C-22

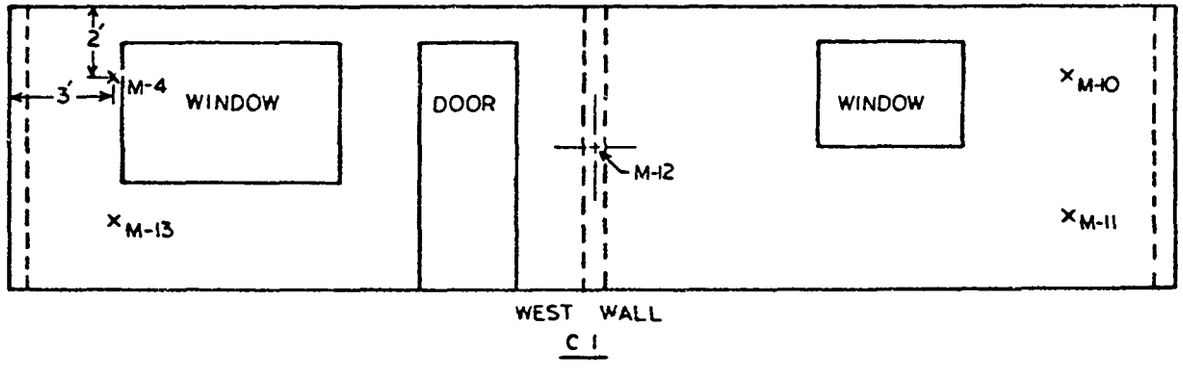
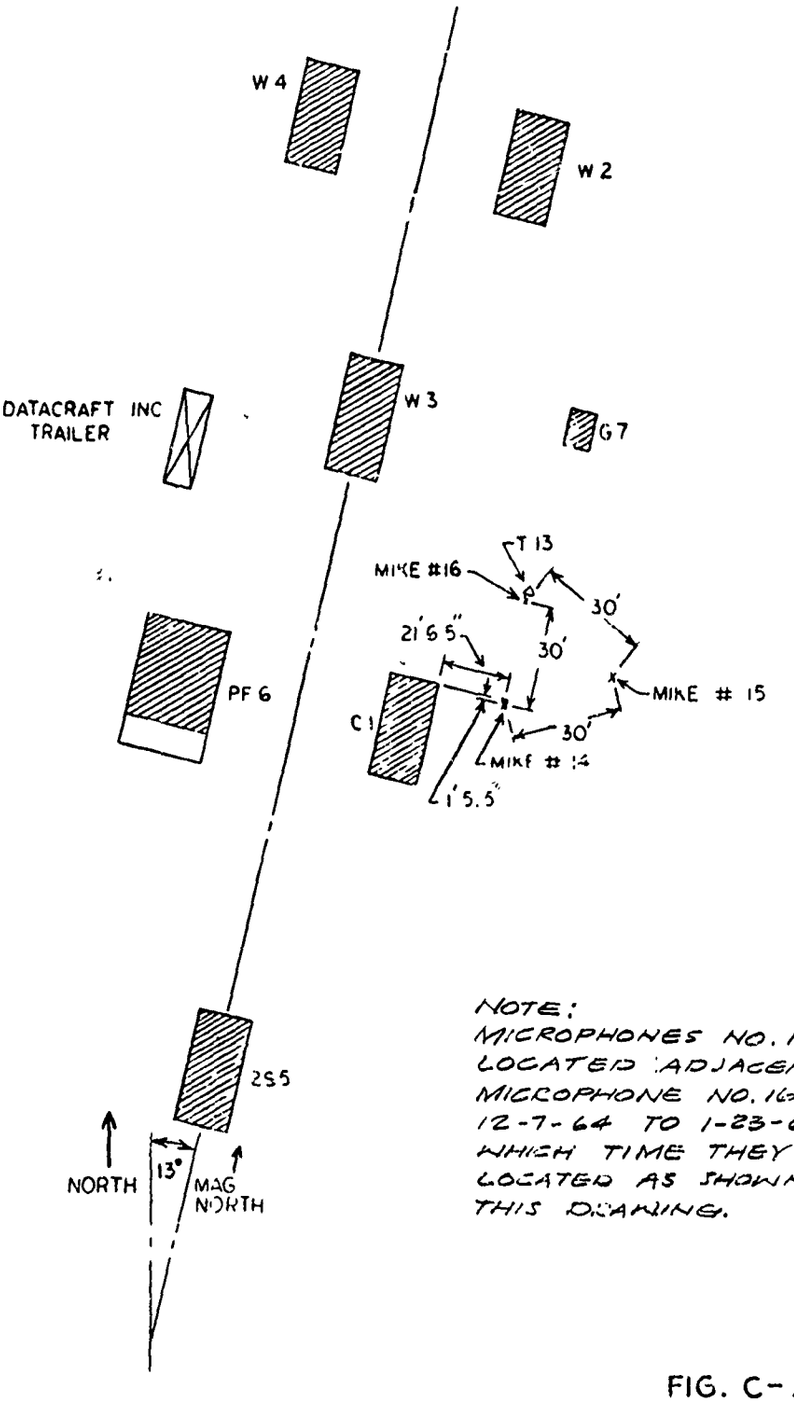


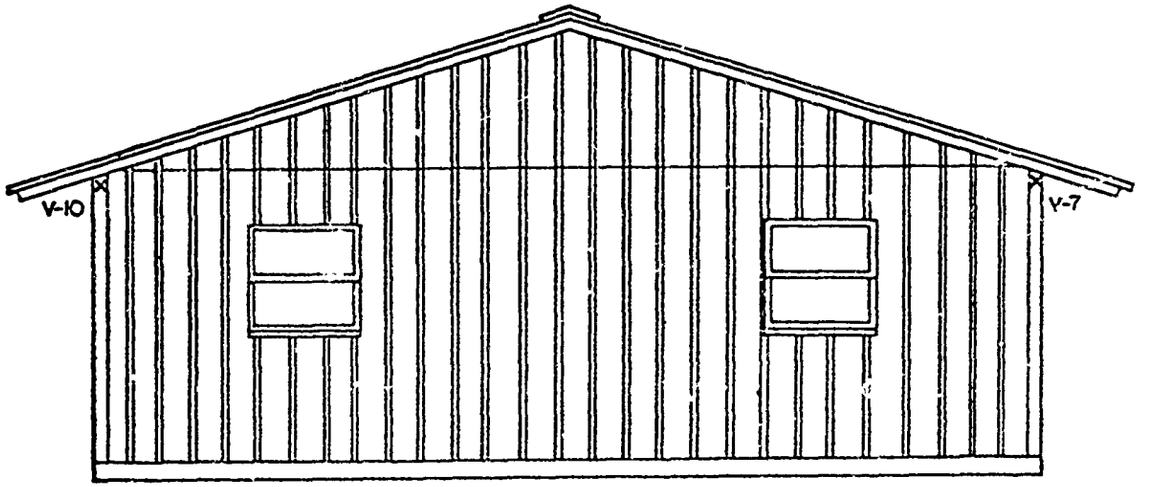
FIG. C-23

DATACRAFT INC.			
DRAWN R. WHITE	SCALE NONE	REVISIONS	DATE
CHECKED			
APPROVED			
DATE 12-7-64			
TITLE INSTRUMENT LOCATIONS		NO. ~~FIG. 19~~	



NOTE:
MICROPHONES NO. 14 & 15 LOCATED ADJACENT TO MICROPHONE NO. 16 FROM 12-7-64 TO 1-23-65 AT WHICH TIME THEY WERE LOCATED AS SHOWN ON THIS DRAWING.

FIG. C-24



NORTH ELEVATION OF PFG

DATACRAFT INC.			
DRAWN R. WHITE	SC 1/4"=1'0"	REVISIONS	DATE
CHECKED			
APPROVED			
DATE ~~9-12-65~~			
TITLE INSTRUMENT LOCATIONS		NO ~~FIG. 21~~	

12-9-64
FIG. C-25

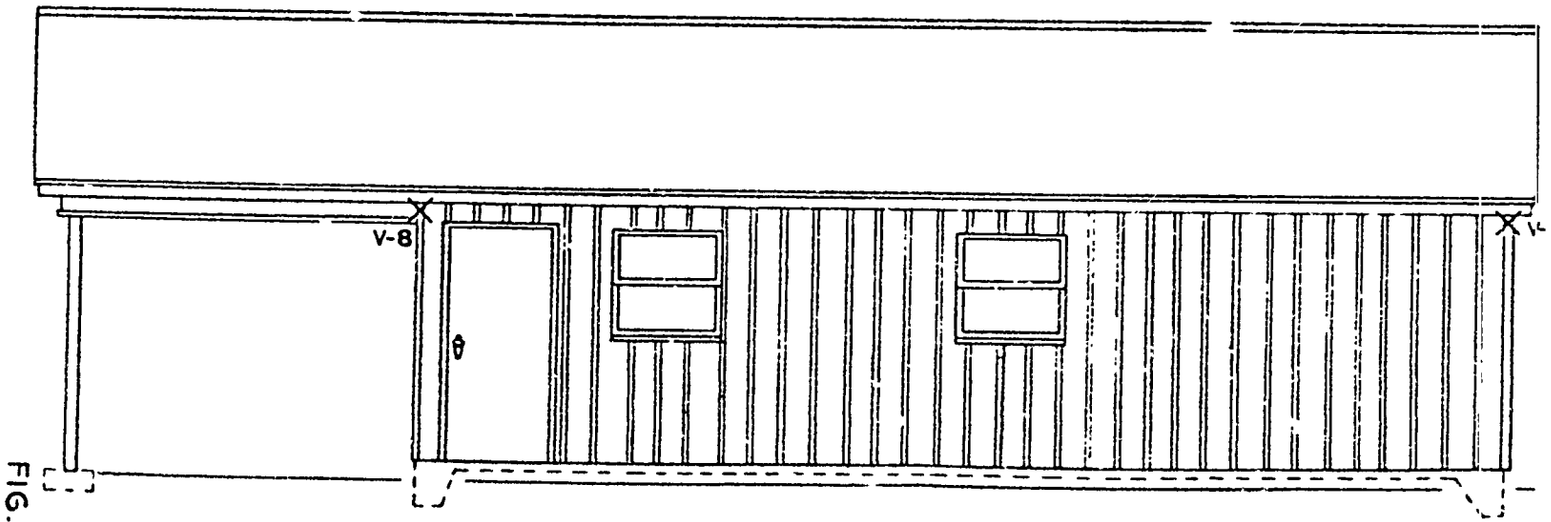
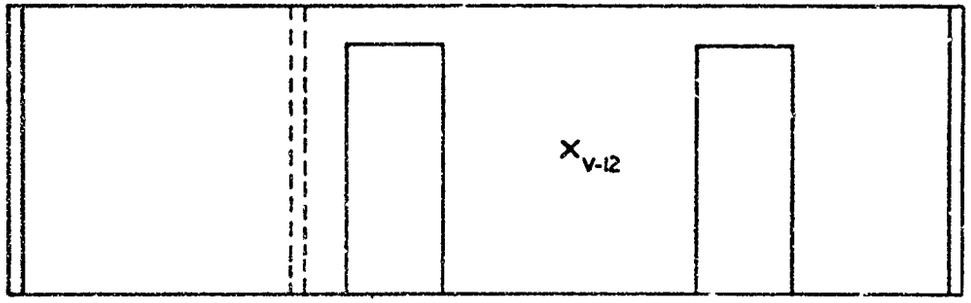


FIG. C-26

EAST ELEVATION OF PF6

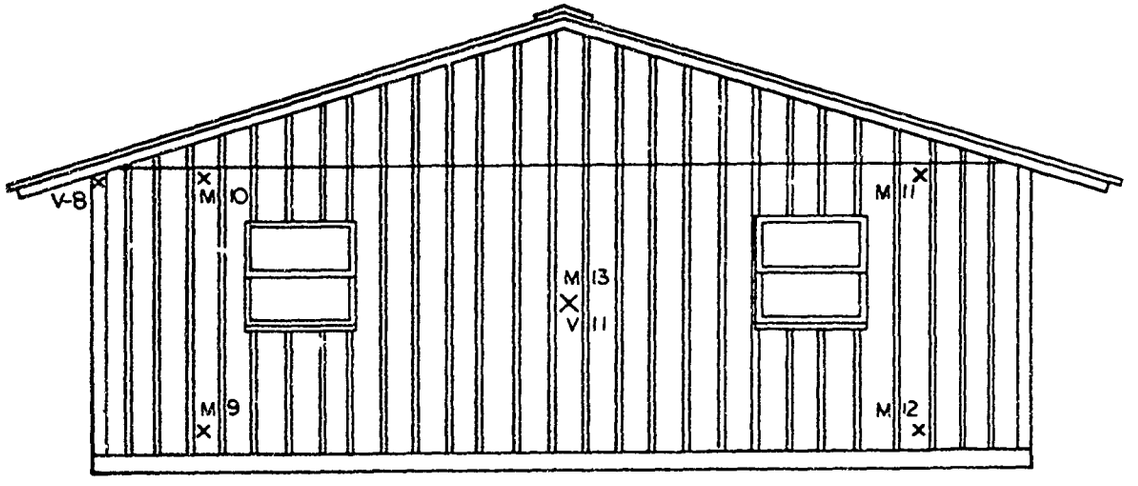
NOTE: NEW VELOCITY PICKUP LOCATIONS ON 12-9-64



SOUTH INSIDE BEDROOM WALL
OF PF6

FIG. C-27

DATACRAFT INC.			
DRAWN R WHITE	SCALE 1/4" = 1'0"	REVISIONS	DATE
CHECKED			
APPROVED			
DATE 1-15-65			
TITLE: INSTURMENT LOCATION		NO ~~FIG. 23~~	

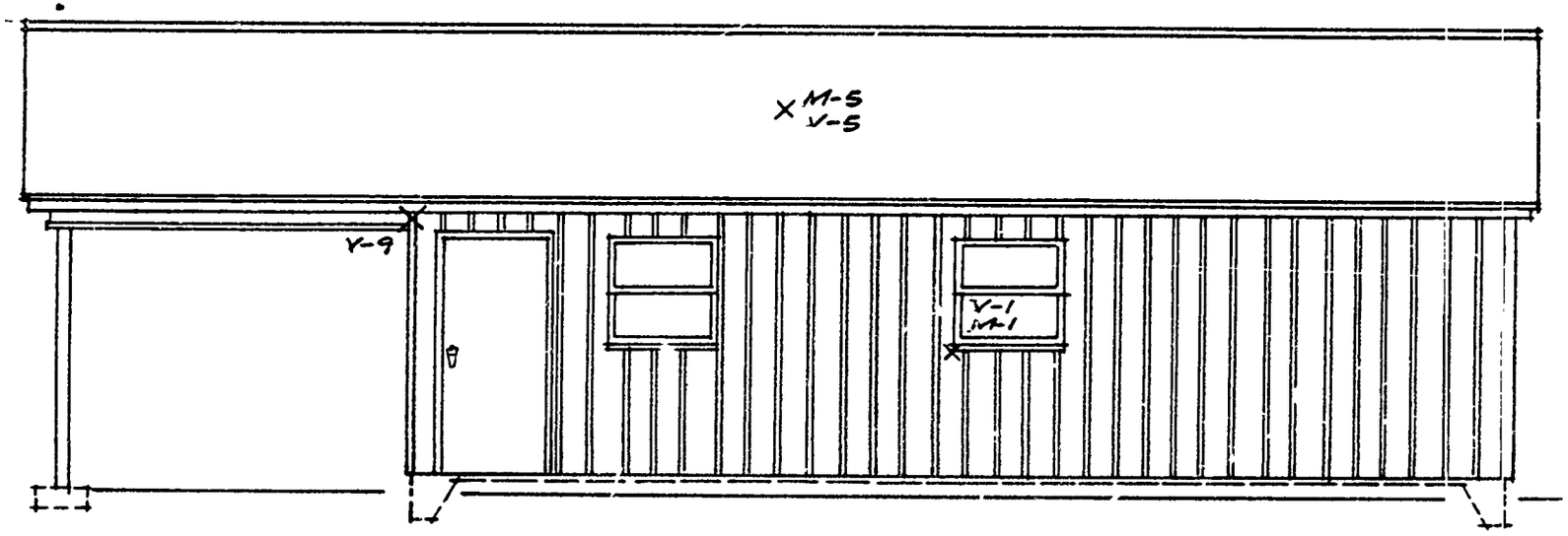


NORTH ELEVATION OF PFG

NOTE: VELOCITY PICKUPS NO. 8 & 11 LOCATED AS PER DWG. ON 1-15-65 ALL OTHER INSTRUMENTS LOCATED AS PER DWG. ON 1-24-65.

DATACRAFT INC.			
DRAWN R. WHITE	SCALE 1/4"=1'0"	REVISIONS	DATE
CHECKED			
APPROVED			
DATE 1-15-65			
TITLE INSTRUMENT LOCATIONS		NO ~~FIG. 24~~	

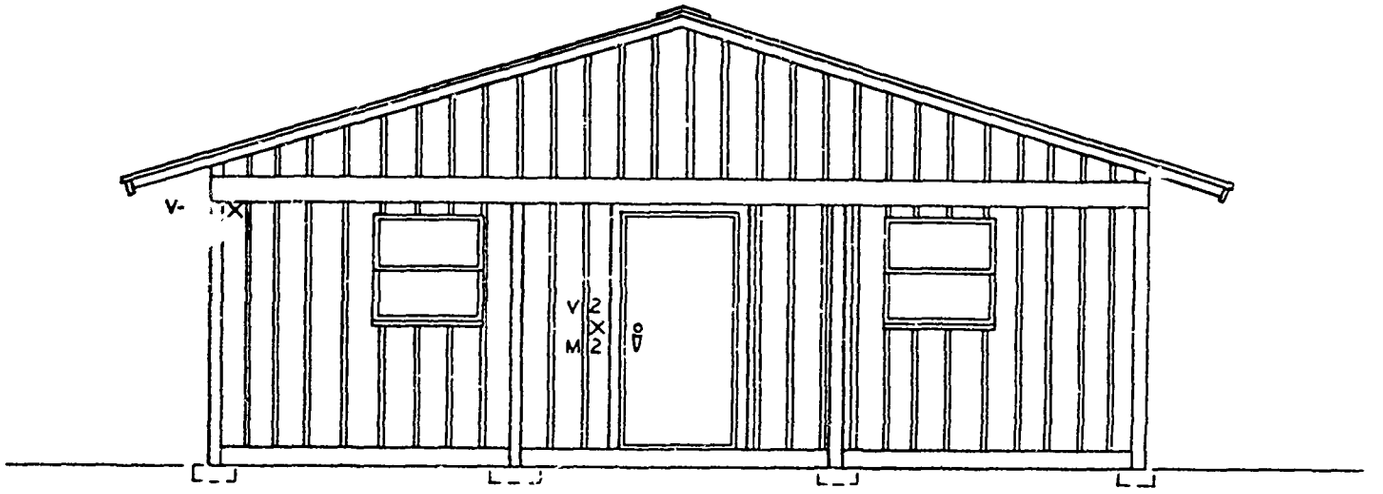
FIG. C-28



PARTIAL EAST ELEVATION OF PFG

NOTE. VELOCITY PICKUP NO. 9
LOCATED AS PER DWG.
ON 1-15-65.
OTHER INSTRUMENTS
LOCATED AS PER DWG.
ON 1-24-65

FIG. C-29

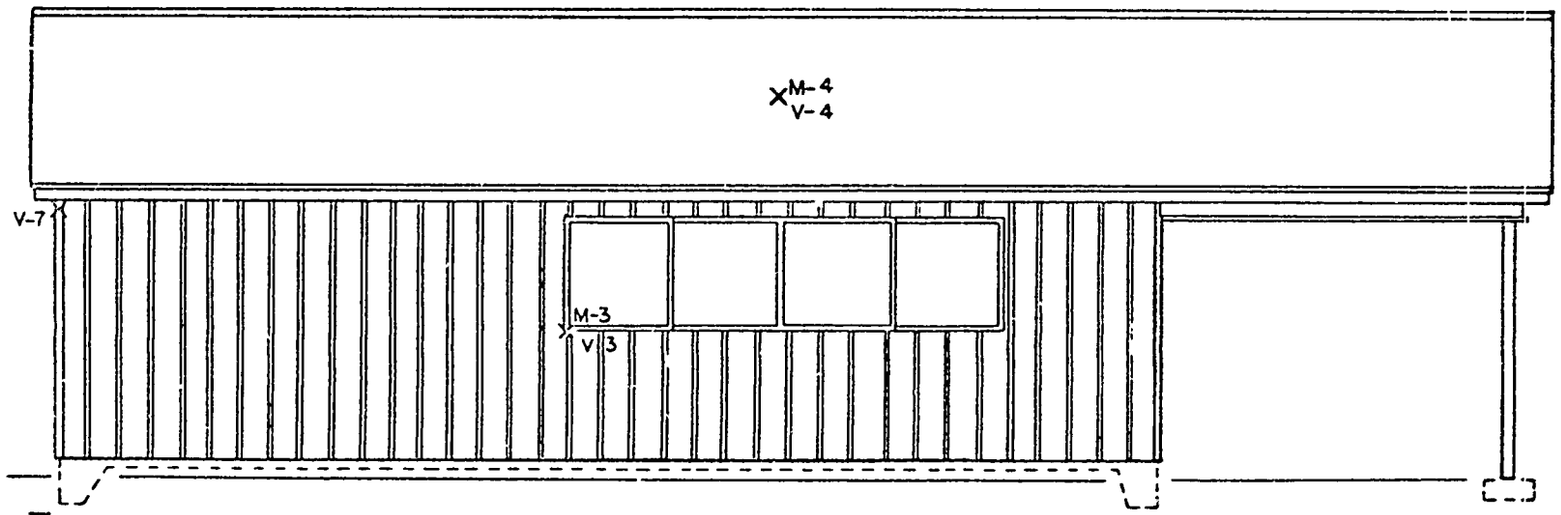


SOUTH ELEVATION OF PF6

NOTE: VELOCITY PICKUP NO. 10 AS PER DWG. ON 1-15-65

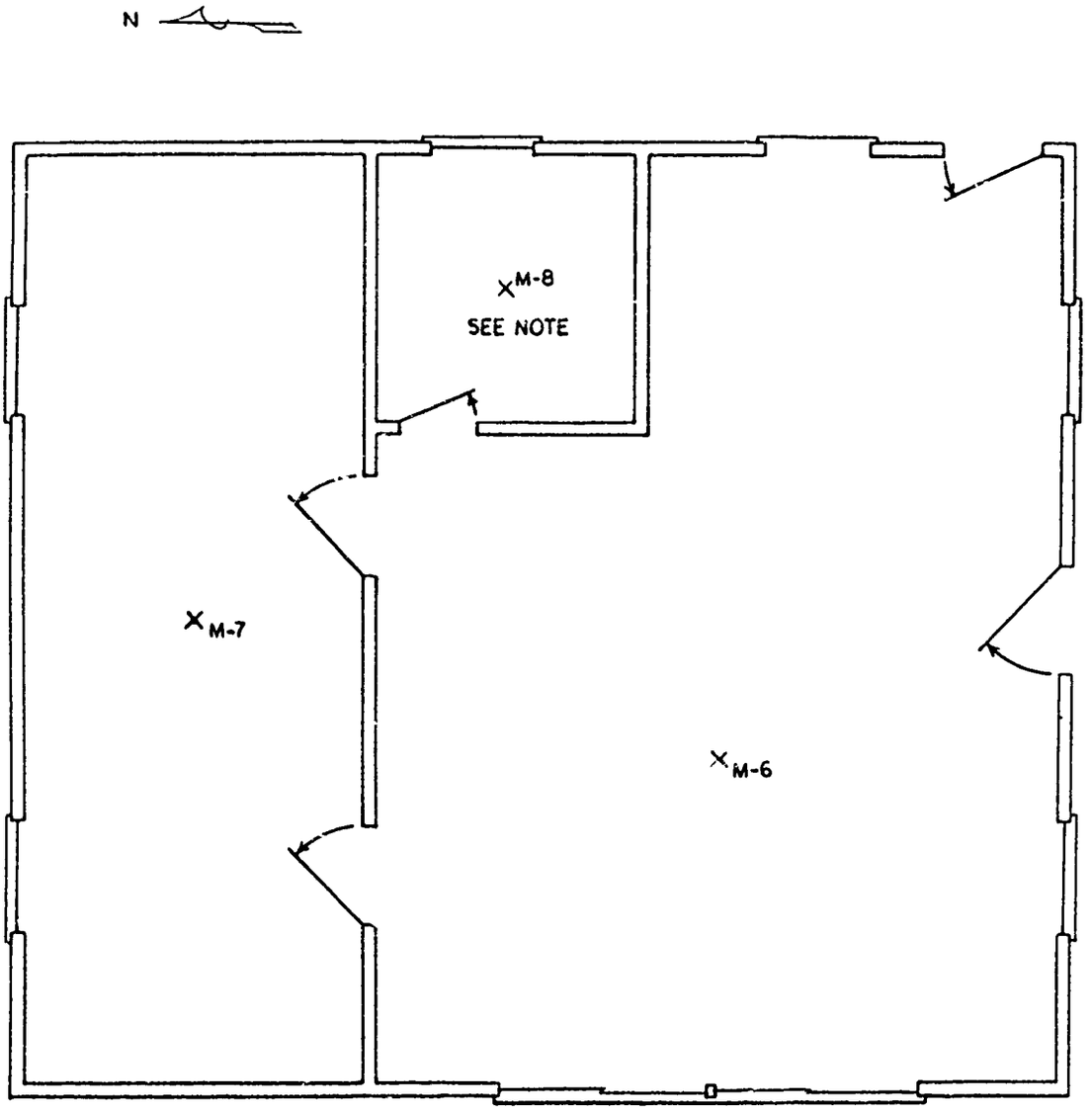
DATACRAFT INC.			
DRAWN R. WHITE	SCALE 1/4" = 1'0"	REVISIONS	DATE
CHECKED			
APPROVED			
DATE 1-24-65			
TITLE INSTRUMENT LOCATIONS		NO ~~FIG. 26~~	

FIG. C-30



WEST ELEVATION OF PF6

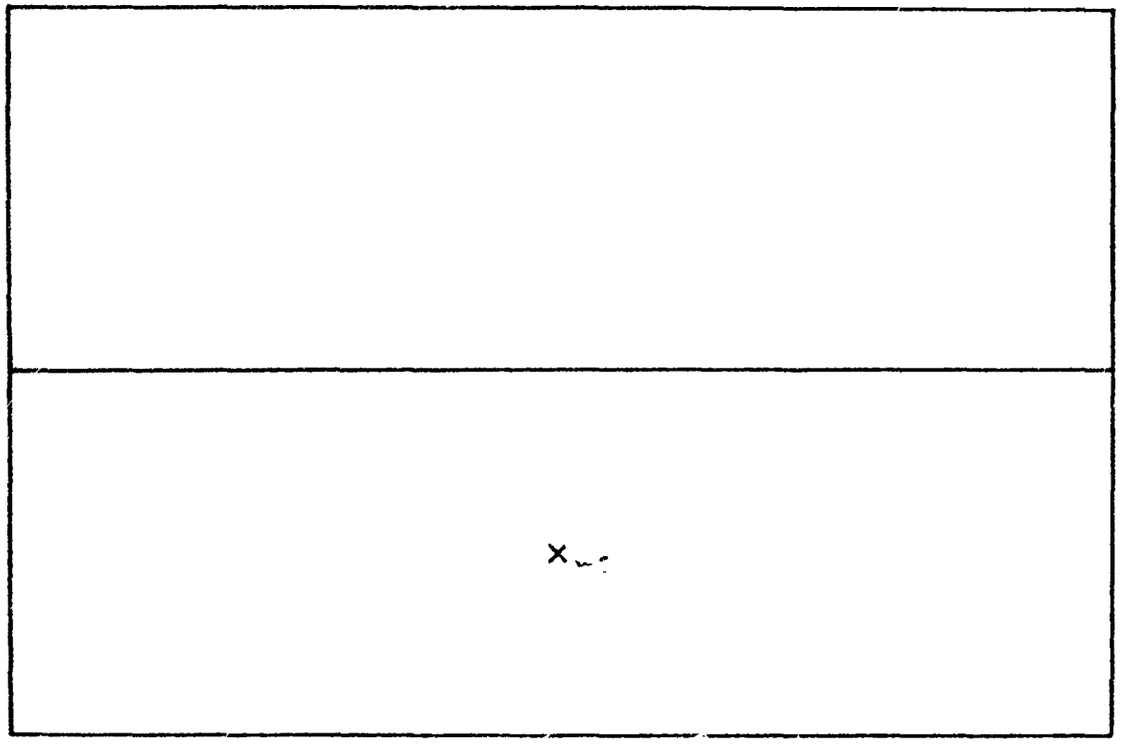
FIG. C-31 1-24-65



FLOOR PLAN FOR PF6

NOTE: MIKE NO. 8 RELOCATED IN ATTIC SPACE OF PF-6 DIRECTLY OVER MIKE NO. 6 ON 1-28-65. MIKES M-6, 7 & 8 SUSPENDED 4' ABOVE FLOOR.

FIG. C-32



TOP VIEW OF - STORE FRONT BUILDING -

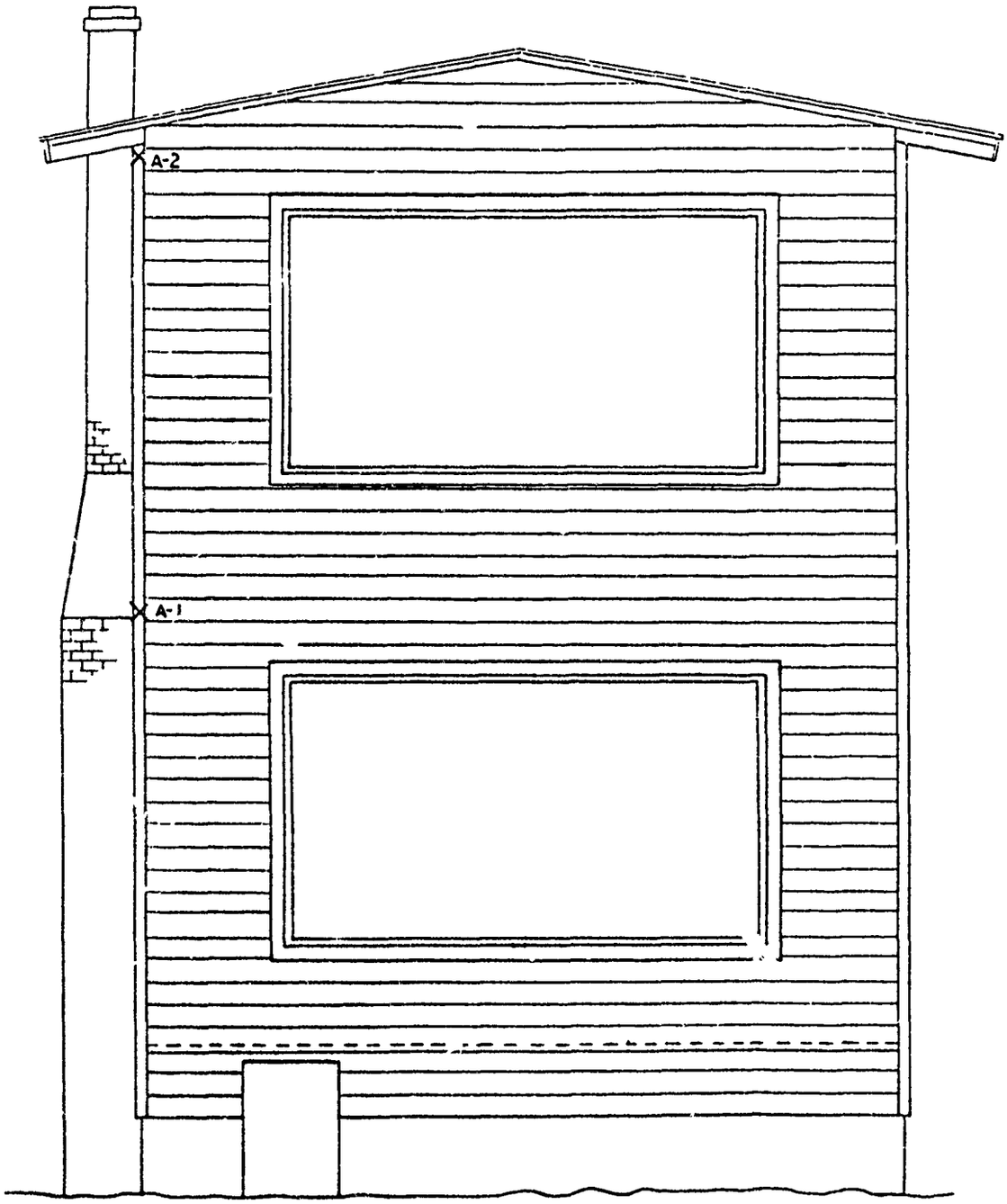
FIG. C - 33

DATACRAFT INC.

DRAWN R. WHITE	SCALE 1/8" = 1'0"	REVISIONS	DATE
CHECKED [illegible]			
APPROVED			
DATE 1-29-65			

TITLE: INSTRUMENT LOCATIONS

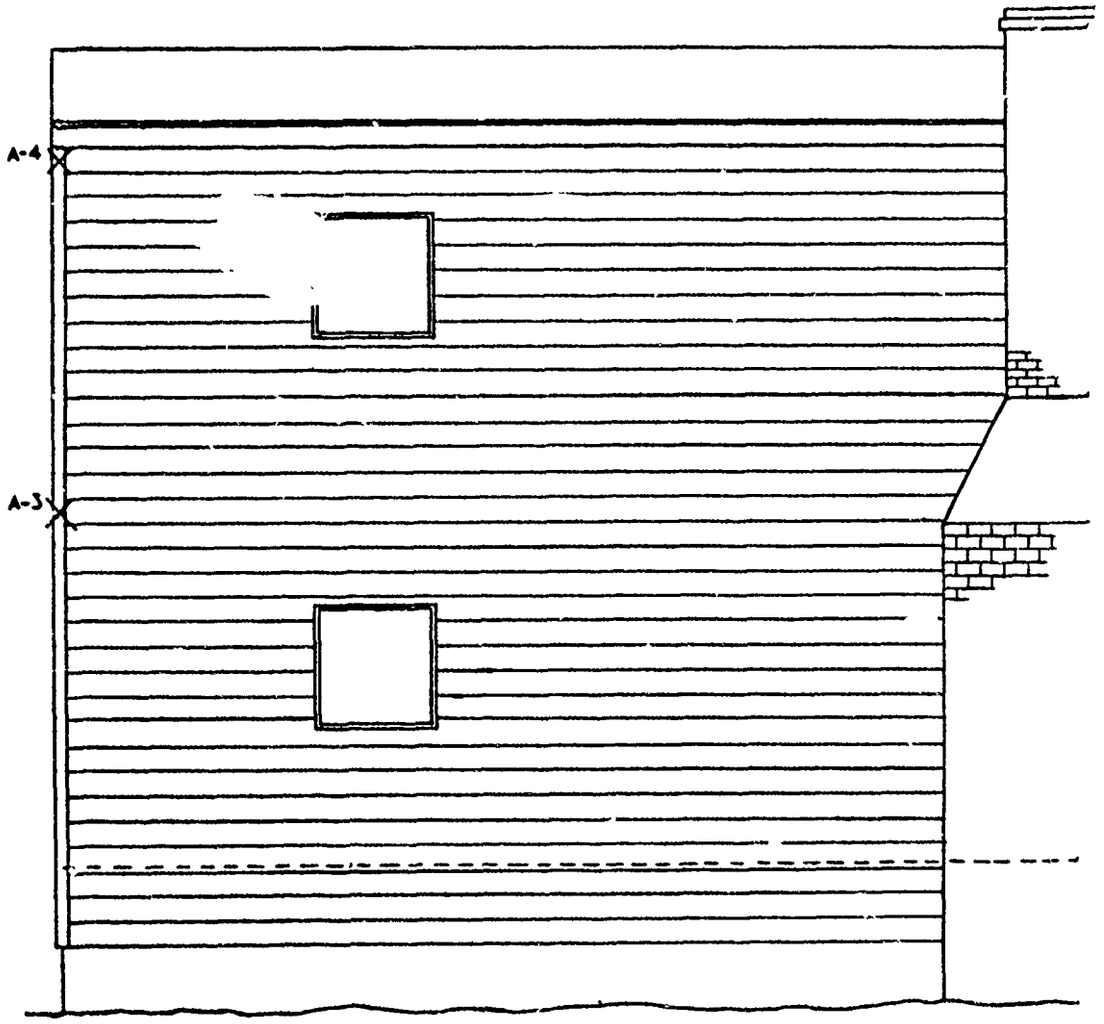
NO. ~~FIG. 29~~



NORTH ELEVATION OF 255

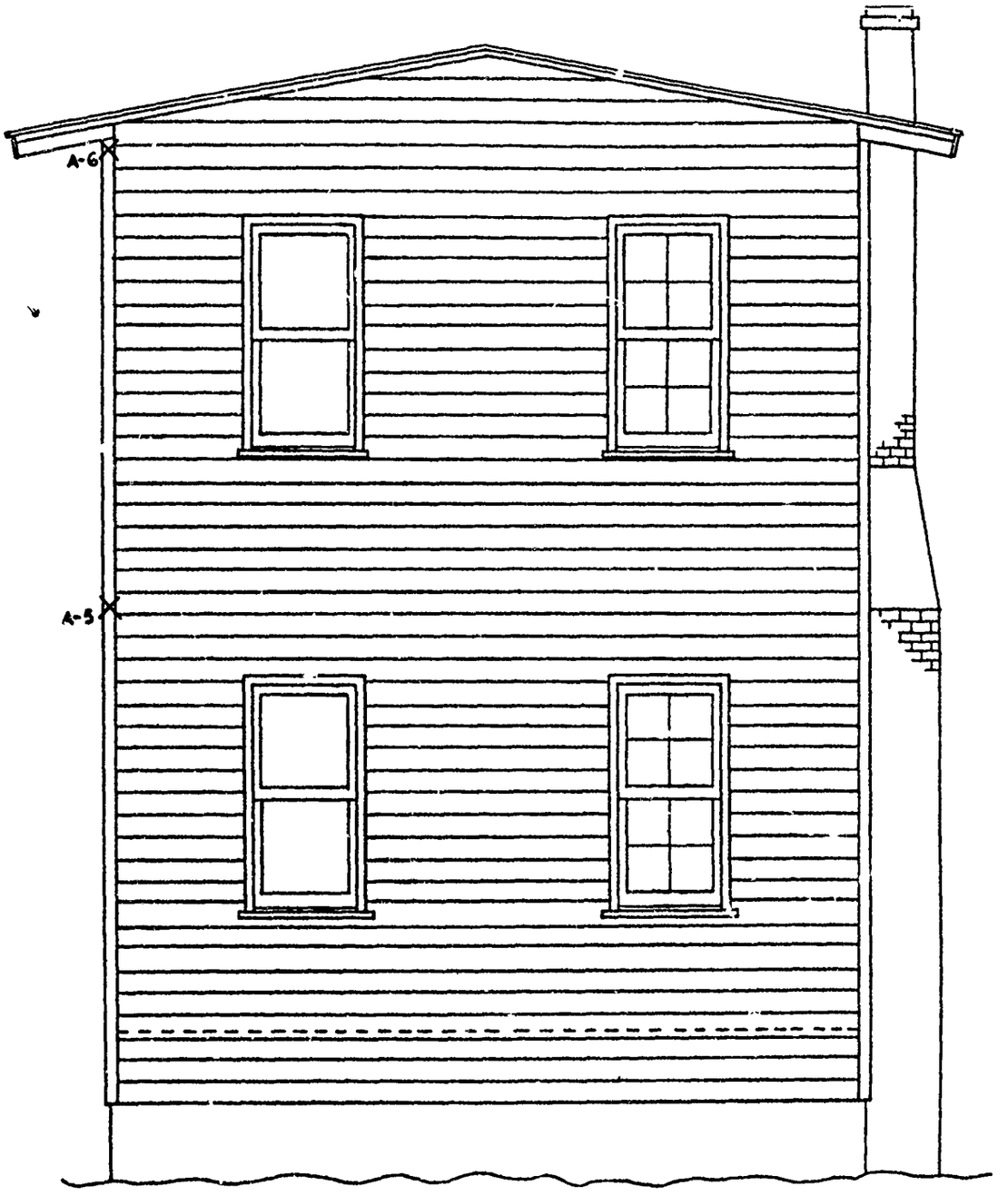
1-29-65

FIG. C-34



EAST ELEVATION OF 2S5

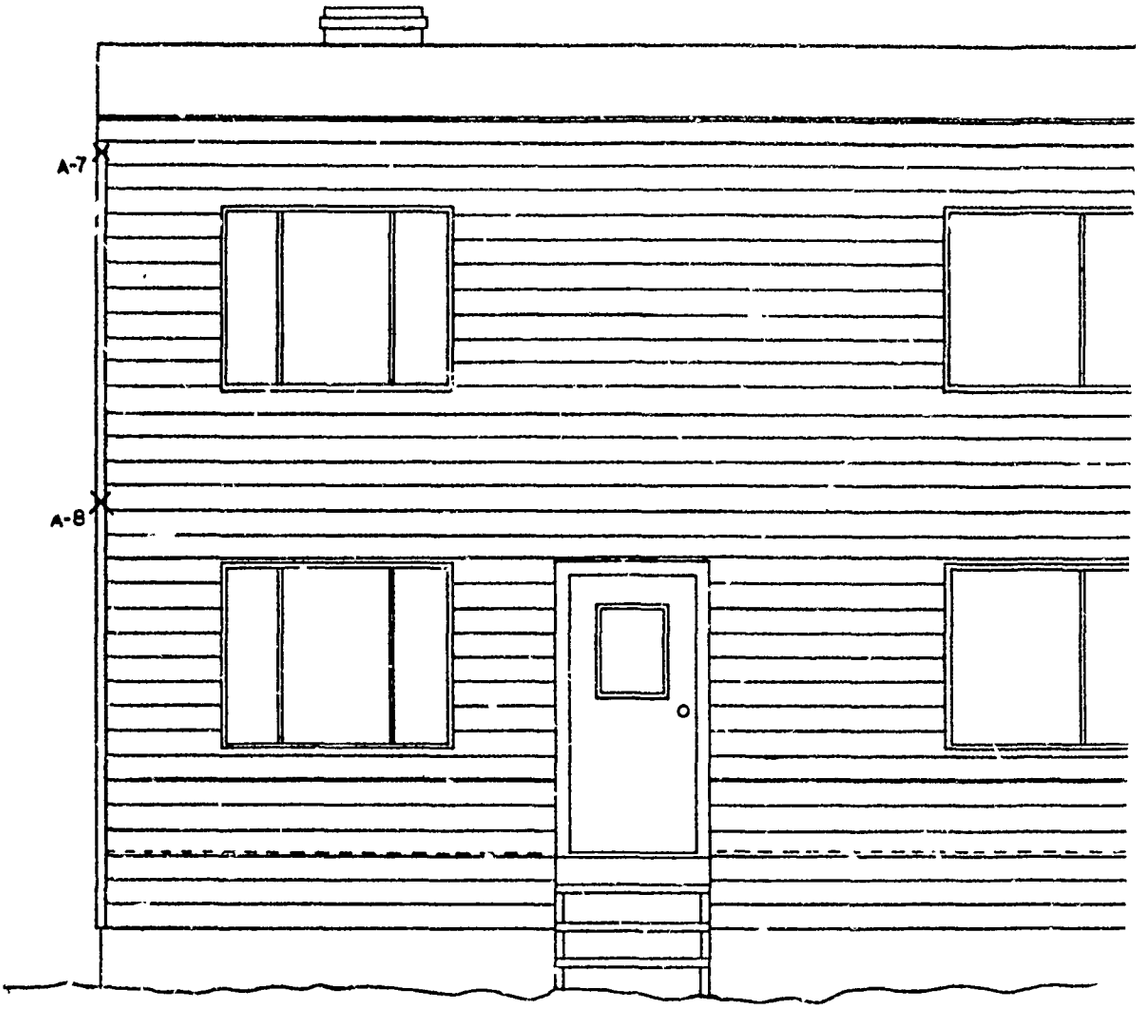
1-29-65
FIG. C-35



SOUTH ELEVATION OF 255

1-29-65

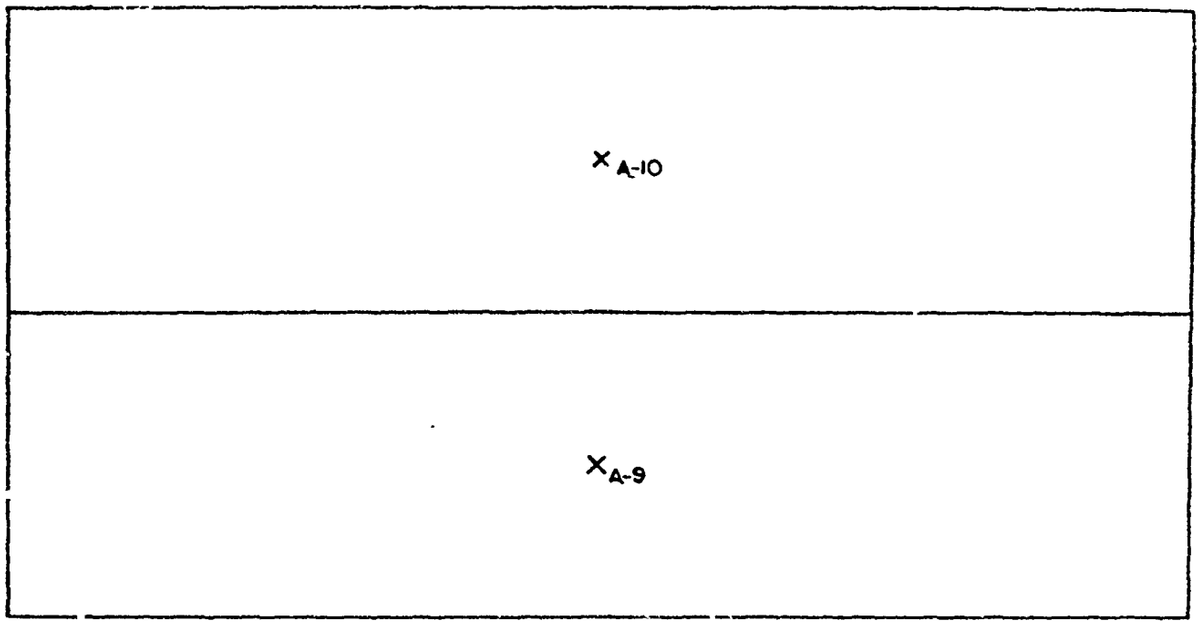
FIG. C-36



PARTIAL WEST ELEVATION OF 2S5

1-29-65

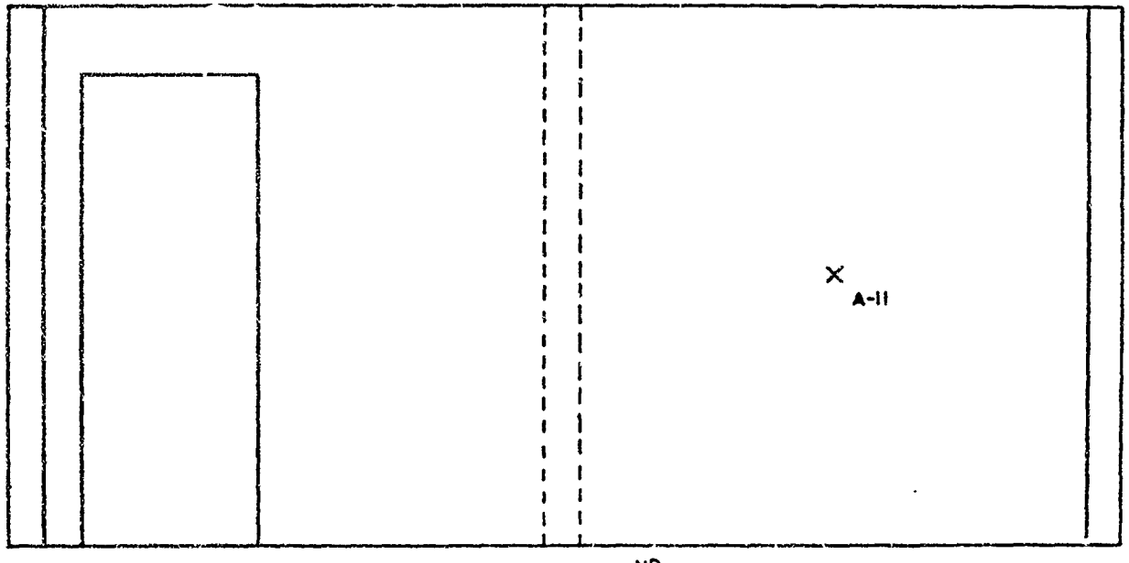
FIG. C-37



ROOF TOP
2S 5

DATACRAFT INC.			
DRAWN R. WHITE	SCALE NONE	REVISIONS	DATE
CHECKED [illegible]			
APPROVED			
DATE ~~12-29-64~~			
TITLE INSTRUMENT LOCATIONS		NO ~~FIG. 34~~	

1-29-65
FIG. C-38

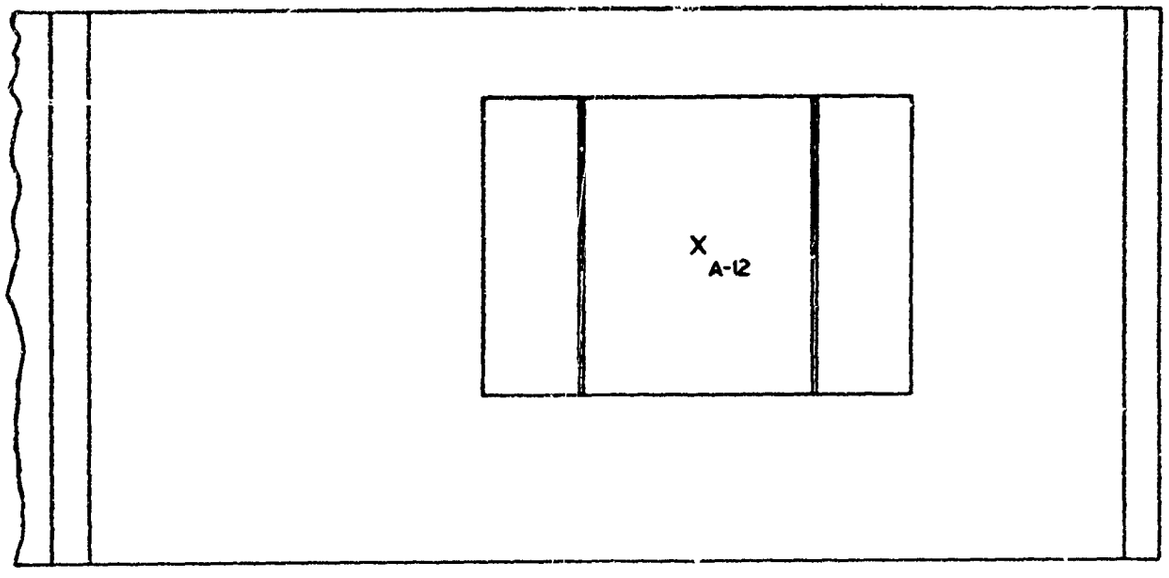


NORTH WALL OF LARGE ROOM 2ND FLOOR OF 255

DATACRAFT INC			
DRAWN R. WHITE	SCALE 1/2" = 1'0"	REVISIONS	DATE
CHECKED R.W.			
APPROVED			
DATE ~~12-29-64~~			
TITLE INSTRUMENT LOCATIONS		NO. ~~FIG. 35~~	

FIG. C-39

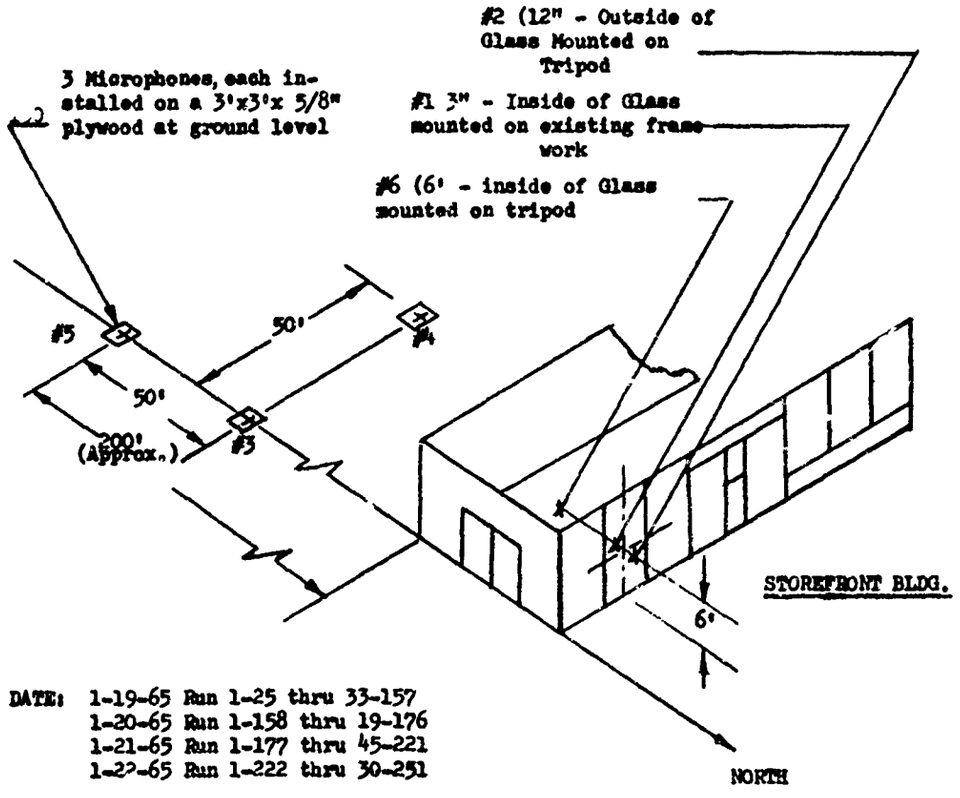
1-29-65



WEST WALL OF LARGE ROOM 2ND FLOOR OF 255

1-29-65
FIG C-0

DATACRAFT INC.			
DRAWN R WHITE	SCALE 1/2" = 1'0"	REVISIONS	DATE
CHECKED RW			
APPROVED			
DATE ~~12-29-64~~			
TITLE INSTRUMENT LOCATIONS		NO ~~FIG. 36~~	



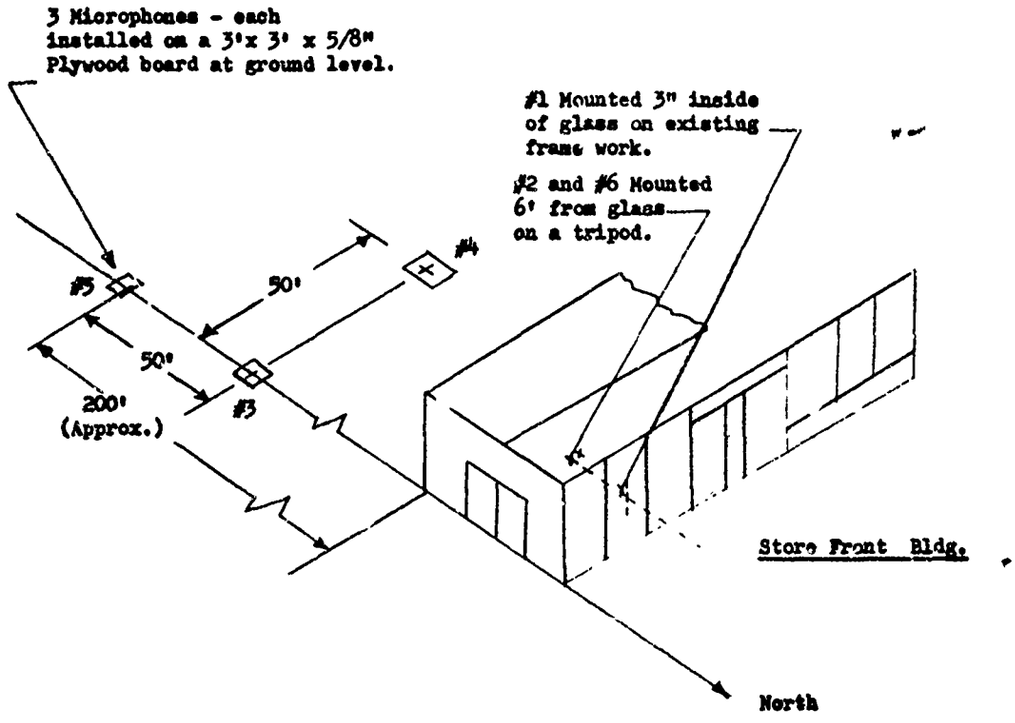
DATE: 1-19-65 Run 1-25 thru 33-157
1-20-65 Run 1-158 thru 19-176
1-21-65 Run 1-177 thru 45-221
1-22-65 Run 1-222 thru 30-251

ENGR.			REVISED	DATE	MICROPHONE LOCATION (Initial Installation) Configuration M	~~FIG. 10~~
CHECK						D6-17485
APR						
APR					THE BOEING COMPANY RENTON, WASHINGTON	~~Page 21~~

TD 1017-80

FIG. C-41

6-7080



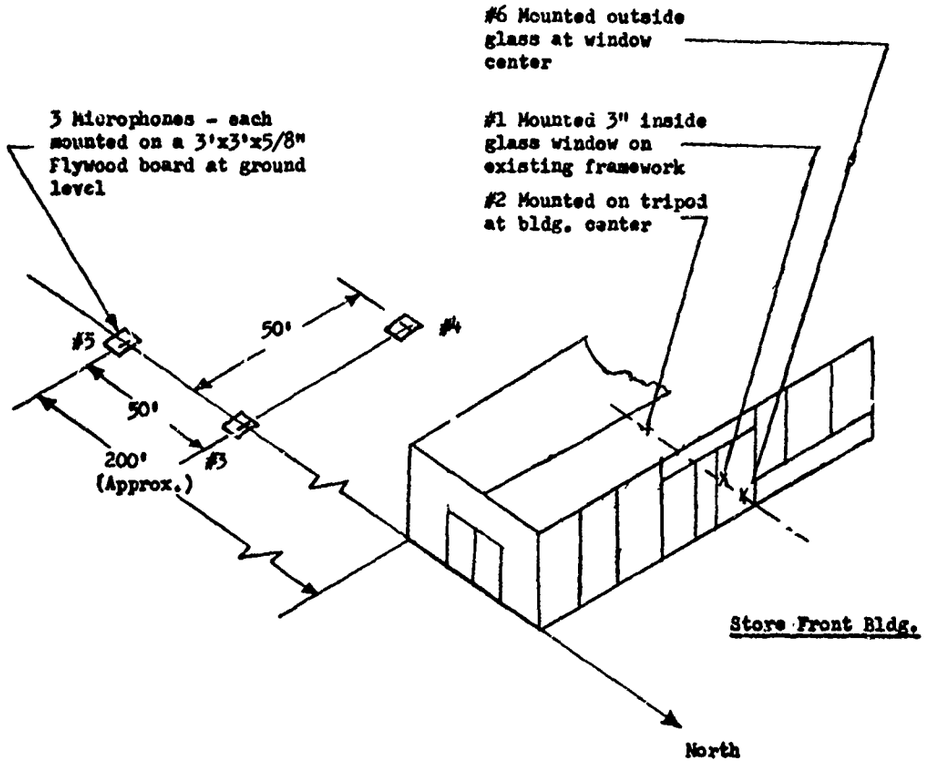
DATE: 1-22-65 Run 31-252 thru 33-254

CALC			REVISED	DATE	MICROPHONE LOCATION DIAGRAM	~~FIG. 11~~
CHECK					CONFIGURATION N	D6-17485
APR						
APR					THE BOEING COMPANY RENTON, WASHINGTON	PAGE ~~22~~

TD 1017 R6

FIG. C-42

8-7000



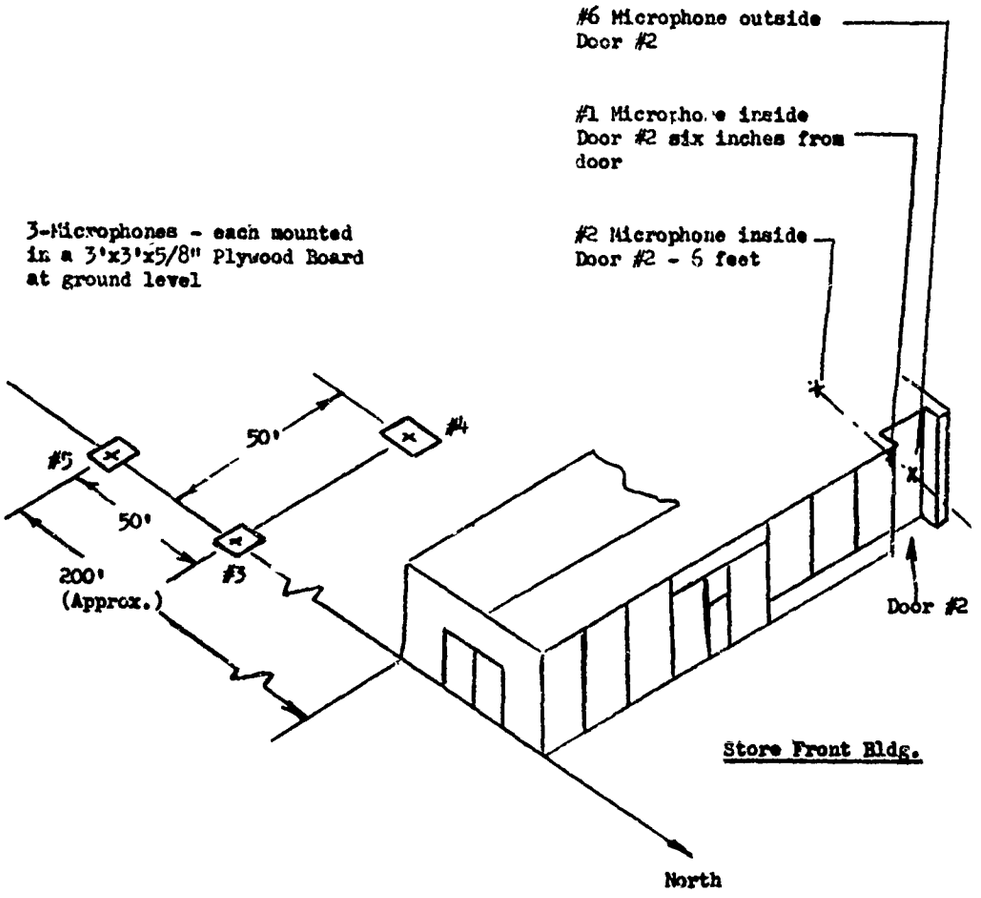
DATE: 1-23-65 Run 1-255 thru 50-304
1-24-65 Run 1-374 thru 52-425

CALC			REVISED	DATE	MICROPHONE LOCATION DIAGRAM	~~FIG. 12~~
CHECK						
APR					CONFIGURATION P	D6-17485
APR						
					THE BOEING COMPANY RENTON, WASHINGTON	PAGE ~~23~~

YB 1017-88

FIG. C-43

6-700U

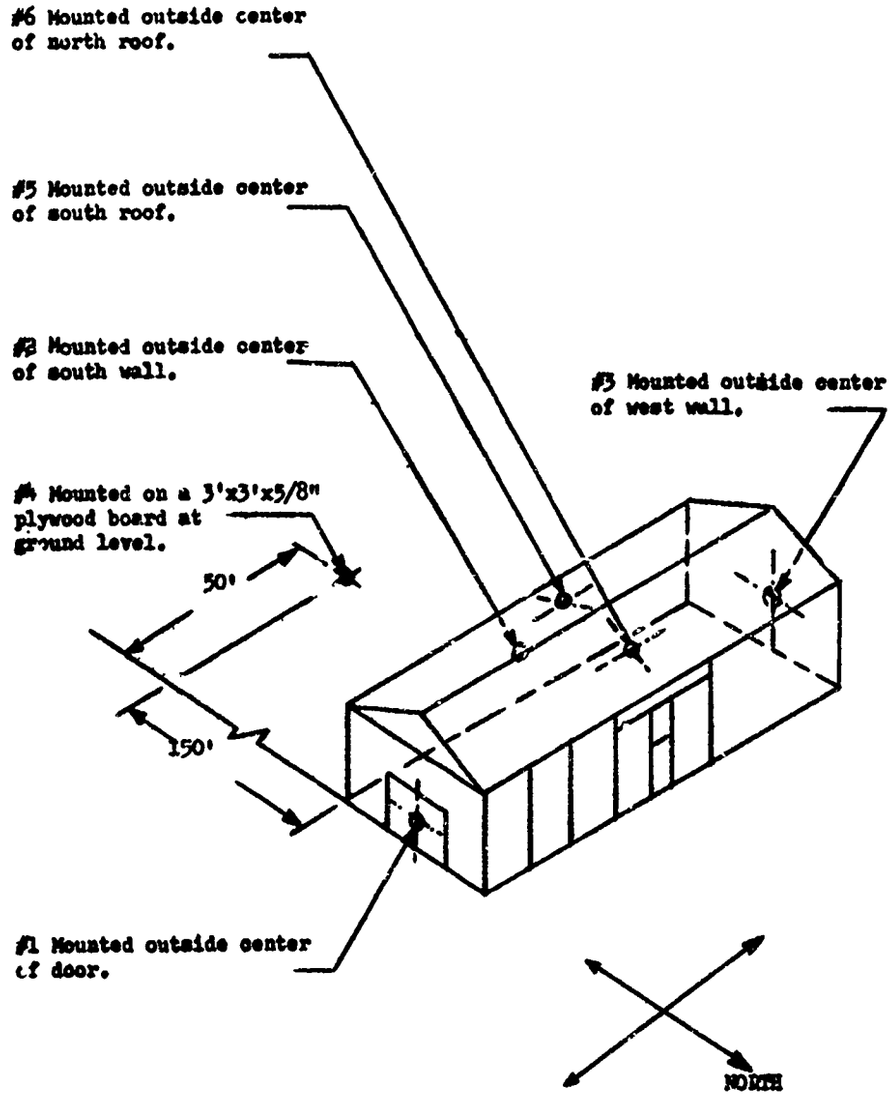


DATE: 1-25-65 Run 1-344 thru 30-373
1-26-65 Run 1-374 thru 52-425

ENGR.			REVISED	DATE	MICROPHONE LOCATION DIAGRAM	~~FIG. 13~~
CHECK					CONFIGURATION Q	D6-17485
APR					THE BOEING COMPANY RENTON WASHINGTON	~~Page 24~~
APR						

TD 1017-80

FIG. C-44



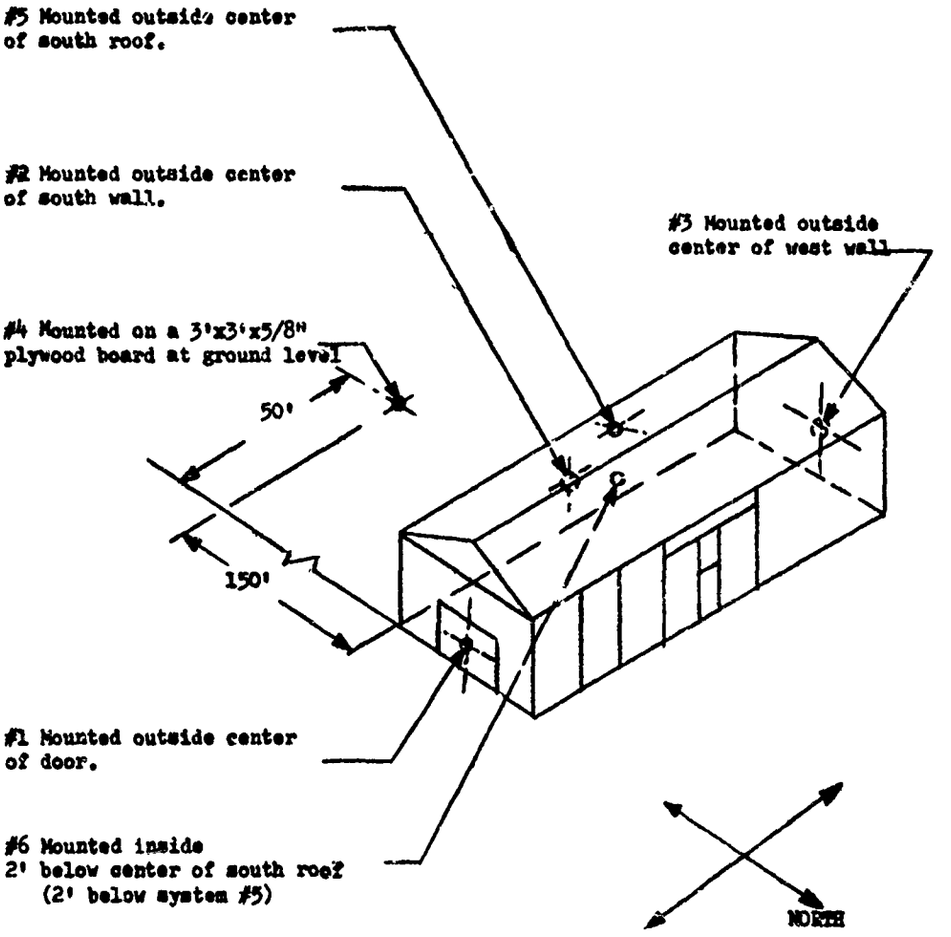
DATE: 1-27-65 Run 1-426 thru 30-459
1-28-65 1-556 thru 39-494

ENGR.			REVISED	DATE	MICROPHONE LOCATION DIAGRAM CONFIGURATION R	~~Fig. 34~~
CHECK						
APR						D6-17485
APR					THE BOEING COMPANY RENTON, WASHINGTON	~~Page 25~~

TD 1017-86

FIG. C-45

6-7000



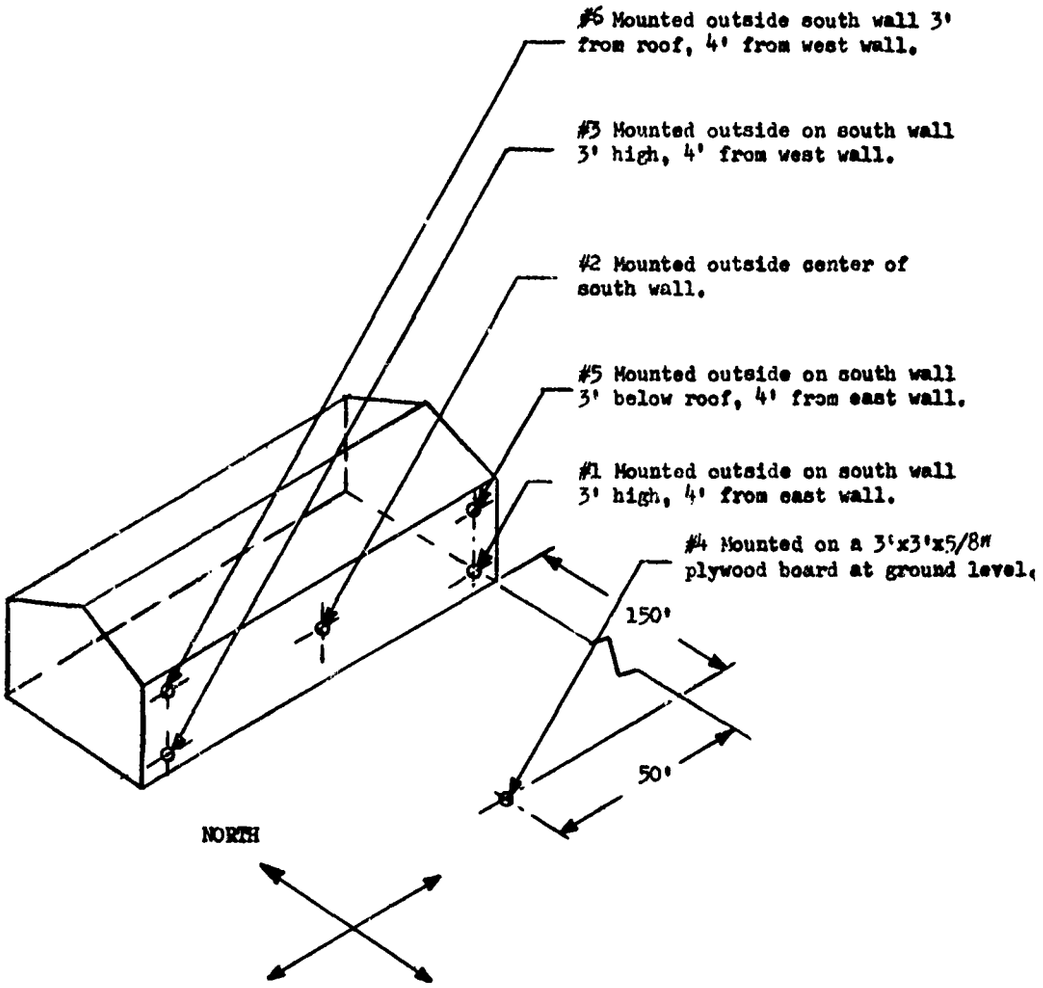
DATE: 1-29-65 Run 1-495 thru 35-529
1-30-65 Run 1-530 thru 30-559

CALC			REVISED	DATE	MICROPHONE LOCATION DIAGRAM CONFIGURATION S	FIG. 15
CHECK						D6-17485
APR						
APR					THE BOEING COMPANY RENTON, WASHINGTON	PAGE 26

TD 1017.00

FIG. C-46

6-7000



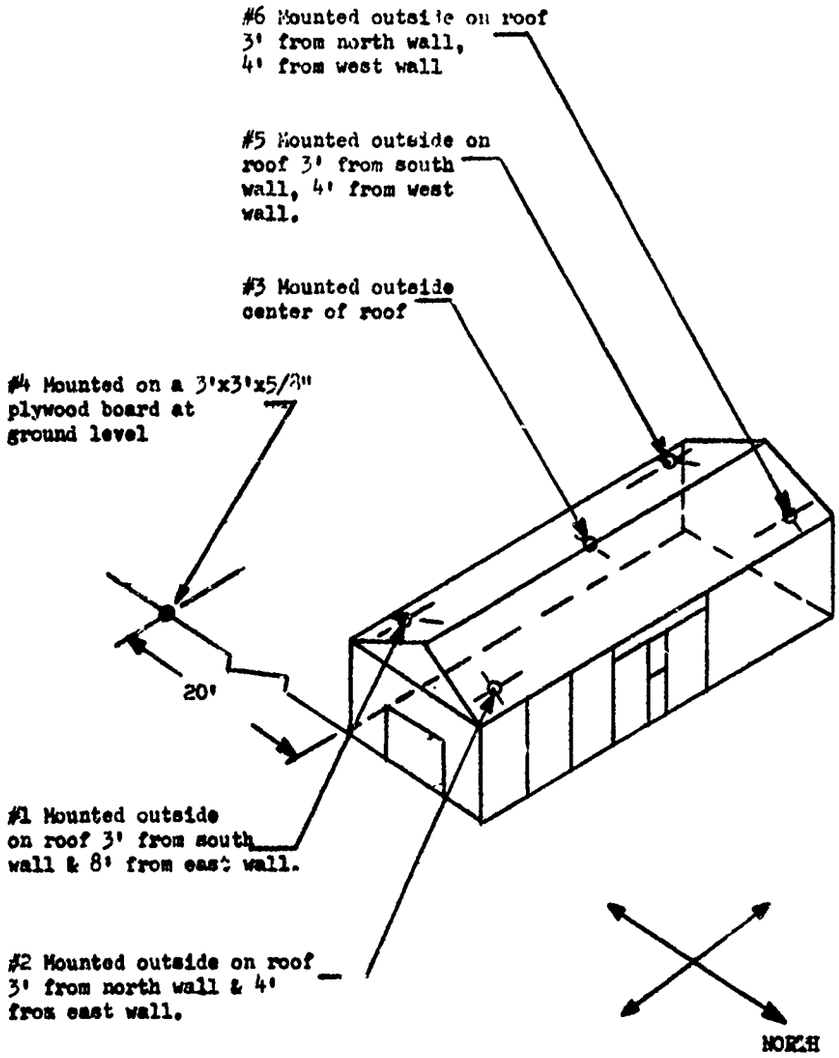
DATE: 1-31-65 Run 1-560 thru 30-589
2-1-65 Run 1-590 thru 31-620

CALC			REVISED	DATE	MICROPHONE LOCATION DIAGRAM CONFIGURATION T	~~FIG. 16~~ D6-17485
CHECK						
APE						
APE					THE BOEING COMPANY RENTON, WASHINGTON	PAGE ~~27~~

TD 1917-R6

FIG. C - 47

6-7000



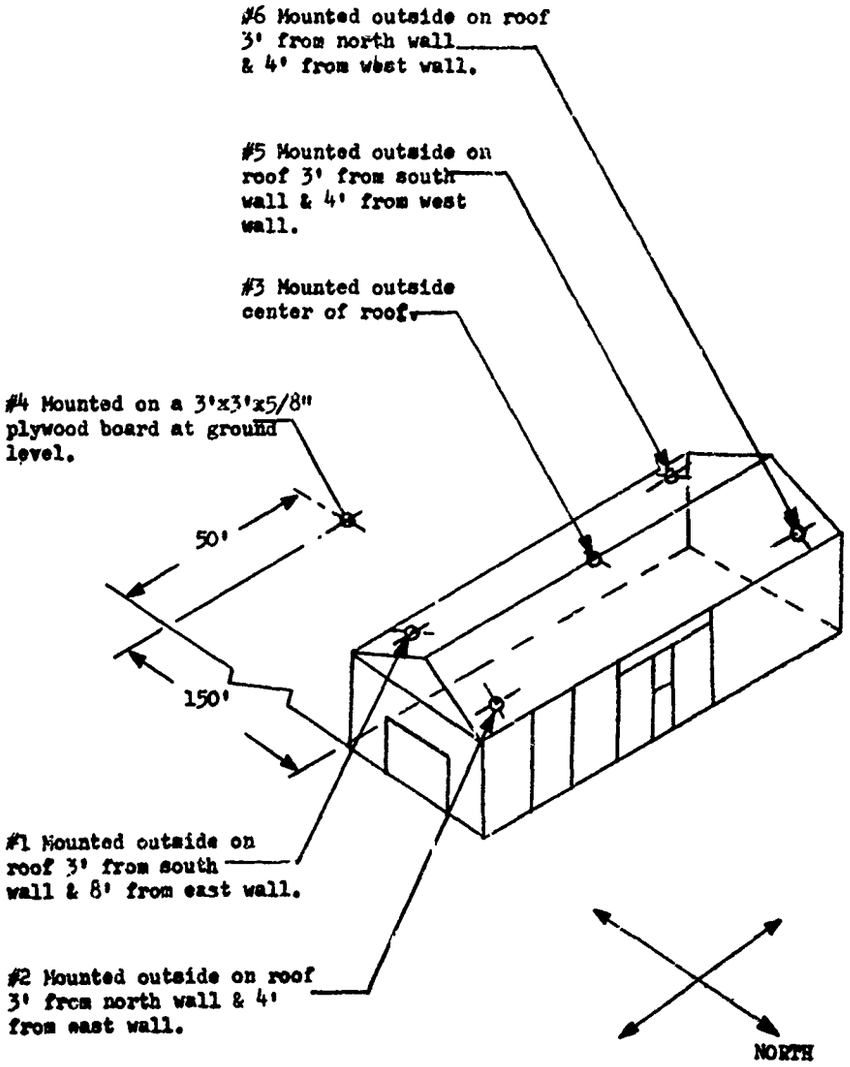
DATE: 2-3-65 Run 1-651 thru 14-664

ENGR.		REVISED	DATE	MICROPHONE LOCATION DIAGRAM	~~PAGE 27~~
CHECK				CONFIGURATION U1	D6-17485
APR				THE BOEING COMPANY RENTON, WASHINGTON	~~PAGE 28~~
PR					

TD 1017-86

FIG. C-48

6-7000



DATE: 2-2-65 Run 1-621 thru 30-650
2-3-65 Run 15-665 thru 30-680

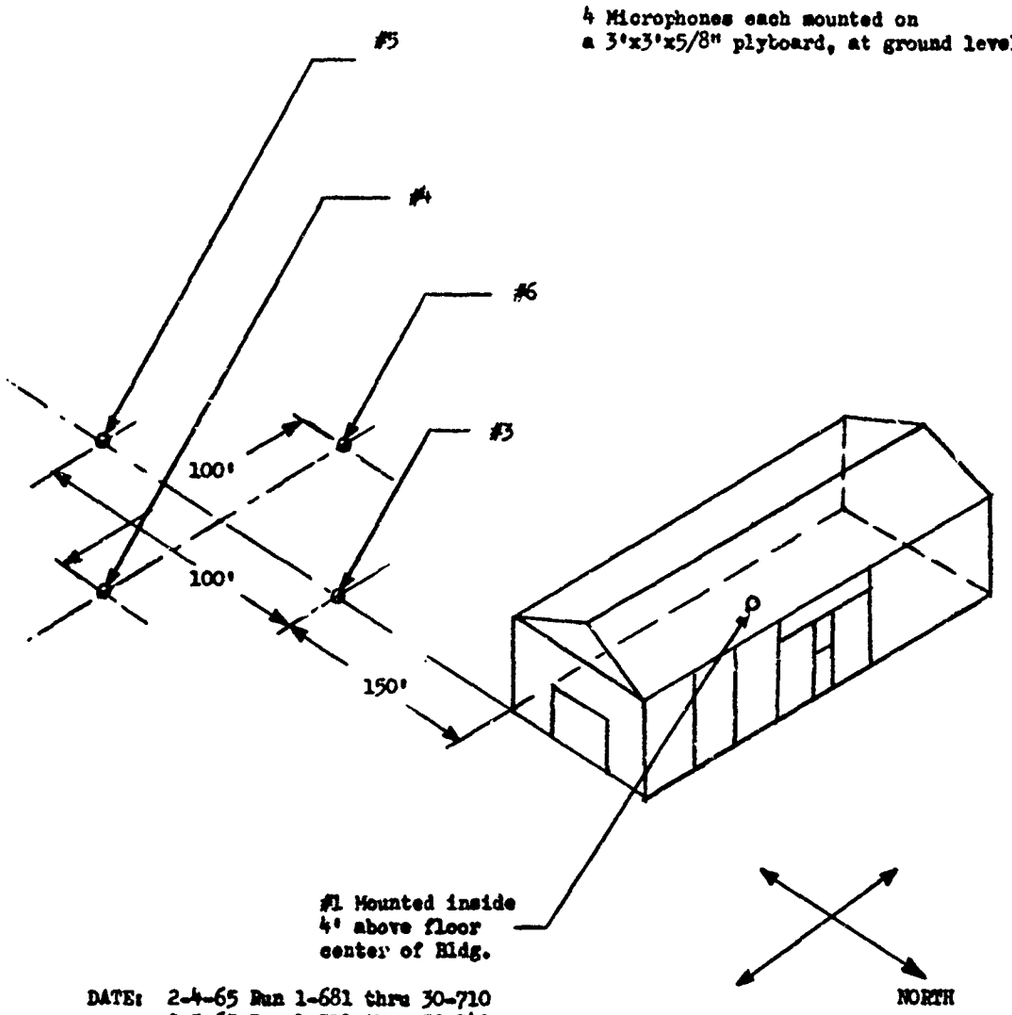
CALC			REVISED	DATE	MICROPHONE LOCATION DIAGRAM CONFIGURATION U2	FIG. 49
CHECK						D6-17485
APR						
APR					THE BOEING COMPANY RENTON, WASHINGTON	PAGE 29

TD 1017 RS

FIG. C-49

6-7000

4 Microphones each mounted on
a 3'x3'x5/8" plyboard, at ground level.



DATE: 2-4-65 Run 1-681 thru 30-710
2-5-65 Run 1-711 thru 30-740
2-6-65 Run 1-741 thru 30-770
2-7-65 Run 1-771 thru 22-792
2-8-65 No Data
2-9-65 Run 1-793 thru 5-797
2-10-65 Run 1-798 thru 6-803

CALC			REVISED	DATE	MICROPHONE LOCATION DIAGRAM CONFIGURATION V	~~FIG. 19~~
CHECK						D6-17485
APR						
APR					THE BOEING COMPANY RENTON, WASHINGTON	PAGE ~~30~~

TD 1017-R9

FIG. C-50

6-7000

Appendix D

LOADING AND RESPONSE DATA

Structural Response Program

Compiled By ______

Date 1-15-65; 1-20-65
House C-1

Phase 2-B				Pressure (p.s.i.)							Acceleration (g)					
1-15-65				Free Field	9	10	11	12	13		7	8	9	10	11	12
Run	Alt	Head	Veh	AV	W Wall UN N	W Wall US N	W Wall LS N	W Wall S N	W Wall LN N		E Wall N Cor E-W	E Wall E Cor N-S	W Wall S Cor E-W	E Wall N Cor N-S	Roof V	Inter Wall N-S
1-1	[illegible]	[illegible]	A		(No Record)						0	.005	0	NR	[illegible]	.165
2-2	[illegible]	1.23	F								0	.006	0		[illegible]	.189
3-3	12.1	1.26	A								2	[illegible]	0		1.950	.106
4-4	12.	1.25	[illegible]								.011	.011	0		1.770	.127
5-5	11.5	1.23	E								.011	.008	0		1.140	.972
6-6	12.	1.26	B								.006	.011	0		1.700	.127
7-7	12	1.26	C								0	.011	.016		1.950	.127
8-8	12.	1.27	G								.006	.008	.016		1.290	.960
9-9	12	1.28	C								.006	.008	.024		2.050	.150
10-10	12.	1.11	D								.011	.008	.008		2.020	.972
11-11	12.	1.23	H								.016	.008	.016		1.150	.102
12-12	12	1.29	D								.011	.011	.008		1.430	.146
13-13	11.9	1.21	E	5.7	2.2	6.0	2.1	2.4	5.5		.011	.011	.016		1.270	.106
14-14	11.9	1.24	B	6.6	2.8	2.7	2.9	2.7	1.8		.006	.008	.008		1.520	1.210
15-15	12.	1.26	E	8.5	7.7	5.9	2.6	8.4	5.5		.011	.008	.008		.964	1.600
16-16	12.	1.26	F	4.1	3.4	3.2	3.2	2.8	1.8		0	.005	.016		.947	.873
17-17	12.	1.25	A	5.6	5.0	3.9	4.0	4.3	3.0		.006	.008	.008		2.500	1.505
18-18	12.	1.25	F	4.7	3.0	3.2	2.4	3.2	1.8		0	.005	.016		.982	1.163
19-19	12.	1.26	G	5.0	2.6	2.2	3.4	3.2	1.8		.011	.005	.024		1.315	1.552

Structural Response Program

Compiled By ______

Date 1-15-65; 1-20-65
House C-1

Phase 2-B				Pressure (p.s.i.)							Acceleration (g)					
1-15-65				Free Field	9	10	11	12	13		7	8	9	10	11	12
Run	Alt	Head	Veh	AV	W Wall UN N	W Wall US N	W Wall LS N	W Wall S N	W Wall LN N		E Wall N Cor E-W	E Wall E Cor N-S	W Wall S Cor E-W	E Wall N Cor N-S	Roof V	Inter Wall N-S
20-20	12.	1.25	C	6.3	4.7	3.9	2.4	2.3	4.8		.006	.008	.016	NR	2.050	.127
21-21	12.	1.28	G	6.1	4.8	3.7	2.6	3.4	2.4		.011	.008	.016		1.060	.795
22-22	11.85	1.26	H	4.3	3.4	2.8	2.8	3.4	1.6		.011	.005	.008		1.948	.678
23-23	11.9	1.26	D	5.6	4.7	5.0	6.5	6.0	4.2		.006	.005	.016		1.770	.662
24-24	12.	1.28	H	9.3	4.3	4.1	4.4	4.4	3.1		.011	.011	.016		2.770	.289
25-25	12.		A	5.1	3.9	3.4	3.5	2.6	2.7		.006	.005	.008		2.720	1.553
26-26	12.5	1.21	E	5.0	3.6	2.7	3.5	3.4	1.9		0	.005	.016		.965	1.116
27-27	11.8	1.26	A	5.1	5.2	2.5	4.1	2.6	3.4		0	.008	.008		2.810	2.013
28-28	12.	1.23	B	5.5	3.6	2.8	2.8	NR	1.8		.006	.008	.008		2.010	1.603
29-29	12.	1.20	E	4.5	3.4	3.2	3.5	3.4	2.1		.006	.005	.008		1.750	.631
End																

D-1

STRUCTURAL RESPONSE PROGRAM

COMPILED BY ______

DATE 1-15-65; 1-20-65

HOUSE C-1

PHASE 2-B 1-16-65				Fire Bird	Pressure (psi) 9	10	11	12	13	Acceleration (g) 7	8	9	10	11	12	
Run	Alt	Hdg	Veh	AV	W Wall UN N	N Wall US N	N Wall LS N	W Wall S N	W Wall LN W	E Wall N Cor E-W	E Wall E Cor N-S	W Wall S Cor E-W	W Wall N Cor N-S	Roof V	Inter Wall N-S	
1-31	11.5	1.21	C		(No	Record	)			0	.003	0	.013	.574	.015	
2-32	11.8	1.23	G	6.1	31	35	38	32	26	.006	.005	.017	.013	.961	.119	
3-33	11.5	1.26	C	6.0	54	66	74	6.8	52	0	.008	.017	.013	1.676	.148	
4-34	12.	1.25	D	6.0	62	70	7.2	62	57	.006	.003	.008	.013	1.352	.090	
5-35	12.	1.25	H	6.0	28	30	32	32	26	.006	.003	.008	.013	1.197	.133	
6-36	12.	1.26	D	6.5	6.3	5.9	72	68	6.3	.006	.003	.017	.013	1.232	.109	
7-37	11.7	1.20	E	6.5	7.4	7.3	8.5	8.5	71	.006	.008	.017	.013	1.352	.114	
8-38	12.	1.21	B	5.6	38	35	3.2	3.2	3.1	.006	.005	.017	.013	1.909	.147	
9-39	12.	1.21	E	6.2	72	61	74	76	55	.006	.005	.017	.013	1.092	.109	
10-40	11.7	1.24	F	6.8	46	49	54	5.2	38	0	.005	.017	.013	1.035	.188	
11-41	11.6	1.26	A	9.0	5.4	51	54	5.2	47	0	.008	[illegible]	[illegible]	2.480	.154	
12-42	12.	1.26	F	5.4	40	40	49	44	35	0	.003	[illegible]	[illegible]	.902	.138	
13-43	12.	1.28	G	7.6	3.2	37	26	NR	25	.006	.005	[illegible]	.026	1.035	.168	
14-44	12.	1.27	C	2.3	5.4	5.7	71	64	47	.006	.008	[illegible]	.013	1.978	.197	
15-45	25	1.35	F	4.0	2.3	26	2.8	2.3	1.5	0	.003	.008	.013	.624	.109	B-5B
16-46	25	1.35	E	5.1	2.3	28	28	26	1.5	.006	.003	.008	.013	.640	.093	B-5B
17-47	25	1.35	F	4.5	3.2	2.8	3.2	32	2.8	0	.003	.008	.026	.504	.109	B-5B
18-48	25	1.35	F	4.0	2.3	2.6	29	2.4	1.5	0	.013	.008	.026	.611	.093	B-5B
19-49	25	1.35	F	2.9	1.8	21	22	2.0	1.5	0	.003	.008	.026	.603	.045	B-5B

STRUCTURAL RESPONSE PROGRAM

COMPILED BY ______

DATE 1-15-65; 1-[illegible]-65

HOUSE C-1

PHASE 2-B 1-16-65				Fire Bird	Pressure (psi) 9	10	11	12	13	Acceleration (g) 7	8	9	10	11	12
Run	Alt	Hdg	Veh	AV	W Wall UN N	N Wall US N	N Wall LS N	W Wall S N	W Wall LN W	E Wall N Cor E-W	E Wall E Cor N-S	W Wall S Cor E-W	W Wall N Cor N-S	Roof V	Inter Wall N-S
20-50	12.	1.24	H	5.5	2.8	2.8	2.9	2.9	2.2	.006	.005	.017	.018	1.376	.114
21-51	11.9	1.23	D	8.7	5.4	57	7.8	72	6.0	.006	.003	.008	.018	1.359	.084
22-52	12.	1.26	H	4.4	1.8	1.9	1.8	1.8	1.5	.006	.003	.008	.018	.942	.054
23-53	12.	1.23	A	5.5	47	3.7	35	36	26	0	.005	.017	.018	1.919	.109
24-54	12.	1.21	E	6.0	40	44	46	41	31	0	.005	.017	.018	1.559	.168
25-55	12.	1.24	A	5.4	3.7	3.8	40	40	2.9	0	.008	.017	.018	1.024	.104
26-56	12.	1.26	B	5.0	3.2	31	31	3.2	26	.006	.005	.017	.018	2.000	.123
27-57	12.	1.27	E	8.3	78	64	7.8	79	59	.012	.008	.025	.018	1.250	.143
28-58	12.	1.28	B	5.8	3.4	26	3.2	30	2.3	.006	.005	.017	.018	1.788	.130
29-59	12.	1.29	C	6.2	5.5	6.4	6.2	6.2	41	.006	.012	.017	.018	2.040	.114
30-60	12.	1.28	G	5.8	31	3.3	32	3.0	21	.006	.005	.005	.018	.067	.109
31-61	12.	1.30	C	6.7	4.7	4.2	4.3	4.6	3.1	.006	.008	.017	.018	2.110	.090
32-62	12.	1.25	D	6.0	6.2	5.4	75	7.5	5.0	.006	.003	.017	.026	1.320	.070
33-63	11.8	1.27	H	4.4	2.3	2.1	26	2.3	1.5	.006	.004	.017	.018	1.170	.078
34-64	11.6	1.26	D	7.6	5.9	6.1	7.2	7.0	47	.006	.003	.017	.018	1.325	.109
End															

Structural Response Program

Compiled By ______ | Date 1-15-65: 1-20-65 | House C-1

Phase 2-B 1-17-65 Run	A.F.	Nom	Vec	Pressure (psi) Free Field AV	9 W Wall LN N	10 N Wall US N	11 N Wall LS N	12 W Wall S N	13 W Wall LN W	Acceleration (g) 7 E Wall N Cor EW	8 S Wall E Cor NS	9 W Wall S Cor EW	10 N Wall N Cor NS	11 Roof V	12 Inter Wall N-S
1-65	11.9	1.20	E	6.1	7.3	7.5	7.0	7.9	7.7	.003	.004	.014	.016	.788	.123
2-66	12.	1.19	B	6.8	3.6	3.0	4.4	3.6	3.7	.003	.004	.009	.016	1.537	.144
3-67	12.05	1.20	E	6.0	5.9	6.3	6.2	6.7	6.1	.013	.004	.009	.016	1.180	.100
4-68	12.	1.22	F	7.0	4.3	4.7	4.8	4.5	4.1	0	.004	.009	.013	1.000	.159
5-69	12.	1.24	A	2.6	4.4	4.2	4.7	4.6	4.7	0	.006	.014	.013	1.950	.198
6-70	12.	1.23	F	6.9	4.9	5.3	5.3	6.0	4.7	0	.004	.009	.006	1.305	.159
7-71	11.9	1.26	G	5.1	3.5	3.7	4.2	3.3	2.9	.007	.004	.009	.013	1.042	.166
8-72	12.	1.24	C	6.6	7.2	8.0	7.8	7.7	6.7	0	.006	.009	.013	1.260	.156
9-73	12.	1.28	G	5.8	3.0	3.0	3.4	2.7	2.5	.007	.004	.009	.013	.941	.144
10-74	11.9	1.25	1	7.5		No	Record			.007	.004	.009	.013	1.140	.127
11-75	12.	1.22	S	5.6			↓			.007	.004	.009	.013	1.423	.079
12-76	12.	1.24	H	5.8	2.6	2.8	2.8	2.7	2.2	.007	.004	.014	.019	.893	.127
13-77	11.8	1.21	A	5.3	5.1	3.7	4.2	4.0	3.2	–	.004	.014	.013	1.789	.159
14-78	11.9	1.20	E	7.3	5.8	6.2	6.2	6.0	4.7	.003	.004	.014	.019	1.176	.247
15-79	12.	1.22	A	4.8	3.7	3.5	3.9	3.7	2.9	0	.004	.014	.013	1.577	.101
16-80	12	1.24	B	5.8	2.9	2.5	2.8	2.7	1.9	.003	.006	.014	.013	1.751	.110
17-81	12.	1.24	E	7.0	6.7	6.3	7.3	7.2	5.3	.007	.006	.014	.013	.947	.154
18-82	12.	1.25	B	6.8	3.6	3.1	3.3	3.3	2.9	.003	.006	.014	.019	1.328	.177
19-83	12.	1.21	C	7.0	6.8	5.8	6.6	7.0	5.8	.003	.006	.009	.013	1.775	.114

Structural Response Program

Compiled By ______ | Date 1-15-65: 1-20-65 | House C-1

Phase 2-B 1-17-65 Run	A.F.	Nom	Vec	Pressure (psi) Free Field AV	9 W Wall LN N	10 N Wall US N	11 N Wall LS N	12 W Wall S N	13 W Wall LN W	Acceleration (g) 7 E Wall N Cor EW	8 S Wall E Cor NS	9 W Wall S Cor EW	10 N Wall N Cor NS	11 Roof V	12 Inter Wall N-S
20-84	12.	1.24	G	5.7	3.0	3.1	3.7	3.0	2.0	.007	.004	.014	.019	1.150	.182
21-85	11.9	1.24	C	6.6	6.1	9.0	8.4	7.5	5.8	.003	.010	.014	.013	1.406	.193
22-86	11.95	1.21	D	3.2	4.0	4.0	4.7	4.5	2.9	.003	.012	.014	.013	1.180	.043
23-87	12.05	1.24	H	5.2	3.0	2.7	3.1	3.1	1.9	.003	.004	.014	.013	1.679	.106
24-88	12.05	1.24	D	8.5	6.2	7.2	7.2	8.2	6.3	.007	.001	.009	.013	1.435	.110
25-89	11.9	1.25	E	5.5	6.3	5.3	6.2	6.4	4.5	.003	.004	.009	.013	1.358	.114
26-90	11.7	1.25	B	6.2	3.2	2.5	3.3	3.0	2.5	.003	.004	.014	.013	1.687	.202
27-91	12.	1.26	E	6.4	7.0	6.3	6.1	7.7	5.1	.007	.006	.014	.013	1.320	.168
28-92	12.	1.20	F	6.9	4.7	4.7	5.6	5.2	2.9	.003	.014	.014	.013	1.190	.195
29-93	12.	1.20	A	8.4	5.2	4.5	5.1	4.9	3.4	.003	.006	.018	.013	1.395	.198
30-94	12.	1.20	F	2.1	4.1	4.5	4.8	4.5	2.9	.003	.004	.014	.013	.936	.180
End															

Structural Response Program

Compiled By______

Date 1-15-65 : 1-20-65
House C-1

Phase 2-A 1-18-65 Run	Alt	Hgt	Vec	Pressure (psf) Free Field Av	9	10	11	12	13	Acceleration (g) 7	8	9	10	11	12
1-95	12.0	1.24	G	5.5	3.2	3.6	3.5	2.9	2.4	.007	.004	.004	.016	1.136	.123
2-96	12.	1.26	C	5.6	4.6	5.9	7.3	6.5	5.4	0	.007	.009	.016	1.579	.118
3-97	12.2	1.25	G	2.4	2.0	2.6	4.3	2.2	2.4	.007	.004	.018	.016	.903	.154
4-98	12.	1.25	[illegible]	4.4	3.7	3.2	3.8	2.4	2.7	.007	.002	.009	.016	1.416	.136
5-99	12.	1.23	D	4.4	5.0	5.2	6.6	6.5	5.4	.027	.002	.009	.007	.912	.061
6-100	11.9	1.25	H	5.1	2.6	3.4	2.2	2.6	8.2	.003	.002	.004	.02	1.249	.092
[illegible]	12.	1.26	B	5.4	4.3	4.1	4.9	4.3	3.8	0	.002	.009	.016	1.645	.179
8-102	12.1	1.22	F	5.8	4.0	4.6	4.9	4.5	3.3	0	.004	.009	.016	1.19	.166
9-103	12.	1.25	A	6.3	3.2	3.9	4.9	4.8	4.4	0	.009	.014	.016	1.722	.197
10-104	11.9	1.21	B	4.8	2.0	3.2	3.2	3.2	2.6	.003	.004	.018	.022	1.962	.175
11-105	12.	1.23	E	5.1	5.3	5.2	5.1	4.3	4.8	.007	.002	.014	.016	1.059	.10[illegible]
12-106	12.	1.23	B	5.3	3.0	2.6	3.2	3.4	2.3	.003	.007	.014	.016	2.0[illegible]	.140
13-1[illegible]	12.	1.25	C	5.6	6.4	7.5	9.5	7.7	6.0	.003	.002	.009	.016	1.560	.157
14-1[illegible]	12.	1.25	G	4.5	2.7	3.6	3.5	3.1	1.8	.007	.004	.014	.016	1.275	.096
15-109	12.	1.27	C	4.7	4.6	5.3	6.3	4.6	4.5	.003	.001	.014	.022	2.023	.105
16-110	12.	1.26	H	5.1	2.0	3.2	3.2	3.1	2.7	.007	.002	.014	.016	2.052	.118
17-111	12.	1.25	D	5.4	6.1	10.0	12.6	9.6	4.5	.007	.002	.014	.016	1.905	.132
18-112	12.	1.29	H	5.1	3.3	3.6	4.4	3.7	3.3	.001	.002	.014	.022	2.155	.192
19-113	11.8	1.20	E	4.5	4.7	5.0	4.7	4.9	3.0	.007	.004	.014	.016	1.100	.065

Structural Response Program

Compiled By______

Date 1-15-65 : 1-20-65
House C-1

Phase 2-B 1-18-65 Run	Alt	Hgt	Vec	Pressure (psf) Free Field Av	9	10	11	12	13	Acceleration (g) 7	8	9	10	11	12
20-114	11.7	1.20	B	6.4	3.7	3.9	3.5	3.7	2.2	.003	.004	.015	.022	2.237	.224
21-115	12.	1.20	E	8.7	6.1	6.0	[illegible]	8.0	6.3	.002	.004	.018	.016	1.241	.157
22-116	12.	1.24	F	5.2	0.9	3.2	3.5	3.4	1.8	.003	.004	.007	.016	1.19[illegible]	.145
23-117	12.1	1.25	A	6.6	4.6	3.9	4.4	4.3	3.3	.003	.007	.018	.016	1.121	.140
24-118	12.	1.25	E	6.2	3.7	5.7	6.0	4.9	2.0	.003	.004	.014	.016	1.250	.188
25-119	12.	1.28	G	6.6	3.3	3.6	4.4	3.1	2.1	.011	.011	.014	.022	1.3[illegible]	.166
26-120	11.9	1.34	C	6.2	5.5	6.8	7.9	7.4	4.5	.002	.001	.025	.022	1.929	.136
27-121	12.1	1.31	G	5.1	2.0	2.2	3.5	2.8	1.5	.007	.002	.014	.016	1.267	.140
28-122	11.8	1.22	D	8.0	7.3	7.8	8.5	8.9	7.3	.003	.004	.014	.016	2.1[illegible]	.155
29-123	12.	1.21	H	5.1	3.0	3.2	3.2	3.4	2.4	.001	.002	.014	.022	1.752	.136
30-124	12.	1.24	D	4.2	4.6	5.5	6.0	5.2	3.6	.003	.002	.018	.016	1.919	.170
End															

STRUCTURAL RESPONSE PROGRAM

COMPILED BY _____

DATE 15-1-20-65
HOUSE C-1

PHASE 2-B				PRESSURE (PSI)						ACCELERATION (g)							
1-19-65				Free Field	9	10	11	12	13	7	8	9	10	11	12		
RUN	ALT	HEAD	VAC		WALL LN N	WALL US W	WALL LS N	WALL S N	WALL LN W	E WALL NCOR E N	S WALL ECOR N S	N WALL ECOR S W	N WALL NCOR W S	ROOF V	INTER WALL N-S		
1-125	12	125	F	6.4	5.1	6.4	5.1	4.1	4.1	.003	.002	.018	.014	2.0	.166		
2-126	28B	142	F	2.0	1.3	1.4	1.6	1.6	1.2	.002	.002	.014	.014	.592	.028		
3-127	30	143	A	2.2		No	Record			0	.005	.009	.002	.402	.043		
4-128	12	126	B	6.1						.002	.008	.018	.014	1.014	.146		
5-129	12	125	E	4.8						.001	.008	.014	.014	.846	.097		
6-130	11	135	B	5.2						.003	.008	.018	.014	1.493	.115		
7-131	12	125	C	6.2	5.9	7.1	8.2	6.9	6.2	.002	.008	.018	.022	1.405	.155		
8-132	12	126	G	6.0	5.4	3.6	4.6	3.4	2.6	.027	.005	.014	.022	1.666	.164		
9-133	12	129	C	8.1	5.3	6.1	6.9	6.6	5.9	.003	.006	.014	.022	1.748	.155		
10-134	12	125	D	6.9	4.7	5.3	6.6	5.3	4.7	.001	.005	.009	.014	1.265	.166		
11-135	11	129	H	5.0	2.2	2.1	3.0	2.5	1.8	.007	.003	.009	.014	1.180	.128		
12-136	11B	124	D	6.5	3.4	3.6	4.2	6.4	5.6	.001	.005	.014	.014	.117	.119		
13-137	25A	133	F	5.7	1.6	3.2	3.0	2.8	1.5	.003	.002	.009	.007	.797	.049		13-58
14-138	25A	129	F	3.4	1.9	2.8	3.3	2.5	"	.003	.002	.009	.007	.446	.020		13-58
15-139	11.6	122	E	10.8	5.0	8.6	8.2	5.6	7.4	.001	.008	.018	.022	1.285	.195		
16-140	25A	133	F	5.7	1.9	3.2	5.3	2.5	1.5	.003	.002	.009	.007	.564	.040		13-58
17-141	12.	125	B	5.1	2.8	2.8	3.0	2.8	2.1	.003	.008	.014	.022	1.264	.115		
18-142	25	135	F	3.1	2.2	2.5	2.6	2.5	1.5	.002	.002	.009	.014	.502	.049		13-58
19-143	12.	122	E	6.0	5.9	3.7	6.2	6.2	4.7	.002	.005	.014	.014	1.255	.097		

STRUCTURAL RESPONSE PROGRAM

COMPILED BY _____

DATE 15-1-20-65
HOUSE C-1

PHASE 2-B				PRESSURE (PSI)						ACCELERATION (g)							
1-19-65				Free Field	9	10			13	7	8	9	10	11	12		
RUN	ALT	HEAD	VAC		WALL LN N	WALL US W	WALL LS N	WALL S N	WALL LN W	E WALL NCOR E N	S WALL ECOR N S	N WALL ECOR S W	N WALL NCOR W S	ROOF V	INTER WALL N-S		
20-144	25	135	F	3.5	1.9	2.1	2.6	1.9	1.5	0	.002	.009	.007	.846	.052		13-58
21-145	30	140	E	2.0	0.9	1.1	1.3	0.9	0.6	0	.002	.004	.007	.427	.021		
22-146	30	13	F	1.4	0.9	0.7	1.0	0.6	0.3	0	0	0	0	.264	.018		
23-147	30	14	F	2.2	0.9	1.1	1.0	0.9	0.6	0	.002	.004	.007	.370	.043		
24-148	12.	128	A	5.6	3.7	3.6	4.3	3.7	2.2	.003	.008	.014	.014	1.668	.190		
25-149	11.9	121	G	5.1	3.1	3.6	3.6	3.1	1.8	.010	.005	.018	.014	1.354	.101		
26-150	12.1	121	C	5.9	4.7	5.3	6.6	5.6	3.8	.002	.008	.018	.022	1.670	.097		
27-151	12	122	G	6.7	3.4	3.9	4.6	3.4	2.4	.001	.005	.018	.014	1.524	.126		
28-152	12.	125	H	4.4		No	Record			.003	.004	.009	.007	1.255	.061		
29-153	12.	125	D	6.4	6.9	7.1	9.5	8.4	5.9	.001	.006	.009	.014	1.368	.132		
30-154	12.	125	H	5.4	1.6	2.8	3.0	3.1	1.5	.001	.005	.014	.014	1.317	.110		
31-155	12.	120	A	6.7	3.4	2.6	5.3	3.1	2.6	.001	.005	.018	.014	1.904	.150		
32-156	12.	123	F	5.4	4.7	5.3	6.2	5.3	2.5	.002	.008	.022	.022	1.674	.116		
33-157	12.	125	A	6.4	4.1	4.3	4.6	4.7	3.5	.002	.011	.018	.018	1.815	.064		
End																	

STRUCTURAL RESPONSE PROGRAM

COMPILED BY ______

DATE 1-15-65 : 1-24-65
HOUSE C-1

PHASE 2-B 1-20-65 RUN	ALT	HDG	VEC	Pressure (psf) Free Field AV	9 W.Wall UN N	10 W.Wall US N	11 W.Wall LS N	12 W.Wall ¢ N	13 W.Wall LN W	Acceleration (g) 7 E.Wall N.Cor EN	8 S.Wall E.Cor N-S	9 W.Wall S.Cor E-W	10 N.Wall N.Cor N-S	11 Roof V	12 Inter Wall N-S
1-158	1.8	126	B	5.7	3.1	3.7	3.5	1.9	2.2	.003	.005	.014	.007	1.761	.111
2-159	12.	1.28	C	1.04		No Rec	ord			.003	.008	.014	.014	1.578	.183
3-160	12.	13	G	2.4						.010	.005	.018	.022	1.415	.314
4-161	12.	13	C	53						.003	.014	.019	.022	1.5[illegible]	.081
5-162	30	1.4	E	2.0	1.2	1.5	1.6	1.2	0.9	0	.002	.014	.007	.042	.045
6-163	30	1.3	F	1.6	1.2	1.5	1.3	0.9	0.3	0	.002	.004	.007	.020	.013
7-164	46	1.4	F	0.9	0.6	1.1	0.9	0.6	0.3	0	.002	.004	0	.038	.009
8-165	11.9	121	D	4.5	4.1	3.7	4.1	4.7	2.9	.002	.002	.009	.007	.986	.026
9-166	13.1	126	H	2.8	3.1	3.3	3.2	2.6	2.9	.007	.005	.014	.014	1.291	.215
10-167	12	124	D	4.7	4.7	4.4	5.4	5.0	4.1	.002	.005	.009	.007	1.098	.054
11-168	11.9	134	E	3.3	6.5	8.6	10.1	10.8	8.7	.010	.005	.014	.022	1.27[illegible]	.197
12-169	12	130	B	8.1	3.4	3.3	3.2	3.1	3.2	.003	.005	.018	.014	1.522	.124
13-170	11.5	130	E	4.1	5.0	4.4	5.1	5.0	4.1	.003	.005	.014	.007	1.136	.063
14-171	12.	1.28	E	4.7	3.1	3.7	3.5	3.4	2.6	.002	.005	.014	.014	.899	.108
15-172	12	1.28	A	5.5	4.4	4.4	5.1	4.7	4.4	.003	.008	.014	.014	1.750	.156
16-173	12.1	130	F	4.7	3.4	3.7	4.1	3.7	2.9	.003	.005	.014	.014	.843	.143
17-174	12.	1.25	G	5.5	3.1	3.7	4.8	3.7	2.6	.007	.005	.021	.029	1.135	.090
18-175	12	130	C	5.6	4.2	5.9	7.9	4.7	5.8	.003	.005	.014	.014	1.405	.022
19-176	12.	1.26	G	7.8	2.4	3.7	4.1	3.1	2.9	.007	.005	.018	.022	1.308	.147
C.J															

STRUCTURAL R[illegible]SE PROGRAM

COMPILED BY ______

DATE 1-15-65 : 1-24-65
HOUSE C-1

PHASE 2-B 1-21-65 RUN	ALT	HDG	VEC	Pressure (psf) Free Field AV	9 W.Wall UN N	10 W.Wall US N	11 W.Wall LS N	12 W.Wall ¢ N	13 W.Wall LN W	Acceleration (g) 7 E.Wall N.Cor EN	8 S.Wall E.Cor N-S	9 W.Wall S.Cor E-W	10 N.Wall N.Cor N-S	11 Roof V	12 Inter Wall N-S
1-177	12	1.30	H	5.2	3.1	3.7	3.8	3.4	3.0	.003	.003	.004	.007	1.310	.147
2-178	12.	1.26	D	4.1	6.0	6.5	7.8	6.2	6.0	.003	0	.004	.007	.945	.086
3-179	12.	130	H	6.5	3.8	4.1	4.9	4.1	3.9	.007	.003	.013	.014	1.621	.188
4-180	12.	1.30	A	6.7	5.0	4.8	6.2	5.0	5.1	0	0	.017	.026	1.937	.205
5-181	12.	131	E	4.6	4.4	4.8	5.5	4.7	4.2	0	0	.013	.022	.692	.165
6-182	12.	130	A	4.4	4.7	4.1	4.9	4.7	4.5	.2	0	.017	.022	1.579	.161
7-183	12.1	1.30	B	5.3	4.1	3.7	3.6	3.8	2.6	.003	.003	.022	.026	1.910	.319
8-184	12.1	1.30	E	4.8	5.3	5.6	5.5	6.2	5.1	.003	0	.013	.014	.843	.134
9-185	12.1	1.30	B	4.3	3.8	4.0	3.2	3.1	3.0	.003	.028	.017	.022	1.730	.165
10-186	12.0	130	C	5.6	5.0	5.6	1.8	6.2	6.9	0	0	.026	.036	1.741	.255
11-187	12.	134	G	4.2	3.1	3.7	3.8	3.1	3.1	.007	.020	.022	.026	1.056	.147
12-188	12.	1.3[illegible]	C	NR	6.2	7.5	6.1	7.8	6.0	0	.017	.017	.022	1.265	.152
13-189	25.	136	E	[illegible]	2.2	1.6	2.9	2.2	1.5	0	0	.004	.007	.756	.065
14-190	12.	1.29	D	5.3	5.6	5.6	7.8	7.5	6.0	.003	0	.009	.014	1.155	.134
15-191	25.	1.30	A	2.9	3.1	3.2	2.6	3.0	1.6	0	0	.009	.007	1.305	.081
16-192	12.	1.31	H	3.5	2.8	1.6	3.2	2.5	2.1	.003	0	.004	.001	1.064	.098
17-193	25.	134	F	NR	2.8	3.3	3.2	1.8	1.8	.003	0	.004	.007	1.011	.081
18-194	12.	1.30	D	4.8	1.2	1.2	7.8	1.2	1.0	.007	0	.009	.014	1.304	.134
19-195	25.	1.[illegible]	A	[illegible]	2.1	2.3	2.2	2.1	2.2	0	0	.009	.014	1.4[illegible]	.075

Structural Response Program

Compiled By ______

Date 1-15-65 : 1-21-65
House C-1

Phase 2-B				Pressure (psf)						Acceleration (g)						
1-21-65				Far Field	9	10	11	12	13	7	8	9	10	11	12	
Run	Alt	Mach	Vic	AV	N Wall LN N	N Wall US N	N Wall LS N	N Wall C N	N Wall LN W	E Wall N Cor EN	S Wall E Cor N-S	N Wall S Cor EW	N Wall N Cor NS	Roof V	Inter Wall N-S	
20-196	25	1.31	F	.6	2.5	1.6	1.9	1.9	1.5	0	0	.004	.007	.731	.075	B-58
21-197	25	1.35	A	2.5	2.8	2.6	2.6	2.8	1.8	0	0	.009	.007	1.247	.049	B-58
22-198	25	1.36	F	2.2	2.5	3.0	3.2	2.6	1.8	0	0	.009	.007	.888	.116	B-58
23-199	21	1.31	E	4.8	6.6	5.6	6.8	7.5	7.0	.003	.003	.013	.022	1.061	.165	
24-200	12.	1.30	B	4.9	4.1	3.3	3.2	3.4	3.0	.003	.005	.017	.014	2.042	.201	
25-201	12	1.30	E	5.3	7.8	7.1	8.1	7.8	7.0	.002	.003	.017	.022	1.075	.138	
26-202	25.	1.35	F	4.6	3.4	4.1	3.0	3.6	3.0	0	.003	.009	.014	.924	.138	B-58
27-203	12.1	1.30	D	4.4	6.2	7.5	8.4	6.9	5.5	.003	.003	.009	.014	1.285	.170	
28-204	25	1.32	A	NR	(No	Record)				.003	.003	.004	.014	1.186	.116	B-58
29-205	12	1.30	A	3.7	2.5	2.6	3.2	2.6	1.8	0	0	.004	.007	.700	.054	
30-206	25.	1.33	F	2.8	2.5	2.6	2.9	4.1	1.5	0	0	.009	.014	1.330	.111	B-58
31-207	26.5	1.33	A	2.8	3.1	2.6	3.2	3.1	2.6	.003	.003	.009	.014	1.500	.276	B-58
32-208	25.5	1.35	E	NR	4.1	5.6	5.5	4.4	3.2	0	0	.009	.014	1.200	.058	B-58
33-209	26.5	1.32	A	2.6	2.2	2.2	2.6	1.9	NR	.018	.003	.017	.029	2.150	.188	B-58
34-210	12.	1.33	H	8.5	4.1	3.7	5.2	4.7	3.0	.003	0	.009	.014	1.162	.165	
35-211	25.3	1.34	E	3.1	3.1	3.7	3.6	3.1	2.6	.002	0	.009	.014	1.229	.086	B-58
36-212	12.	1.28	D	3.6	4.7	5.6	5.5	5.6	3.9	0	0	.009	.014	1.286	.081	
37-213	25	1.36	A	2.9	1.9	2.2	3.2	3.1	2.1	.003	.003	.009	.014	1.201	.156	B-58
39-215	25.	1.34	E	NR	3.1	3.7	4.2	3.1	1.8	.010	.003	.017	.022	1.045	.125	B-58

Structural Response Program

Compiled By ______

Date 1-15-65 : 1-21-65
House C-1

Phase 2-B				Pressure						Acceleration					
1-21-65					9	10	11	12	13	7	8	9	10	11	12
Run	Alt	Mach	Vic	AV	N Wall LN N	N Wall US N	N Wall LS N	N Wall C N	N Wall LN W	E Wall N Cor EN	S Wall E Cor N-S	N Wall S Cor S-W	N Wall N Cor NS	Roof V	Inter Wall N-S
40-216	12	1.30	G	6.0	3.4	4.1	4.5	3.4	2.6	0	0	.026	.029	1.915	.152
41-217	11.0	1.28	C	5.2	4.7	5.6	6.5	6.2	3.9	.007	.003	.013	.014	1.257	.152
42-218	12.	1.31	G	5.2	3.1	3.7	3.6	3.1	2.6	.007	.003	.009	.014	1.808	.312
43-219	12.	1.31	H	7.9	3.4	3.7	4.9	3.8	3.0	.007	0	.009	.014	1.193	.152
44-220	11.9	1.30	D	4.8	6.2	5.4	7.5	6.2	4.5	.007	.003	.013	.014	1.581	.183
45-221	11.7	1.31	H	8.8	3.1	3.7	3.8	3.1	2.6	(No	Record)				
End															

STRUCTURAL RESPONSE HISTORY

COMPILED BY _____

DATE 15-45:1-24-65

HOUSE C-1

PHASE 2-B

1-22-65

RUN	TIME	ITEM	VEL	FREE FIELD	PRESSURE (psf) 9	10	11	12	13	ACCELERATION (g) 7	8	9	10	11	12
				AV	WALL LIN N	WALL US N	WALL LS N	WALL S	WALL LN W	EWALL NCOR S.N	EWALL ECOR N.S	WALL SCOR S.W	WALL NCOR N.S	ROOF V	INTER WALL N-S
1-222	12	130	A	NR	3.4	4.1	2.2	5.0	6.2	1	NO	RECORD			
2-223	12	131	F	2.5	3.1	2.9	3.5	2.8	2.8	0	.002	.005	.007	.032	.084
3-224	12	128	A	4.6	4.1	3.7	2.8	3.8	3.4	0	.006	.014	.016	.471	.026
4-225	12	127	B	10.7	5.9	3.7	2.8	3.4	4.3	.003	.006	.018	.022	.261	.146
5-226	12	126	E	10.9	5.0	8.1	9.2	10.2	8.0	.003	.006	.014	.022	.115	.146
6-227	12	127	A	2.1	2.2	1.9	2.9	2.8	1.8	0	.004	.009	.007	.829	.058
7-228	12.9	1.4	C	4.3	4.4	5.2	5.1	5.3	3.4	.003	.008	.014	.022	.029	.065
8-229	12	131	G	3.1	3.1	2.1	3.5	3.1	1.8	.003	.004	.009	.016	.995	.119
9-230	12.1	133	C	7.1	5	3.7	6.4	4.7	4.6	0	.004	.005	.016	.293	.058
10-231	30-31	1.4	E	1.6	1.6	1.5	1.6	1.6	0.9	0	.002	.005	.007	.047	.046
11-232	30-32	1.4	A	1.6	2.2	1.8	1.6	1.9	1.5	0	.002	.005	.007	.082	.058
12-233	30-33	1.4	E	2.2	2.9	1.5	1.3	1.2	0.6	0	.002	.005	.007	.029	.022
13-234	30-34	1.4	A	5.9	2.5	1.8	2.2	2.5	2.6	.003	.006	.009	.014	.526	.065
14-235	1.49	1.35	E	4.5	(N/A - Re	cord)				.003	.006	.014	.014	.817	.158
15-236	1.49	1.35	B	5.9	4.2	3.7	4.3	3.9	3.5	.003	.008	.018	.022	.982	.169
16-237	12.9	131	C	4.4	4.7	4.4	5.0	6.2	4.0	.003	.006	.009	.014	.050	.127
17-238	12.	129	F	6.2	3.1	3.7	3.5	3.1	2.5	.003	.004	.009	.014	.560	.127
18-239	1.0	1.30	A	3.9	3.2	3.3	3.2	3.1	2.6	0	.004	.007	.014	.810	.058
19-240	1.0	1.35	F	1.2	6.5	6.0	6.7	5.0	4.5	.003	.004	.014	.022	.749	.226

STRUCTURAL RESPONSE PROGRAM

COMPILED BY _____

DATE 15-45:1-24-65

HOUSE C-1

PHASE 2-B

1-24-65

RUN	TIME	ITEM	VEL	FREE FIELD	PRESSURE (psf) 9	10	11	12	13	ACCELERATION (g) 7	8	9	10	11	12
				AV	WALL LIN N	WALL US N	WALL LS N	WALL S	WALL LN W	EWALL NCOR S.N	EWALL ECOR N.S	WALL SCOR S.W	WALL NCOR N.S	ROOF V	INTER WALL N-S
20-241	1.6	1.41	G	2.1	1.6	2.2	2.4	1.7	1.4	.002	.002	.009	.014	1.02	.029
21-242	1.65	1.41	C	1.4	1.2	1.6	1.3	0.9	0.8	0	.002	.009	.007	.207	.086
22-243	2.0	1.2	G	0.9	0.6	0.7	0.6	0.6	0.6	0	.006	.005	0	.045	.015
23-244	30-21	1.4	E	2.6	1.6	2.0	2.9	1.6	1.4	0	.002	.005	.007	.826	.029
24-245	30-29	1.4	A	2.1	1.6	1.6	1.4	1.2	1.2	0	.006	.005	.007	.029	.086
25-246	30-35	1.6	F	4.6	0.6	1.8	2.9	2.0	1.5	0	.006	.005	.007	.661	.211
26-247	30-25	1.6	A	1.5	1.2	0.7	0.8	1.2	1.2	0	0	.005	.007	.792	.086
27-248	25	1.41	A	1.5	0.5	0.6	0.6	0.8	0.6	0	.001	.005	.007	.581	.035
28-249	25	1.4	F	2.4	1.2	1.5	2.1	1.9	1.5	0	.004	.005	.007	.263	.046
29-250	25	1.4	A	1.6	1.6	1.5	1.6	1.6	1.4	0	.002	.005	.007	.816	.058
30-251	24.9	1.4	F	2.3	1.2	1.6	1.6	1.4	1.2	0	.002	.002	.007	.026	.034
31-252	25	1.5	B	0.6	0.6	0.9	1.1	1.2	0.6	0	0	0	0	.008	.811
32-253	25	1.4	E	1.6	1.6	1.5	1.3	1.6	1.4	0	0	.005	0	.021	.023
33-254	25	1.5	B	NR	0.6	1.1	1.1	0.9	0.3	0	[illegible]	.005	0	.021	.058
End															

Structural Response Program

Compiled By ______

Date [illegible]

House C-1

Phase 2-B 1-23-65 Run	Alt	Head	Veh	Pressure (psf) Free Field AV	9	10	11	12	13		Acceleration (g) 7	8	9	10	11	12	
1-255	1.9	1.25	C	NR	6.0	7.5	10.8	2.3	NR		.003	.001	.009	.014	1.408	.093	
2-256	11.9	1.25	G	6.9	3.3	2.3	4.0	2.0	2.2		.002	.004	.009	.014	.924	.143	
3-257	11.93	1.29	C	4.6	5.5	[illegible]	7.2	5.7	4.9		.002	.007	.009	.007	1.889	.081	
4-258	11.3	1.30	D	4.2	5.5	5.4	6.8	7.1	5.6		.003	.002	.005	.007	1.174	.086	
5-259	12.	1.29	H	6.0	3.0	2.4	3.4	3.0	2.6		.002	.002	.005	.007	1.118	.134	
6-260	12	1.30	D	3.1	5.7	5.9	6.5	6.2	4.7		.002	.002	.009	.014	1.347	.122	
7-261	12.	1.28	E	6.7	9.1	6.8	9.3	10.2	7.7		.003	.007	.018	.014	1.152	.129	
8-262	12.	1.27	B	4.3	3.0	3.3	3.1	2.8	2.5		.003	.001	.014	.007	1.278	.113	
9-263	12.	1.28	E	2.9	3.2	2.6	3.2	2.6	2.6		.002	.004	.009	.001	.979	.060	
10-264	12.	1.30	B	2.7	2.8	2.3	2.7	2.2	2.1		0	.004	.009	[illegible]	1.29	.066	
11-265	11.9	1.30	F	4.9	5.2	4.9	5.1	4.4	4.1		0	.007	.009	.001	1.180	.229	
12-266	11.9	1.31	A	4.0	3.2	3.8	3.4	3.2	2.7		0	.007	.014	.014	1.822	.116	
13-267	11.9	1.30	F	3.1	2.2	2.6	3.5	2.7	1.8		0	.004	.009	.001	.549	.054	
14-268	25.	1.36	F	2.0	1.9	2.3	2.6	2.4	1.5		0	.002	.005	.001	.476	.041	B-58
15-269	12.	1.25	G	3.1	2.8	2.6	3.4	2.2	1.6		.002	.004	.009	.007	1.156	.095	
16-270	25.	1.35	A	NR	4.3	3.7	4.3	4.0	2.8		0	.009	.009	.001	1.276	.054	B-58
17-271	12.1	1.29	G	3.8	4.4	5.4	6.1	4.7	3.7		.003	.001	.009	.014	1.089	.098	
18-272	25	1.34	F	4.1	3.2	3.7	4.0	3.5	2.9		0	.004	.014	.014	.281	.122	B-58
19-273	12.	1.26	G	5.7	4.0	4.4	4.8	4.3	2.6		.007	.007	.018	.024	1.448	.197	

Structural Response Program

Compiled By ______

Date [illegible]

House C-1

Phase 2-B 1-23-65 Run	Alt	Head	Veh	Pressure (psf) Free Field AV	9	10	11	12	13		Acceleration (g) 7	8	9	10	11	12	
20-274	25.	1.34	A	2.7	2.4	2.3	2.7	2.4	1.6		0	.004	.005	.001	1.380	.059	B-58
21-275	25	1.35	E	2.8	2.5	2.6	2.9	2.7	1.6		0	.004	.005	0	.256	.032	B-58
22-276	25.	1.36	A	2.6	2.9	2.1	2.2	2.5	1.8		0	.004	.009	.001	1.211	.054	B-58
23-277	25.	1.36	F	2.3	1.7	1.7	1.8	1.9	1.2		0	.004	.005	0	[illegible]	.032	B-58
24-278	24.6	1.35	A	3.1	2.5	2.3	2.6	2.7	2.2		0	.001	.009	.001	1.330	.054	B-58
25-279	12.	1.26	H	5.2	3.3	2.8	3.4	3.2	2.5		.006	.004	.014	.014	1.554	.140	
26-280	12	1.31	D	5.2	6.3	5.2	7.1	6.3	5.0		.006	.004	.009	.014	.898	.113	
27-281	12.	1.28	H	7.1	3.5	3.5	4.5	3.8	2.9		.006	.004	.009	.014	[illegible]	.113	
28-282	12.	1.28	D	12.7	14.2	13.8	14.9	15.8	14.2		.010	.004	.018	.019	1.544	.165	
29-283	25.	1.36	E	2.9	2.8	2.1	2.7	2.8	1.5		0	[illegible]	[illegible]	.001	.652	.050	B-58
30-284	25.	1.36	A	2.1	2.2	1.7	1.9	1.9	1.5		0	.002	.005	.001	.925	[illegible]	B-58
31-285	12	1.29	B	3.3	2.8	2.8	3.2	2.6	2.9		[illegible]	.004	.009	.014	1.829	.066	
32-286	25.	1.36	F	2.6	2.2	1.7	2.9	1.9	1.5		0	[illegible]	[illegible]	[illegible]	[illegible]	.041	B-58
33-287	20.5	1.39	E	6.6	9.1	7.2	8.0	9.4	8.8		[illegible]	.009	.014	[illegible]	1.216	[illegible]	
34-288	25.	1.37	A	2.1	2.2	[illegible]	[illegible]	2.2	1.5		0	.002	.005	.007	1.012	[illegible]	B-5[illegible]
35-289	12.	1.29	B	4.2	2.8	3.1	3.2	[illegible]	2.6		[illegible]	.001	.014	.007	1.441	.121	
36-290	25.	1.32	E	2.9	1.6	1.9	1.6	1.3	0.9		0	[illegible]	[illegible]	.001	[illegible]	[illegible]	B-5[illegible]
37-291	25.	1.37	A	4.4	3.2	2.8	2.2	3.5	2.7		[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	B-[illegible]
38-292	25.	1.36	F	2.1	1.8	[illegible]	4.5	2.2	1.9		[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	.104	B-[illegible]

STRUCTURAL RESPONSE PROGRAM

COMPILED BY ____

DATE 1-5:1-20-65
HOUSE C-1

PHASE 2-B				PRESSURE							ACCELERATION					
1-22-65					9	10	11	12	13		7	8	9	10	11	12
RUN	ALT	HDG	VEL	AV	WALL UN N	WALL US N	WALL LS N	WALL S N	WALL LN W		E WALL W COR E/W	E WALL E COR N S	WALL G COR E/W	WALL W COR N S	Accel V	INTER WALL N-S
59-293	12	165	C	43	5.7	5.2	6.1	6.1	4.1							
60-294	25	137	A	29	3.2	3.5	4.2	4.1	2.9		0					13.68
61-295	12	130	G	3.1	1.3	1.0	1.2	0.9	0.6							
62-296	25	131	F	23	2.5	2.1	2.9	2.5	1.5		0					13.59
63-297	12	125	C	22	7.0	7.6	9.5	7.9	6.5							
64-298	12	126	G	1.3	6.3	6.2	6.1	6.3	4.4							
65-299	12	126	H	3.7	3.2	3.1	3.2	3.2	1.8							
66-300	12	125	I	2.8	4.4	4.2	4.8	4.1	3.2							
67-301	12	126	H	2.1	2.8	1.7	2.2	2.8	1.5							
68-302	12	129	E	42	4.4	4.9	6.1	6.3	5.9							
69-303	12	130	B	42	3.5	3.1	3.2	3.2	2.6							
70-304	12	130	C	46	7.9	6.2	7.3	7.9	5.6							
End																

STRUCTURAL RESPONSE PROGRAM

COMPILED BY ____

DATE 1-5:1-20-65
HOUSE C-1

PHASE 2-B				PRESSURE (PSF)							ACCELERATION (g)					
1-24-65				Free Field	9	10	11	12	13		7	8	9	10	11	12
RUN	ALT	HDG	VEL	AV	WALL UN N	WALL US N	WALL LS N	WALL S W	WALL LN W		E WALL W COR E/W	E WALL E COR N S	WALL G COR E/W	WALL W COR N S	Accel V	INTER WALL N-S
1-305	12	---	F	44	(NO Record)											
2-306	12	123	A	46												
3-307	12	120	F	42												
4-308	12.5	125	A	3.8												
5-309	12	124	G	49												
6-310	12	124	C	44												
7-311	12	120	G	45												
8-312	12	120	C	44												
9-313	12	125	A	48												
10-314	12	125	V	50												
11-315	12	125	A	42												
12-316	12	129	V	45												
13-317	12	124	A	44												
14-318	12	---	F	43												
15-319	12	126	A	3.6												
16-320	12	121	C	6.1												
17-321	12	126	C	3.1												
18-322	12.5	126	C	4.1												
19-323	12	126	C	2.9												

STRUCTURAL RESPONSE PROGRAM

COMPILED BY _____

DATE 1-5-65 : 1-14-65

HOUSE C-1

PHASE 2-B				PRESSURE (psf)						ACCELERATION (g)					
1-24-65				Free Field	9	10	11	12	13	7	8	9	10	11	12
RUN	ALT	WIND	VEL	AK											
20-324	12	1.23	C	6.1						.003	.001	.014	.014	2.170	.232
21-325	12	1.23	G	5.4						.003	.001	.014	.014	2.112	.160
22-326	12	1.24	C	NR						.003	.004	.009	.014	1.590	.102
23-327	12	1.24	G	4.3						.002	.001	.014	.014	1.210	.147
24-328	12	1.20	H	7.4						.010	.004	.014	.014	1.955	.291
25-329	12	1.21	D	4.6						.001	.001	.014	.014	1.140	.098
26-330	12	1.21	H	NR						.001	.001	.014	.014	1.257	.102
27-331	12	1.20	D	6.5						.002	.001	.014	.014	1.445	.124
28-332	12	1.21	E	4.6						.003	.004	.014	.014	1.035	.169
29-333	12	1.24	B	2.8						.003	.004	.009	.022	1.932	.142
30-334	12	1.23	E	8.1						.007	.001	.023	.029	1.174	.268
31-335	12	1.25	B	4.1						.003	.002	.005	.007	.857	.095
32-336	129	1.20	F	4.2						.002	.002	.014	.014	1.092	.147
33-337	12	1.2	A	NR						0	.002	.005	.007	.969	.054
34-338	12	1.21	F	NR						.003	.002	.005	.014	.819	.160
35-339	12	1.21	A	2.9						.002	.002	.005	.007	1.788	.085
36-340	12	1.21	G	3.0						.007	.004	.014	.014	1.539	.085
37-341	12	1.20	C	4.9						.003	.002	.009	.029	2.092	.169
38-342	12	1.22	G	4.4						.003	.002	.005	.007	1.445	.083
39-343	12	1.22	C	3.9						.003	.001	.018	.022	1.100	.090

STRUCTURAL RESPONSE PROGRAM

COMPILED BY _____

DATE 2-1-65 : 2-3-65

HOUSE C-1

PHASE 2-B				DISPLACEMENT (in)					
2-1-65				Free Field	1/2	2	3	4	5
RUN	ALT	WIND	VEL	AK					
1-590	12	1.24	G	5.2	.516	.130	.100	.081	.042
2-591	12	1.25	C	NR	.102	.200	.137	.151	.069
3-592	129	1.25	G	4.0	.063	.125	.087	.071	.042
4-593	129	1.24	H	5.2	.100	.187	.137	.121	.056
5-594	205	1.25	D	4.5	.075	.150	.100	.111	.056
6-595	205	1.25	H	5.1	.081	.150	.125	.106	.042
7-596	208	1.20	A	4.6	.127	.237	.162	.194	.098
8-597	205	1.23	F	4.8	.089	.150	.125	.101	.049
9-598	205	1.22	A	3.9	.107	.225	.152	.161	.096
10-599	205	1.21	B	5.2	.114	.229	.162	.151	.209
11-600	12	1.23	E	NR	.076	.125	.087	.096	.042
12-601	205	1.26	B	8.0	.140	.262	.200	.202	.090
13-602	12	1.23	E	3.2	.076	.135	.087	.081	.042
14-603	12	1.26	C	8.7	.100	.214	.150	.160	.076
15-604	12	1.26	E	3.9	.063	.125	.087	.091	.049
16-605	12	1.25	E	3.8	.086	.107	.075	.076	.042
17-606	12	1.24	B	NR	.114	.225	.162	.174	.081
18-607	12	1.26	E	5.2	.076	.150	.075	.101	.053
19-608	12	1.25	B	4.9	.516	.125	.100	.096	.049

STRUCTURAL RESPONSE RECORD

COMPILED BY _____

DATE 2-1-65 TO 2-3-65

HOUSE C-1

PHASE 2-B — DISPLACEMENT (in.)

2-1-65

RUN	WL	WH	VEL	PEAK	1/2	1	2	3	4	5
						N	N	N	N	N
20-609	12.	1.24	E	3.7	.065	.112	.215	.026	.035	
21-610	12.	1.23	A	4.9	.154	.288	.212	.212	.108	
22-611	12.	1.22	E	2.5	.078	.125	.080	.046	.042	
23-612	12.	1.23	A	4.5	.178	.325	.288	.111	.139	
24-613	12.	1.27	G	4.4	.100	.187	.137	.116	.058	
25-614	12.	1.24	C	4.1	.076	.155	.112	.121	.096	
26-615	12.8	1.27	G	9.6	.076	.125	.100	.096	.145	
27-616	12.8	1.28	C	4.6	.114	.237	.187	.182	.083	
28-617	12.8	1.26	G	6.6	.127	.225	.125	.146	.076	
29-618	12.8	1.22	H	6.7	.063	.112	.087	.071	.042	
30-619	12.1	1.22	D	6.0	.127	.237	.175	.192	.083	
31-620	12.	1.26	H	4.7	.065	.125	.087	.021	.035	
End										

STRUCTURAL RESPONSE RECORD

COMPILED BY _____

DATE 2-1-65 TO 2-3-65

HOUSE C-1

PHASE 2-B — DISPLACEMENT (in.)

2-2-65

RUN	WL	WH	VEL	PEAK	1/2	1	2	3	4	5
						N	N	N	N	N
1-621	12.8	1.27	A	4.1	(No Record)					
2-622	12.8	1.27	E	4.8				↓		
3-633	12.	1.26	A	4.4	.112	.250	.162	.175	.026	
4-634	12.	1.19	B	4.7	.112	.225	.162	.165	.026	
5-635	12.	1.23	E	6.3	.225	.125	.087	.085	.035	
6-636	12.	1.20	B	4.7	.100	.220	.150	.150	.069	
7-627	12.	1.21	C	5.1	.112	.225	.150	.172	.083	
8-628	12.	1.25	G	4.6	.075	.225	.100	.172	.042	
9-629	12.	1.25	C	4.6	.100	.200	.165	.180	.063	
10-630	12.	1.23	D	6.0	(No Record)					
11-631	11.9	1.27	H	4.4	.080	.175	.125	.140	.042	
12-632	11.9	1.27	D	4.8	.080	.187	.125	.140	.069	
13-633	12.	1.16	E	8.8	.150	.263	.180	.215	.111	
14-634	11.9	1.26	B	4.5	.088	.162	.132	.110	.053	
15-635	12.	1.24	E	4.8	.075	.150	.100	.110	.055	
16-636	12.	1.25	F	5.6	.110	.175	.125	.096	.055	
17-637	12.	1.25	A	4.5	.125	.263	.187	.160	.097	
18-638	12.	1.24	F	3.0	.050	.070	.060	.044	.028	
19-639	11.95	1.26	G	3.7	.080	.150	.100	.100	.055	

Structural Response Program

Compiled By ______

Date 2-1-65 2-2-65

House C-1

Phase 2-B 2-2-65 Run	W.C.	Mass	Loc.	Displacement (in) Free Field	1/2 H Mass	2 H Mass	3 H Mass	4 H Mass	5 H Mass
20-640	12.	1.24	H	3.4		(N	R	)	
21-641	12.0	1.25	G	3.7					
22-642	12.0	1.25	D	4.5					
23-643	12.0	1.27	G	3.2					
24-644	12.	1.24	H	NR					
25-645	11.8	1.23	B	46					
26-646	12.	1.21	A	43					
27-647	12.	1.25	E	NR					
28-648	12.	1.33	A	49					
29-649	12.	1.29	B	42					
30-650	12.	1.22	A	46					
End									

Structural Response Program

Compiled By _____

Date 1-18-65

House W-2

Phase 2-B					Scratch Gauge (in)			
					Pre Test			
Run	Alt	Hour	Vec	AM		IN	OUT	TTL
7-101	12.	1.24	A	5.9		.22	.34	.56
8-102	12.1	1.32	E	5.8		.22	.28	.50
9-103	12.	1.35	A	6.3		.26	.36	.62
10-104	11.9	1.21	B	4.8		.24	.32	.56
11-105	12.	1.23	E	5.1		.18	.18	.36
12-106	12.	1.33	B	5.3		.24	.34	.58
13-107	12.	1.25	C	5.6		.28	.38	.66
14-108	12	1.25	G	4.5		.24	.24	.48
15-109	12.	1.27	C	4.7		.20	.28	.48
16-110	12.	1.26	H	5.1		.22	.24	.46
17-111	12.	1.25	▽	5.4		.16	.22	.38
18-112	12.	1.29	H	5.1		.18	.24	.42
19-113	11.8	1.20	E	4.5		.22	.22	.44
20-114	11.7	1.28	B	5.4		.24	.30	.54
21-115	12.	1.20	E	8.7		.18	.18	.36
22-116	12.	1.24	E	5.2		.18	.22	.40
23-117	12.1	1.25	A	6.6		.24	.30	.54
24-118	12.	1.25	F	6.2		.28	.28	.56
25-119	12	1.28	G	6.6		.14	.22	.36

Structural Response Program

Compiled By _____

Date 1-18-65

House W-2

Phase 2-B					Scratch Gauge (in)			
					Pre Test			
Run	Alt	Hour	Vec	AM		IN	OUT	TTL
26-120	11.9	1.38	C	6.2		.42	.42	.84
27-121	12.1	1.31	G	5.1		.12	.22	.34
28-122	11.8	1.22	▽	8.0		.24	.28	.52
29-123	12.	1.21	H	5.7		.18	.28	.46
30-124	12.	1.28	▽	4.2		.16	.22	.38

Structural Response Program

Compiled By _____

Date 1-21-65

House W-2

Phase 2-B				Scratch Gauge (in)			
				Free Field	IN	OUT	TTL
Pin	Alt	Hdng	Loc	AM			
1-177	12.	1.30	H	5.2	.24	.27	.51
2-178	12.	1.38	D	4.1	.24	.31	.55
3-179	12.	1.30	H	6.8	.25	.24	.49
4-180	12	1.30	A	6.7	.24	.25	.48
5-181	12.	1.31	E	4.6	.11	.17	.28
6-182	12.	1.30	A	4.4	.27	.35	.62
7-183	12.1	1.30	B	5.3	.24	.35	.59
8-184	12.1	1.30	E	4.8	.20	.23	.43
9-185	12.1	1.31	B	4.3	.23	.32	.55
10-186	12.	1.30	C	5.6	.14	.40	.74
11-187	12.	1.30	G	4.2	.18	.24	.42
12-188	12.	1.30	C		.36	.44	.76
13-189	25.	1.36	E	2.5	.26	.21	.47
14-190	12.	1.39	D	5.3	.26	.25	.51
15-191	25	1.30	A	2.9	.48	.44	.88
16-192	12.	1.31	H	3.5	.20	.28	.48
17-193	25	1.30	F		.26	.24	.50
18-194	12.	1.30	D	4.8	.21	.21	.42
19-195	24	1.36	A	2.8	.45	.38	.83

Structural Response Program

Compiled By _____

Date 1-21-65

House W-2

Phase 2-B				Scratch Gauge (in)			
				Free Field	IN	OUT	TTL
Pin	Alt	Hdng	Loc	AM			
20-196	25	1.31	E	2.6	.27	.21	.48
21-197	25	1.55	A	2.5	.40	.37	.77
22-198	25.	1.36	F	3.2	.25	.23	.48
23-199	12.1	1.31	E	4.8	.10	.10	.20
24-200	12.	1.30	B	4.9	.22	.35	.57
25-201	12.	1.30	E	5.3	.13	.21	.34
26-202	25.	1.35	F	4.6	.25	.23	.48
27-203	12.1	1.30	C	4.4	.20	.30	.50
28-204	25.	1.32	A		.24	.37	.61
29-205	12.	1.30	A	5.7	.23	.29	.52
30-206	25.	1.35	F	3.8	.27	.15	.42
31-207	26.5	1.33	A	3.8	.41	.45	.86
32-208	25.5	1.35	F		.48	.37	.85
33-209	26.5	1.32	A	2.6	.32	.38	.70
34-210	12.	1.33	H	5.5	.34	.29	.63
35-211	25.5	1.36	E	3.1	.19	.17	.36
36-212	12.	1.38	D	3.6	.18	.24	.42
37-213	25.	1.36	A	2.9	.41	.33	.74
38-214	12.1	1.24	H		.29	.35	.64

STRUCTURAL RESPONSE PROGRAM

COMPILED
By ______

DATE 1-21-65
HOUSE W-2

PHASE 2-B				SCRATCH GAUGE (in)				
Run	Alt.	Hov.	Vec.	Fire Field AX	IN	OUT	TTL	Remarks
39-215	25.	1.37	F		.27	.32	.69	B 58
40-216	12.	1.30	G	6.0	.21	.25	.46	
41-217	11.9	1.28	C	5.2	.37	.43	.80	
42-218	12.	1.31	G	5.2	.25	.27	.52	
43-219	12.	1.31	H	7.9	.27	.37	.64	
44-220	11.9	1.30	▽	4.8	.14	.24	.38	
45-221	11.7	1.31	H	8.8	.27	.30	.57	

STRUCTURAL RESPONSE PROGRAM

COMPILED
By ______

DATE 1-23-65
HOUSE W-2

PHASE 2-B				SCRATCH GAUGE (in)				
Run	Alt.	Hov.	Vec.	Fire Field AX	IN	OUT	TTL	Remarks
1-255	11.9	1.35	C		.21	.29	.50	
2-256	11.9	1.35	G	6.9	.18	.19	.37	
3-257	11.93	1.29	C	4.6	.20	.29	.49	
4-258	11.3	1.30	▽	4.1	.18	.21	.39	
5-259	12.	1.29	H	[illegible]	.21	[illegible]	.43	
6-260	12.	1.30	▽	3.1	.16	.21	.37	
7-261	12.	1.28	E	6.7	.17	.18	.35	
8-262	12.	1.27	B	4.3	.23	.29	.52	
9-263	12.	1.28	E	2.9	.20	.29	.49	
10-264	12.	1.30	B	3.7	.24	.25	.49	
11-265	11.9	1.30	F	4.9	.28	.40	.68	
12-266	11.9	1.31	A	4.0	.19	.06	.25	
13-267	11.9	1.30	E	3.1	—	—	—	
14-268	25	1.36	F	1.8	.20	.24	.44	B-58
15-269	12.	1.34	G	3.1	.22	.21	.43	
16-270	25.	1.35	A	`	.35	.38	.73	B-58
17-271	12.1	1.29	C	3.8	.31	.45	.76	
18-272	25.	1.36	F	4.1	.28	.30	.58	B-58
19-273	12.	1.26	G	5.7	.23	.25	.48	

Structural Response Program

Compiled By ______

Date 1-23-65
House W-2

Phase 2-B				Scratch Gauge (in)				
Run	ALT	[illegible]	[illegible]	Fire Ball AX	IN	OUT	TTL	
20-274	25.	1.34	A	2.7	.29	.32	.61	B-58
21-275	25.	1.35	F	2.8	.29	.31	.60	B-58
22-276	25	1.36	A	2.6	.26	.29	.57	B-58
23-277	25.	1.36	F	2.3	.27	.29	.56	B-58
24-278	24.6	1.35	A	3.1	.12	.19	.32	B-58
25-279	12.	1.26	H	5.2	.22	.31	.53	
26-280	12.	1.31	▽	3.2	.12	.15	.27	
27-281	12.	1.28	H	2.1	.22	.30	.52	
28-282	12.	1.28	▽	2.7	.17	.19	.36	
29-283	25.	1.36	F	2.9	.28	.29	.57	B-58
30-284	25.	1.36	A	2.1	.28	.28	.56	B-58
31-285	12.	1.29	B	3.3	.28	.34	.62	
32-286	25.	1.36	F	2.6	.28	.33	.61	B-58
33-287	2.05	1.29	E	6.6	.30	.19	.49	
34-288	25.	1.37	A	2.1	.26	.30	.56	B-58
35-289	12.	1.29	B	4.2	.30	.39	.69	
36-290	25.	1.37	F	2.9	.14	.20	.34	B-58
37-291	25	1.37	A	4.4	.24	.33	.57	B-58
38-292	25.	1.36	F	3.1	.31	.35	.66	B-58

Structural Response Program

Compiled By ______

Date 1-23-65
House W-2

Phase 2-B				Scratch Gauge (in)				
Run	ALT	[illegible]	[illegible]	Fire Ball AX	IN	OUT	TTL	
39-293	12.	1.25	C	4.3	.25	.35	.60	
40-294	25.	1.37	A	2.9	.29	.40	.69	B-58
41-295	12	1.30	G	3.7	.10	.08	.18	
42-296	25	1.37	E	2.3	.31	.29	.60	B-58
43-297	12.	1.25	C	2.2	.24	.34	.78	
44-298	12.	1.26	G	7.3	.33	.33	.66	
45-299	12.	1.26	H	3.7	.24	.29	.53	
46-300	12.1	1.25	▽	2.8	.15	.19	.34	
47-301	12.	1.26	H	2.1	.19	.23	.42	
48-302	12.	1.29	E	4.2	.20	.20	.40	
49-303	12.	1.30	B	4.2	.24	.33	.57	
50-304	12.	1.30	E	4.8	.32	.27	.55	

Structural Response Program

Compiled By

Date 1-31-65
House W-3

Phase 2-B				Displacement					
Run	[illegible]	[illegible]	[illegible]	Free Field	1	2	3	4	5
1-560	11.97	1.25	E	2.6	.150	.184	.125	.010	.036
2-561	12.	1.25	B	3.9	.125	.138	.125	.148	.072
3-562	11.95	1.26	E	4.8	.050	.100	.025	.021	NR
4-563	12.	1.24	F	4.5	.062	.112	.087	.021	.043
5-564	12.	1.25	A	5.2	.150	.287	.175	.192	.098
6-565	12.5	1.26	F	3.6	.063	.105	.087	.071	.036
7-566	12.	1.24	G	5.4	.100	.150	.125	.026	.050
8-567	12.	1.24	C	4.3	.130	.250	.125	.173	.036
9-568	12.	1.23	G	4.3	.120	.155	.125	.092	.050
10-569	12.	1.23	H	NR	.100	.258	.187	.153	.076
11-570	12.	1.25	F	6.5	.025	.125	.100	.082	.043
12-571	12.	1.23	D	3.7	.075	.150	.112	.112	.058
13-572	13.	1.27	F	5.1	.150	NR	.212	.194	.10
14-573	12.	1.22	H	6.1	.162	NR	.225	.189	.094
15-574	12.	1.26	F	4.0	.075	NR	.150	.019	.043
16-575	12.	1.25	A	3.4	.162	.300	.238	.214	.118
17-576	12.	1.22	F	4.0	.075	.125	.087	.025	.043
18-577	12.	1.24	A	4.2	.138	.250	.200	.173	.086
19-578	12.	1.26	B	4.2	.138	.287	.215	.184	.094

Structural Response Program

Compiled By

Date 1-31-65
House W-3

Phase 2-B				Displacement					
Run	[illegible]	[illegible]	[illegible]	Free Field	1	2	3	4	5
20-579	12.	1.25	E	NR	.060	.100	.025	.167	.037
21-580	12.	1.24	B	4.5	.150	.281	.225	.184	.092
22-581	12.	1.22	C	6.6	.138	.245	.175	.173	.086
23-582	12.	1.23	G	4.7	.108	.125	.130	.092	.043
24-583	12	1.22	C	5.6	.150	.280	.180	.214	.101
25-584	12.	1.20	D	5.9	.100	.175	.138	.133	.012
26-585	12.	1.24	H	4.6	.138	.225	.179	.133	.017
27-586	12.	1.21	D	7.0	.088	.140	.100	.162	.050
28-587	12.	1.22	E	NR	.063	.112	.025	.082	.043
29-588	12.	1.24	E	4.9	.145	.213	.225	.184	.086
30-589	12.	1.24	E	4.2	.010	.115	.080	.082	NR
End									

Structural Response Proposal

Coupled
By RLH

Date 12-2-69 / 12-15-69
House W1-G

Phase 2-A

Pin	Pressure (psf) Free Field	1 N Wall N	2 E Wall E	3 W Wall S	4 S Wall W	5 N Roof	6	7	8	Displacement (10^{-2}) in. 1	2	3	4	5	6	1 Floor N-S	2 Floor E-W	3 Floor V	Acceleration (g) 1	2	3	4	5	6 Roof V
1-288	17.0	1.45	H	NR	NC	NC	NR	NR	NC	NC	NC	NC	NR	NR	NR	NR	NR	NR	NR	NR	NR	NC	NR	NC	NC	NC
2-289	17.2	1.4	D													.06	.04	.21	↓	↓	↓	↓	↓	↓
3-290	17.1	1.4	H													NR	NR	NR	.022	.061	.17	.012	.027	.030
4-291	17.0	1.3	A													.32	.27	.126	.008	.003	.014	.006	.014	.015
5-292	17.5	1.42	F							.20	.30	.14	.30	.35		NR	NR	NR	.019	.009	.029	.018	.049	.063
6-293	18.0	1.25	A							.14	.14	.17	.18	.33		NR	NR	NR	.009	.003	.036	.009	.058	.037
7-294	19.4	1.35	B							.50	.12	.47	.11	.32		.106	.18	.64	.011	.003	.047	.006	.033	.016
8-295	18.3	1.25	E							.26	.13	.23	.11	.31		.47	.28	.160	.011	.003	.031	.009	.016	.019
9-296	17.0	1.40	B							.49	.18	.55	.23	.44		NR	NR	NR	.022	.005	.056	.012	.036	.052
10-297	23.5	1.45	C							.25	.17	.42	.15	.37		.28	.16	.81	.014	.009	.016	.024	.033	.026
11-298	23.0	1.6	G							.20	NA	.33	.06	.23		NR	NR	NR	.011	.014	.016	.018	.019	.019
12-299	20.0	1.38	C							.43	.13	.64	.11	.19		NR	NR	NR	.011	.003	.020	.039	.022	.022
13-300	21.0	1.5	D							.23	.12	.40	.11	.22		.13	.24	.106	NR	NR	NR	NR	NR	NR
14-301	21.0	1.4	H							.44	.17	.55	.17	.24		.21	.25	.126	↓	↓	↓	↓	↓	↓
15-302	23.0	1.5	D							.24	.20	.27	.17	.34		NR	NR	NR	↓	↓	↓	↓	↓	↓
16-303	23.0	1.45	E							.24	.17	.35	.21	.37		NR	NR	NR	.014	.003	.025	.018	.042	.041
17-304	24.2	1.65	B							.25	.18	.23	.12	.29		.15	.13	.101	.014	.003	.020	.024	.038	.030
END																								

Structural Response Proposal

Coupled
By RLH

Date 12-2-69 / 12-15-69
House W1-G

Phase 2-A
12-5-64

Pin	Pressure (psf) Free Field	1 N Wall N	2 E Wall E	3 W Wall S	4 S Wall W	5 N Roof	6	7	8	Displacement (10^{-2}) in. 1	2	3	4	5	6	1 Floor N-S	2 Floor E-W	3 Floor V	Acceleration (g) 1	2	3	4	5	6 Roof V
1-305	12.2	1.2	E	5.5	3.2	NC	1.6	NR	4.9	NR	NR	NR	.25	.22	.30	.22	.97	.18	NR	NR	NR	NR	NR	NR	NR
2-306	12.2	1.2	A	NR	6.2		4.2		11.9				.43	.22	.19	.22	.99	.15							
3-307	12.0	1.2	E	6.2	3.4		3.4		6.0				.32	.24	.33	.24	.81	.22							
4-308	12.0	1.25	G	4.8	3.2		3.5		4.6				.99	.14	.78	.23	.65	.64	1.18	.74	1.654	.021	.010	.078	.018	.088	.041
5-309	12.0	1.25	C	NR	/	NC	?	X	EC	G	PC	D	.87	.22	.69	.21	.64	.11	.32	.51	2.01	NR	NR	NR	NR	NR	NR
6-310	12.3	1.21	G	5.6	2.9		3.0		3.4				.87	.13	.91	.29	.43	.03	NR	NR	NR	.018	.010	.077	.018	.043	.023
7-311	12.0	1.2	H	5.3	3.4		2.3		4.1				.30	.24	.39	.43	.64	.42	.56	.38	2.36	.018	.006	.088	.015	.020	.039
8-312	12.2	1.2	D	5.3	4.0		6.3		4.8				NR	NR	NC	NC	NC	NC	.85	.68	2.86	.024	.003	.089	.021	.035	.063
9-313	12.0	1.2	H	7.0	5.6		2.7		3.0				.105	.14	.110	.32	.57	.09	NR	NR	NR	.021	.006	.115	.015	.032	.058
10-314	12.0	1.21	A	NR	/	NC	?	X	EC	G	PC	D	NR	NR	NR	NC	NC	NC	.27	.32	NR	NR	NR	NR	NR	NR	NR
11-315	12.2	1.2	E	5.9	3.2		4.7		7.8				.2	.12	.2	.32	.132	.04	1.2	.95	NR	.028	.006	.048	.027	.082	.060
12-316	12.0	1.2	A	4.9	6.7		4.1		8.3				.44	.18	.20	.33	.132	.11	NR	NR	NR	.021	.003	.048	.018	.090	.048
13-317	12.0	1.24	B	7.6	6.2		4.3		9.7				.42	.17	.52	.22	.77	.04				.021	.006	.055	.015	.055	.045
14-318	18.8	1.26	E	5.3	3.0		4.2		7.6				.59	.42	.65	.39	.169	NR				.031	.003	.059	.027	.055	.052
15-319	12.0	1.22	B	7.0	7.0		4.3		5.1				.33	.16	.49	.20	.111	NR				.024	.006	.063	.015	.053	.037
16-320	12.0	1.21	C	7.3	6.5		4.3		4.9				.53	.21	.54	.22	.77	NC	1.31	.70	2.16	.018	.006	.077	.012	.035	.030
17-321	12.0	1.2	G	4.2	4.2		4.8		5.1				.36	.24	.74	.31	.86	.20	.32	.74	2.27	.021	.006	.077	.018	.067	.037
18-322	12.2	1.2	C	6.5	5.2		4.1		4.1				.29	.19	.94	.30	.77	NR	NR	NR	NR	.071	.003	.070	.012	.058	.045
19-323	12.0	1.2	D	7.0	4.6		3.2		6.0				.64	.16	.123	.44	.18	.74	1.31	.89	NR	.031	.003	.106	.018	.038	.060

STRUCTURAL RESPONSE PROGRAM

Compiled By ______

Date 12-2-64; 12-15-64
House W-4

Phase I-A 12-5-64 Run	Yld	Mach	Vc	Free Field (psf)	Pressure (psf) 1 N Wall N	2 E Wall E	3 S Wall S	4 W Wall W	5 N Roof	6 E Roof	7 Big Room	8 Small Room	Displacement (10^{-2} in) 1 W Wall N Cor E-W	2 N Wall E Cor N-S	3 E Wall S Cor E-W	4 S Wall W Cor N-S	5 Inter Wall N-S	6 W Wall E-W	Floor 1 N-S	Floor 2 E-W	Floor 3 V	Acceleration (g) 1 N-S	2	3	4	5 Inter Wall N-S	6 Roof V
20-324	12.0	1.21	H	5.6	4.9	NR	2.7	NR	5.5	NR	NR	NR	.44	.19	1.21	.29	.45	.22	1.03	.92	2.52	.074	.003	.110	.015	.032	.034
21-325	12.0	1.2	D	6.2	3.4		1.5		3.6				.57	.24	1.12	.42	.65	.44	NR	NR	NR	.024	.003	.097	.018	.043	.041
22-326	12.2	1.2	E	3.2	2.7		3.8		4.3				.32	.43	.68	.44	.66	.11				.021	.003	.050	.030	.060	.048
23-327	12.0	1.2	B	5.3	6.3		1.3		5.1				.22	.18	.66	.23	.74	.11				.021	.006	.071	.018	.060	.037
24-328	12.0	1.2	E	3.9	2.9		4.6		4.1				.33	.43	.70	.36	.63	.14				.024	.003	.060	.024	.058	.048
25-329	12.0	1.21	F	5.6	3.0		5.2		2.7				.12	.32	.20	.31	.79	NR				.024	.006	.028	.024	.064	.062
26-330	11.75	1.2	A	5.3	7.6		1.5		6.5				.22	.22	.34	.22	.90	NR				.021	.006	.048	.018	.082	.045
27-331	11.9	1.21	F	6.2	3.2		5.7		6.1				.12	.30	.29	.26	.77	.37				.021	.006	.048	.021	.064	.070
28-332	12.4	1.08	G	5.1	3.4		3.8		4.3				.52	.30	1.04	.33	1.00	.48	.49	.62	2.54	.018	.006	.093	.027	.087	.041
29-333	12.0	1.2	C	7.9	5.7		1.3		4.8				.32	.29	.83	.22	.96	.34	1.38	1.27	2.22	.021	.003	.070	.021	.075	.037
30-334	12.0	1.21	G	6.6	3.0		3.4		3.9				.25	.22	.65	.24	.77	.06	NR	NR	NR	.021	.006	.073	.015	.067	.037
END																											

STRUCTURAL RESPONSE PROGRAM

Compiled By RLH

Date 12-2-64; 12-15-64
House W-4

Phase I-A 12-6-64 Run	Yld	Mach	Vc	Free Field (psf)	Pressure (psf) 1 N Wall N	2 E Wall E	3 S Wall S	4 W Wall W	5 N Roof	6 E Roof	7 Big Room	8 Small Room	Displacement (10^{-2} in) 1 W Wall N Cor E-W	2 N Wall E Cor N-S	3 E Wall S Cor E-W	4 S Wall W Cor N-S	5 Inter Wall N-S	6 W Wall E-W	Floor 1 N-S	Floor 2 E-W	Floor 3 V	Acceleration (g) 1 N Wall W Cor N-S	2 E Wall N Cor E-W	3 S Wall E Cor N-S	4 W Wall S Cor E-W	5 Inter Wall N-S	6 Roof V
1-335	12.35	1.2	H	NR	4.2	NR	1.6	NR	3.5	NR	NR	NR	1.14	.23	1.28	.39	1.04	.92	NR	NR	NR	.024	.005	.108	.018	.040	.037
2-336	12.0	1.2	D	NR	5.0		2.0		4.7				NR	NR	NR	NR	NR	NR	.98	.89	2.68	.021	.005	.113	.012	.028	.037
3-337	12.0	1.2	H	4.9	5.8		2.3		4.7				1.10	.13	1.06	.29	.58		NR	NR	NR	.014	.005	.036	.017	.059	.041
4-338	12.0	1.2	H	5.2	6.0		1.2		6.0				.35	.14	.22	.15	1.10		.59	.44	1.90	.013	.005	.041	.024	.059	.034
5-339	12.0	1.21	F	1.9	3.1		3.1		4.2				.25	.21	.22	.22	1.05		.90	.21	2.12	.018	.003	.036	.021	.100	.055
6-40	11.7	1.2	H	6.0	1.5		2.0		6.0				.47	.21	.22	.19	2.16		NR	NR	NR	.014	.003	.066	.018	.063	.037
7-341	12.1	1.22	B	NR									.99	.12	.64	.13	1.17		1.27	.53	NR	NR	NR	NR	NR	NR	NR
8-342	11.9	1.21	C	6.3	3.7		1.2		1.7				.99	.24	.64	.38	1.32		.34	.44	1.86	.028	.005	.061	.030	.063	.060
9-343	12.0	1.2	B	1.4	5.0		1.0		2.6				.82	.10	.57	.11	.94		NR	NR	NR	.016	.003	.041	.012	.053	.026
10-344	12.0	1.2	C	6.0	6.6		1.0		4.2				.60	.21	.96	.29	1.14		NR	NR	NR	.018	.005	.088	.018	.063	.060
11-345	12.0	1.22	G	4.4	2.9		2.0		3.3				.94	.23	.67	.22	.90		.35	.30	2.58	.021	.005	.077	.021	.059	.034
12-346	12.2	1.2	C	4.4	5.2		1.0		3.7				.54	.17	.85	.27	.92		NR	NR	NR	.021	.003	.082	.018	.028	.044
13-347	11.8	1.21	D	3.5	3.1		1.0		3.5				.79	.21	1.17	.30	.75	.13	.23	.53	1.48	.018	.003	.109	.015	.037	.036
14-348	12.0	1.21	H	4.6	4.4		2.0		5.3				1.07	.18	1.16	.28	.59	NR	.71	.87	2.76	.024	.005	.118	.018	.034	.045
15-349	12.0	1.2	D	4.4	3.7		1.2		1.3				.67	.13	.89	.28	.71		NR	NR	NR	.021	.003	.093	.018	.039	.045
16-350	12.0	1.21	E	6.0	3.5		4.1		5.3				.61	.45	.52	.40	1.32		1.72	.76	NR	.032	.003	.056	.039	.081	.067
17-351	12.0	1.25	B	6.3	5.0		1.0		1.2				.37	.14	.55	.20	1.06		.42	.42	2.07	.021	.005	.072	.018	.066	.043
18-352	12.0	1.22	E	5.7	2.5		2.5		3.5				.62	.40	.57	.33	1.12		NR	NR	NR	.028	.005	.061	.030	.063	.048

STRUCTURAL RESPONSE PROGRAM

COMPILED
By RLH

DATE 12-3-69; 12-15-69
HOUSE W-4

PHASE 2-A 12-6-64 Run	W.T	Hor	Vc	PRESSURE (psf) Free Field 0 AK	1 N Wall N	2 E Wall E	3 S Wall S	4 W Wall W	5 N Roof	6 E Roof	7 Big Room	8 Small Room	DISPLACEMENT (10⁻²) IN 1 Wall N cor E-W	2 Wall E cor N-S	3 Wall S cor E-W	4 Wall W cor N-S	5 Inter Wall N-S	6 N Wall E-W	1 Floor N-S	2 Floor E-W	3 Floor V	ACCELERATION (g) 1 Wall W cor N-S	2 Wall N cor E-W	3 Wall E cor N-S	4 Wall S cor E-W	5 Inter Wall N-S	6 Roof V
19-353	12.0	1.2	F	5.2	2.7	NR	2.7	NR	4.6	NR	NR	NR	.20	.16	.22	.20	1.05	NR	43	.74	256	.014	.005	.036	.021	.056	.048
20-354	11.0	1.2	A	4.9	6.4		6.8		4.0				.36	.25	.30	.20	1.42		1.93	93	2.84	.021	.005	.040	.024	.100	.048
21-355	12.0	1.2	F	5.7	2.9		4.1		4.2				.22	.27	.12	.21	1.05		NR	NR	NR	.018	.005	.031	.027	.069	.060
22-356	12.0	1.2	G	4.9	3.5		NR		5.4				.50	.50	.88	.30	1.39					.018	.005	.097	.024	.096	.052
23-357	11.9	1.23	C	8.2	7.7		NR		12.7				.44	.26	.72	.23	1.56					.018	.003	.088	.024	.090	.049
24-358	11.8	1.2	G	NR →									.52	.26	.79	.27	1.12					.021	.005	.093	.021	.075	.082
25-359	12.0	1.21	H	5.7	5.6		2.5		4.2				.49	.29	1.10	.28	.62		33	74	254	N.R.	NR	NR	NR	NR	NR
26-360	11.8	1.21	D	6.3	3.5		4.9		4.6				.52	.35	1.09	.48	1.36	.35	42	.38	2.54						
27-361	11.8	1.24	H	4.4	5.2		[illegible]		2.9				NR →					NR	NR	NR	NR						
28-362	12.1	1.2	A	NR →									NR →						.42	.28	1.61						
29-363	12.0	1.2	F	4.6	2.3		5.5		4.2				.24	.23	.23	.21	1.26		40	.53	2.00	.024	.005	.052	.027	.081	.052
30-364	12.0	1.2	H	2.7	2.5		4.3		6.7				.18	.17	.18	.19	1.14		NR	NR	NR	.018	.003	.036	.012	.084	.041
END																											

STRUCTURAL RESPONSE PROGRAM

COMPILED
By RLH

DATE 12-3-69; 12-15-69
HOUSE W-4

PHASE 2-A 12-7-64 Run	W.T	Hor	Vc	PRESSURE (psf) Free Field 0 AK	1 N Wall N	2 E Wall E	3 S Wall S	4 W Wall W	5 N Roof	6 E Roof	7 Big Room	8 Small Room	DISPLACEMENT (10⁻²) IN 1 Wall N cor E-W	2 Wall E cor N-S	3 Wall S cor E-W	4 Wall W cor N-S	5 Inter Wall N-S	6 N Wall E-W	1 Floor N-S	2 Floor E-W	3 Floor V	ACCELERATION (g) 1 Wall W cor N-S	2 Wall N cor E-W	3 Wall E cor N-S	4 Wall S cor E-W	5 Inter Wall N-S	6 Roof V
1-365	9.0	1.2	A	NR →									NR →						2.10	.65	NR	NR	NR	NR	NR	NR	NR
2-366	9.2	1.2	E	7.6	4.9	NR	10.6	NR	[illegible]	NR	NR	NR	NR →						1.73	1.65	NR						
3-367	9.2	1.2	A	8.1	9.0		5.4		8.1				.55	.58	.39	.56	1.56	NR	NR	NR	NR						
4-368	9.0	1.2	C	NR →									.58	.25	.37	.44	1.66	NR	NR	.74	NR						
5-369	9.0	1.2	F	NR →									.72	.25	1.33	.77	1.93	.66	NR	NR	NR						
6-370	9.0	1.2	C	.18	2.7		5.9		11.8				.64	.30	2.75	.57	.97	NR	NR	NR	NR						
7-371	9.0	1.15	D	4.6	5.6		7.2		7.2				.96	.72	1.63	.84	NR		2.38	.70	NR						
8-372	9.2	1.22	A	8.1	5.6		5.4		6.0				.46	.24	.33	.39	1.10		NR	NR	NR						
9-373	9.3	1.2	C	9.2	4.8		6.6		[illegible]				.61	.48	1.49	.78	1.22										
10-374	9.0	1.24	E	6.2	7.6		10.2		7.5				.40	.93	.64	.79	1.32					.048	.006	.050	.057	.086	.129
11-375	8.8	1.22	D	4.9	9.3		8.3		5.1				.22	.12	.24	.24	.95					.021	.003	.026	.012	.044	.097
12-376	9.0	1.2	E	2.1	4.0		10.1		5.5				[illegible]	.61	.66	.70	1.43					.039	.006	.054	.042	.083	.108
13-377	9.0	1.21	F	12.6	[illegible]		[illegible]		7.4				[illegible]	.71	.21	.58	1.52					.065	.006	.038	.045	.096	.125
14-378	9.0	1.21	A	5.7	[illegible]		4.6		6.7				.48	.24	.24	.33	1.31					.074	.003	.035	.021	.092	.066
15-379	9.1	1.2	F	12.5	5.8		13.3		[illegible]				.1	.77	.34	.79	1.82					.052	.010	.046	.063	.130	.108
16-380	9.0	1.23	A	5.2	5.9		4.1		4.6				.27	.25	.28	.36	1.45					.024	.003	.035	.024	.102	.060
17-381	9.0	1.2	F	[illegible]	4.6		10.2		[illegible]				.39	.72	.33	.66	1.76					.048	.010	.042	.051	.121	.108
18-382	9.0	1.24	A	[illegible]	10.6		6.2		[illegible]				.56	.34	.44	.53	[illegible]					.031	.006	.046	.027	.115	.122

Structural Response Program

Coupled By RLH

Date 12-7-64 / 12-8-64 / 12-8-64

House W-6

Phase 2-A

Pressure (psf) — Displacement (10^{-3} in.) — Acceleration (g)

Pin	Pressure 1	2	3	4	5	6	7	8	Displacement 1	2	3	4	5	6	7	8	9	Acceleration 1	2	3	4	5	6
1-393	5.7	3.58	NR	6.58	NR	5.07	NR	NR	NR	NR	.21	.52	.88	.53	.59	NR	NR	NR	NR	.039	.010	.060	.039	.067	.074
20-394	13.3	4.22		5.98		5.29					.106	.47	.156	.77	.88					.035	.006	.115	.033	.069	.069
21-395	6.24	3.87		9.88		2.73					.77	.48	.91	.53	.96					.039	.010	.068	.036	.064	.282
END																									

Coupled By RLH

Date 12-8-64 / 12-8-64

House W-6

Phase 2-A

Pressure (psf) — Displacement (10^{-3} in.) — Acceleration (g)

Pin	Pressure 1	2	3	4	5	6	7	8	Displacement 1	2	3	4	5	6	7	8	9	Acceleration 1	2	3	4	5	6
1-394	11.0	11.4	NR	8.4	NR	11.3	NR	NR	NR	NR	.55	.36	.50	.35	.296	.30	NR	NR	NR	.028	.006	.049	.030	.188	.244
2-391	11.2	7.1		14.2		12.0					.66	.78	.30	.76	.146	.32				.041	.010	.034	.087	.117	.144
3-392	9.1	12.7		7.5		10.1					.58	.32	.63	.42	.339	NR				.028	.006	.053	.02	.226	.194
4-393	9.1	8.2		7.3		9.3					.26	.33	.158	.53	.144					.028	.006	.128	.036	.120	.154
5-394	7.6	12.4	E	9.1	5.8	13.9		10.61			.48	.78	.31	.79	.218					.052	.010	.038	.064	.162	.159
6-395	7.0	12	C	10.2	10.7	6.3		9.3			.96	.34	.160	.08	.121					.043	.003	.128	.036	.125	.154
7-396	7.5	12	D	11.7	8.6	8.8		9.0			.234	.72	.210	.74	.165					.043	.006	.163	.048	.142	.167
8-397	7.5	12	A	11.7	12.7	7.9		14.0			.25	.39	.49	.45	.288					.034	.006	.058	.034	.265	.232
9-398	7.5	12	D	11.2	7.7	9.8		12.7			.215	.28	.215	.76	.187					.041	.006	.167	.054	.162	.218
10-399	7.5	12	E	10.2	5.9	11.0		8.8			.169	.78	.141	.66	.150					.052	.010	.076	.048	.110	.159
11-400	7.45	12	H	12.1	11.8	7.7		10.3			.84	.40	.49	.50	.339					.033	.006	.061	.037	.229	.175
12-401	7.5	12	E	9.9	6.9	14.6		11.3			.187	.89	.100	.76	.168					.055	.010	.079	.051	.131	.150
13-402	7.5	12.1	F	11.8	6.6	11.5		9.5			.41	.77	.38	.76	.196					.052	.010	.034	.051	.150	.124
14-403	7.5	12	A	11.6	9.5	10.9		9.6			.24	.39	.50	.44	.334					.031	.006	.056	.024	.240	.154
15-404	7.5	12.2	F	11.2	5.2	12.1		9.1			.40	.78	.31	.78	.224					.062	.010	.034	.048	.134	.146
16-405	7.5	12	C	9.8	9.4	7.7		10.3			.82	.38	.160	.41	.189					.028	.006	.133	.033	.184	.157
17-406	7.5	12	A	14.5	9.9	7.3		9.8			.62	.40	.52	.39	.312					.034	.006	.065	.01	.229	.160
18-407	7.5	12	F	10.7	5.4	10.0		9.3			.47	.61	.29	.09	.149					.041	.010	.038	.041	.120	.113
19-408	7.5	12	H	13.1	9.4	6.3		9.1			.71	.20	.62	.33	.209					.028	.003	.060	.024	.187	.135

Coupled By RLH

Date 12-8-64

House W-6

Phase 2-A

Pressure (psf) — Displacement (10^{-3} in.) — Acceleration (g)

Pin	Pressure 1	2	3	4	5	6	7	8	Displacement 1	2	3	4	5	6	7	8	9	Acceleration 1	2	3	4	5	6
20-409	7.5	12.1	E	13.1	5.4	NR	12.3	NR	9.5	NR	NR	NR	NR											
21-410	7.5	12.2	D	11.3	7.3		7.7		7.6															
22-411	7.5	12.1	E	12.0	6.4		13.3		10.3															
END																								

Structural Response Program

Coupled By RLH

Date 12-2-69 12-15-69

House W1-G

Phase 2-A 12-9-64 Run	Vel	Wave	Inc	Pressure (psf) Free Field	1	2	3	4	5	6	7	8	Displacement (10⁻³ in) 1	2	3	4	5	6	1	2	3	Acceleration (g) 1	2	3	4	5	6
1-416	7.0	1.2	A	14.0	10.4	NR	6.0	NR	11.0	NR	NR	NR	.61	.89	.54	.45	3.12	NR	NR	NR	NR	.031	.006	.048	.035	.165	.149
2-417	7.0	1.2	E	10.3	8.0		16.1		12.4				.48	.147	.41	.86	1.99					.055	.010	.037	.061	.122	.153
3-418	7.0	1.2	A	11.7	13.9		7.3		10.7				.59	.84	.66	.44	3.52					.028	.006	.056	.032	.185	.179
4-419	6.2	1.2	C	14.2	13.3		2.9		14.1				.47	.157	.44	.88	1.99					.039	.006	.139	.092	.132	.135
5-420	7.0	1.2	E	10.3	6.9		13.2		13.1				.252	.121	.389	.75	1.73	2.34				.055	.010	.137	.058	.138	.179
6-421	7.0	1.2	D	13.7	11.8		10.4		14.8				.121	.122	.99	.53	.44	NR				.048	.010	.199	.043	.109	.201
7-422	7.0	1.2	A	12.0	12.9		7.7		14.6				.239	.124	.254	.66	1.83	2.19				.034	.010	.094	.035	.259	.230
8-423	7.0	1.2	D	11.2	9.5		9.6		10.0				.119	.109	.88	.12	2.18	.14				.045	.004	.174	.046	.112	.144
9-424	7.0	1.25	E	14.0	7.9		12.6		13.6				.94	.74	.56	.45	3.19	NR				.089	.013	.079	.070	.159	.232
10-425	6.2	1.22	A	14.7	11.4		6.9		10.7				.107	.141	.87	.109	4.28					.024	.010	.060	.026	.217	.218
11-426	7.0	1.22	E	9.5	6.0		13.4		10.5				.88	.105	.56	.54	3.78					.079	.010	.064	.055	.144	.207
12-427	7.0	1.15	E	15.4	6.5		14.4		11.5				.50	.158	.96	.77	1.53					.083	.013	.053	.048	.141	.139
13-428	7.1	1.2	A	12.1	13.8		8.5		12.4				1.14	.84	.188	.66	2.63					.039	.010	.060	.038	.197	.197
14-429	7.2	1.2	F	10.6	6.0		11.5		7.7				.24	.111	.208	.66	1.53					.052	.014	.042	.044	.069	.128
15-430	7.0	1.2	C	15.6	13.8		7.7		11.9				.201	.59	.251	.77	2.76					.039	.013	.139	.035	.181	.164
16-431	7.0	1.2	D	12.9	10.3		10.2		12.3				.122	.86	.66	.53	3.61					.045	.006	.199	.043	.115	.194
17-432	7.0	1.19	C	16.5	11.6		7.5		11.9				.58	.147	.63	.76	1.82					.042	.006	.181	.029	.195	.164
18-433	7.0	1.2	A	12.3	11.6		7.1		10.0				.30	.86	.66	.46	2.75					NR					
19-434	7.0	1.21	F	11.2	5.8	↓	13.4	↓	10.5	↓	↓	↓	NR	NR	NR	NR	—	↓	↓	↓	↓	NR	↓	↓	↓	↓	↓

Structural Response Program

Coupled By RLH

Date 12-2-69 12-15-69

House W1-G

Phase 2-A 12-9-64 Run	Vel	Wave	Inc	Pressure (psf) Free Field	1	2	3	4	5	6	7	8	Displacement (10⁻³ in) 1	2	3	4	5	6	1	2	3	Acceleration (g) 1	2	3	4	5	6
20-435	7.0	1.2	A	11.2	11.4	NR	7.5	NR	10.5	NR	NR	NR	NR	NR	NR	NR	NR	NR	NR	NR	NR	.034	.006	.060	.032	.218	.202
21-436	7.0	1.2	E	15.3	6.5		14.6		10.0													.069	.010	.107	.055	.112	.143
22-437	7.0	1.17	D	11.7	7.7		10.4		10.7													.048	.010	.188	.052	.106	.132
23-438	7.0	1.18	E	16.2	7.7	↓	12.1	↓	15.5	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	.074	.010	.186	.064	.131	.156
END																											

Structural Response Program

Coupled By RLH

Dated 2-19-12-15-68

House W-9

Ransom-A 12-10-64 Run	Wind Dir	Wind Vel	Exp	Pressure (psf) Ref Pitot NW	1 N Wall N	2 E Wall E	3 W Wall W	4 W Wall N	5 N Roof	6 E Roof	7 Int	8	Displacement (10^{-2}) in 1	2	3	4	5	6	1	2	3	Acceleration (g) 1	2	3	4	5	6
1-443	6.5	1.3	A	17.7	20.9	NR	10.1	NR	17.0	NR	NR	NR	NR	NR	NR	NR	NR	NR	NR	NR	NR	.027	.013	.066	.047	.365	.273
2-444	6.5	1.2	F	17.5	20.7		21.5		14.9													.142	.016	.038	.076	.264	.190
3-445	6.4	1.15	C	15.4	18.7		9.5		14.9													.048	.010	.734	.041	.304	.179
4-446	6.5	1.2	F	10.5	12.9		13.4		10.5													.052	.013	.041	.067	.177	.143
5-447	6.5	1.18	C	13.3	15.2		8.7		15.9													.034	.010	.169	.032	.157	.143
6-448	6.5	1.14	D	14.6	11.2		15.3		15.1													.048	.010	.224	.021	.183	.197
7-449	6.5	1.19	A	21.3	19.3		10.3		15.6													.041	.013	.083	.044	.444	.374
8-450	6.45	1.19	D	19.7	18.6		16.7		21.4													.076	.010	.214	.073	.183	.263
9-451	6.5	1.2	E	15.8	12.9		25.6		16.4													.117	.013	.132	.125	.274	.248
10-452	6.5	1.1	A	12.3	15.9		8.5		12.4													.037	.010	.196	.035	.389	.208
11-453	6.5	1.1	F	12.7	8.1		16.9		9.1													.076	.016	.104	.029	.267	.155
12-454	6.45	1.1	F	16.6	9.5		23.3		15.9													.049	.013	.067	.033	.334	.156
13-455	6.5	1.1	A	12.3	14.2		9.7		13.5													.078	.006	.046	.041	.298	.174
14-456	6.5	1.1	F	11.1	7.7		15.9		11.0													.055	.013	.037	.061	.204	.135
15-457	6.5	1.16	C	23.3	19.2		7.8		14.0													.037	.010	.154	.028	.229	.222
16-458	6.5	1.14	D	18.3	17.2		13.8		14.5													.076	.010	.154	.023	.197	.251
17-459	6.4	1.15	C	20.0	14.8		9.1		14.9													.031	.010	.161	.038	.256	.194
18-460	6.0	1.2	A	11.9	12.2		6.6		10.8													.031	.010	.076	.035	.318	.164
19-461	6.5	1.1	F	11.2	8.9	↓	17.9	↓	13.5	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	.042	.013	.053	.076	.207	.207

Structural Response Program

Coupled By RLH

Dated 2-19-12-15-68

House W-9

Ransom-A 12-10-64 Run	Wind Dir	Wind Vel	Exp	Pressure (psf) Ref Pitot NW	1 N Wall N	2 E Wall E	3 W Wall W	4 W Wall N	5 N Roof	6 E Roof	7 Int Room	8 Outside Room	Displacement (10^{-2}) in 1	2	3	4	5	6	1	2	3	Acceleration (g) 1	2	3	4	5	6
20-462	6.4	1.1	A	20.4	15.1	NR	10.1	NR	13.6	NR	NR	NR	NR	NR	NR	NR	NR	NR	NR	NR	NR	.044	.010	.083	.047	.425	.237
21-463	6.5	1	E	11.7	8.7		15.7		9.1													.076	.016	.164	.074	.187	.178
22-464	6.45	1	D	18.3	7.5		23.3		9.3													.062	.006	.191	.061	.167	.120
23-465	6.5	1	E	10.2	6.9		16.6		11.0													.055	.006	.092	.047	.167	.131
END						↓		↓		↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓	↓						

Structural Response Program

COUPLED
By RLH

Date 12-14 : 12-15-64
House W-6

Phase-A 12-11-64				Pressure (P.S.F.)								Displacement (10^{-2}) in.									Acceleration (g)					
Run	Sec.	Lic.	Veh.	Front of House	1	2	3	4	5	6	7	8	1	2	3	4	5	6	1	2	3	1	2	3	4	5	6
					In Front				In Front	Side Room	Side Room	Side Room															
1-470	6.25	1.11	A	20.5	19.9	NR	12.5	NR	18.2	NR	NR	NR	NA						NR	NR	NR	.055	.006	.076	.053	.368	.226
2-471	6.25	1.15	F	20.2	20.0		19.5		14.7				.46	.417	.64	.530	3.02	NR				.075	.013	.068	.024	.232	.211
3-472	6.1	1.15	A	20.4	20.0		11.9		21.3				.47	.71	.80	.62	NR					.041	.006	.096	.044	.164	.328
4-473	6.1	1.15	C	16.3	17.5		8.9		17.0				.161	.53	2.64	.60	4.0					.041	.006	.199	.038	.257	.252
5-474	6.05	1.13	F	6.3	6.2		22.8		15.2				.55	1.22	.60	.90	3.87					.081	.013	.178	.028	.254	.195
6-475	6.2	1.12	C	15.5	18.3		8.4		14.2				.145	.47	2.34	.58	4.2					.034	.010	.181	.038	.182	.207
7-476	6.1	1.1	D	21.2	17.8		16.1		22.5				.330	1.15	2.70	.91	NR					.017	.003	.099	.012	.065	.038
8-477	6.1	1.1	A	14.3	14.2		10.0		15.2				.161	1.15	1.20	.76	5.9					.052	.013	.192	.054	.402	.182
9-478	6.1	1.1	D	23.1	18.4		13.1		13.7				NA	.94	2.49	.83	NR					.078	.010	.279	.031	.228	.215
10-479	6.1	1.1	E	11.4	9.9		24.7		13.7				NR	AA	AA	AA	AA					.024	.006	.135	.083	.222	.205
11-480	6.1	1.13	F	14.3	9.8		20.6		15.4													.029	.010	.094	.083	.307	.197
12-481	6.1	1.11	A	19.6	18.8		11.1		16.1													.047	.013	.128	.062	.495	.280
13-482	6.1	1.13	F	13.6	13.3		23.5		16.2													.029	.016	.080	.092	.349	.262
14-483	6.1	1.16	C	18.0	17.5		9.7		18.2													.044	.010	.215	.041	.329	.219
15-484	6.1	1.16	D	22.4	19.6		13.1		14.4													.075	.010	.222	.077	.167	.228
16-485	6.1	1.17	C	20.0	22.9		11.9		23.0													.055	.014	.238	.053	.470	.342
17-486	6.2	1.17	A	NR																		.041	.010	.080	.044	.435	.280
18-487	6.1	1.15	F	16.3	18.9		24.5		16.2													.089	.013	.152	.089	.301	.197
19-488	6.1	1.2	A	23.1	23.2		12.8		18.0													.047	.010	.066	.047	.537	.342

Structural Response Program

COUPLED
By RLH

Date 12-14 : 12-16-64
House W-6

Phase-A 12-11-64				Pressure (P.S.F.)								Displacement (10^{-2}) in.									Acceleration (g)					
Run	Sec.	Lic.	Veh.	Front of House	1	2	3	4	5	6	7	8	1	2	3	4	5	6	1	2	3	1	2	3	4	5	6
					In Front				In Front	Side Room	Side Room	Side Room															
20-488	6.1	1.16	F	25.3	20.4	NR	27.4	NR	18.2	NR	NR	NR	NA						NR	NR	NR	.103	.013	.106	.101	.336	.280
21-489	6.1	1.18	A	12.7	12.3		10.6		17.5				NA									.024	.006	.078	.039	.466	.237
22-491	6.1	1.19	E	13.1	8.2		17.8		15.7				NA									.089	.010	.096	.092	.334	.186
END																											

STRUCTURAL RESPONSE PROGRAM

COUPLED
By RLH

DATE: 12-12-64
HOUSE W-9

PHASE-A 12-12-64 RUN	(100)			PRESSURE (PSF) Free Field 0.W	1 N	2	3 W	4 W	5 N	6 R. Room	7 Bath Room	8 Utility Room	DISPLACEMENT (10^{-2} in.) 1	2	3	4	5	6	1 FLOOR N-S	2 FLOOR E-W	3 FLOOR V	ACCELERATION (g) 1	2	3	4	5	6
1-426	17.0	13	E	2.5	1.7	NR	4.5	NR	2.6	NR	NR	NR	NR	NR	NR	NR	NR	NR	32	.32	2.15	.012	NR	.014	.014	.041	.034
2-427		13	B	3.1	4.2		2.3		3.2										.11	.28	1.10	.003		.031	.005	.043	.024
3-428		128	E	NR															NR	NR	NR	.009		.030	.005	.041	.043
4-499		13	F	3.1	2.0		4.5		3.1										.40	.28	1.84	.007		.017	.014	.056	.051
5-500		128	A	3.3	4.7		2.0		3.8										.23	.25	1.60	.003		.014	.005	.034	.031
6-501		13	E	3.9	1.8		3.7		2.9										NR	NR	NR	.002		.020	.008	.047	.041
7-502		128	H	3.1	3.4		2.3		2.7										.39	.32	1.26	.003		.038	.003	.027	.031
8-503		128	D	3.9	3.0		3.7		3.4										.37	.40	NR	.007		.046	.005	.032	.057
9-504	16.8	13	H	4.3	3.0		2.5		3.8										NR	NR	NR	.007		.059	.003	.027	.047
10-505	17.0	126	H	2.3	2.7		1.8		2.3										.20	.20	1.23	.003		.004	.003	.047	.034
11-506		126	F	2.7	2.1		3.3		2.8										.26	.26	1.43	.003		.011	.008	.043	.051
12-507		126	H	4.7	2.9		2.0		2.2										NR	NR	NR	.003		.004	.003	.053	.024
13-508		126	B	3.7	4.2		1.8		3.2										.11	.31	1.17	.003		.035	.005	.053	.037
14-509		13	E	3.1	1.8		3.2		2.4										.43	.40	2.23	.009		.020	.011	.035	.037
15-510		13	B	2.3	2.9		2.0		1.7										NR	NR	NR	.003		.031	.003	.035	.030
16-511		13	C	NR															.17	.20	.94	NR					
17-512		13	F	1.8	1.3		2.3		1.3										.20	.14	.92	.003		.011	.005	.032	.037
18-513		13	C	1.4	1.8		1.2		1.5										NR	NR	NR	.003		.028	.003	.027	.014
19-514		128	D	2.9	2.1		2.2		2.0										.32	.35	1.63	.019		.055	.008	.030	.034

STRUCTURAL RESPONSE PROGRAM

COUPLED
By RLH

DATE: 12-19-64
HOUSE W-9

PHASE-A 12-12-64 RUN	(100)			PRESSURE (PSE) Free Field 0.W	1 N	2	3 W	4 W	5 N	6 R. Room	7 Bath Room	8 Utility Room	DISPLACEMENT (10^{-2} in.) 1	2	3	4	5	6	1 FLOOR N-S	2 FLOOR E-W	3 FLOOR V	ACCELERATION (g) 1	2	3	4	5	6
20-515	17.0	13	H	4.7	4.0	NR	2.7	NR	3.7	NR	NR	NR	NR	NR	NR	NR	NR	NR	.68	.31	2.08	.007	NR	.007	.008	.032	.066
21-516		13	D	3.7	2.3		2.2		2.4										NR	NR	NR	.007		.052	.005	.030	.034
22-517		13	E	2.9	1.3		3.7		2.4										.28	.28	1.54	.007		.007	.016	.030	.034
23-518		13	B	2.9	2.0		1.7		1.8										.09	.26	.82	.003		.035	.003	.032	.034
24-519		13	E	2.7	1.6		2.3		1.7										NR	NR	NR	.007		.024	.005	.030	.041
25-520		13	F	4.5	2.1		4.0		4.0										.59	.28	1.97	.012		.032	.018	.074	.084
26-521		13	E	1.6	0.9		1.3		1.1										.12	.14	.60	.003		.004	.005	.023	.030
27-522		131	F	NR															NR	NR	NR	NR					
28-523		13	F	2.3	1.3		1.8		1.5										.19	.12	.83	.003		.007	.005	.027	.029
29-524		13	F	1.6	1.2		1.8		1.8										.08	.12	.62	.003		.011	.005	.035	.034
30-525		127	D	3.5	1.8		2.7		2.9										NR	NR	NR	.007		.035	.008	.027	.034
END																											

Structural Response Program

Coupled
By RLH

Date 12-2-64 / 12-15-64
House W-6

Phase 2-A				Pressure (PSF)									Displacement (10^{-2} in)									Acceleration (g)					
12-13-64				Free Field	1	2	3	4	5	6	7	8	1	2	3	4	5	6	1 Floor N-S	2 Floor E-W	3 Floor V	1	2	3	4	5	6 Roof V
Run	W/O	Mach																									
1-526	20.4	1.4	E	2.9	1.5	NR	3.0	NR	2.8	NR	NR	NR	NR	NR	NR	NR	NR	NR	.15	.28	1.46	.012	.003	.029	.013	.029	.037
2-527		1.4	B	2.1	2.0		2.0		1.8										.02	.12	.86	.010	.003	.036	.008	.033	.021
3-528		1.4	E	2.3	1.2		2.7		2.2										NR	NR	NK	.012	.003	.020	.016	.037	.037
4-529		1.4	E	2.9	1.5		2.7		2.3										.17	.20	1.55	.012	.003	.020	.016	.043	.038
5-530		1.42	A	2.5	2.6		1.5		2.8										.20	.11	1.22	.010	.003	.017	.008	.040	.025
6-531		1.38	F	2.3	1.4		2.7		2.3										NR	NR	NR	.012	.003	.020	.010	.043	.038
7-532		1.4	H	2.9	2.0		2.2		2.7										.31	.31	1.85	.012	.003	.061	.010	.017	.037
8-533			D	2.0	1.5		2.0		1.5										.19	.28	1.12	.015	.003	.053	.008	.033	.025
9-534			H	2.1	1.4		1.7		1.6										NR	NR	NR	.012	.003	.044	.008	.017	.029
10-535			A	2.0	2.2		1.3		1.3										.14	.12	.99	.010	.003	.020	.005	.037	.021
11-536			F	2.3	1.4		2.9		2.4										.15	.19	1.34	.012	.003	.020	.016	.043	.038
12-537			A	2.1	2.4		1.3		1.7										NR	NR	NR	.010	.003	.017	.008	.037	.017
13-538			B	1.8	2.7		1.5		1.7										.06	.15	.77	.010	.003	.041	.005	.030	.021
14-539			E	3.7	1.5		2.7		1.8										.31	.30	NR	.015	.003	.029	.018	.043	.037
15-540			B	2.1	1.9		1.5		1.5										NR	NR	NR	.012	.003	.061	.008	.037	.021
16-541			C	3.1	2.3		1.3		2.7										.34	.14	1.23	.010	.003	.029	.010	.037	.021
17-542			F	2.3	1.2		1.9		1.2										NR	NR	NR	.019	.003	.029	.013	.037	.021
18-543			C	2.1	2.2		1.5		1.8										NR	NR	NR	.010	.003	.036	.013	.043	.029
19-544			D	2.1	1.9		1.9		2.2										.34	.37	1.91	.022	.003	.065	.010	.041	.037

Structural Response Program

Coupled
By RLH

Date 12-2-64 / 12-15-64
House W-6

Phase 2-A				Pressure (PSF)									Displacement (10^{-2} in)									Acceleration (g)					
12-13-64				Free Field	1	2	3	4	5	6	7 Liv Room	8 Small Room	1	2	3	4	5	6	1 Floor N-S	2 Floor E-W	3 Floor V	1	2	3	4	5	6 Roof V
Run	W/O	Mach																									
20-545	20.4	1.4	H	2.9	2.2	NR	2.9	NR	3.3	NR	NR	NR	NR	NC	NK	NK	NR	NK	.31	.28	1.54	.010	.005	.065	.019	.020	.038
21-546		1.4	D	2.3	1.9		2.0		2.2										NR	NR	NK	.015	.003	.061	.013	.037	.037
22-547		1.39	E	2.3	1.5		2.9		2.7										NR	NR	NK	.019	.003	.041	.021	.050	.057
23-548		1.4	B	2.3	2.8		1.9		2.0										NR	NR	NR	.010	.003	.053	.008	.037	.032
24-549		1.41	E	2.1	1.2		2.4		1.3										NR	NK	NK	.019	.003	.036	.018	.040	.032
25-550		1.4	F	2.9	1.9		3.6		2.3										.32	.29	1.69	.019	.005	.032	.023	.057	.057
26-551			A	2.9	2.2		1.7		1.7										.29	.12	1.23	.010	.003	.017	.013	.047	.037
27-552			F	6.0	1.4		2.2		1.6										NR	NR	NK	.012	.003	.020	.016	.047	.017
28-553			H	3.3	2.0		2.0		1.6										.32	.19	1.15	.012	.003	.065	.013	.020	.029
29-554			D	2.3	1.7		2.0		2.0										.19	.31	1.12	.015	0	.053	.013	.03[illegible]	.029
30-555			H	6.4	2.6		3.6		3.1										NR	NR	NR	.015	.005	.077	.015	.054	.053
END																											

Structural Response Program

Compiled By RLH

Date 12-2-69; 12-15-69
House W-4

Phase 2-A 12-14-64 Run				Pressure (PSF)	1	2	3	4	5	6	7	8	Displacement (10^{-2}) in 1	2	3	4	5	6	1	2	3	Acceleration (g) 1	2	3	4	5	6
1-556	12.0	1.28	A	—	NR	→							.26	.21	.20	.15	1.30	NR	1.08	.31	1.71	.007	NR	.006	.005	.058	.421
2-557	12.0	1.28	F	—	NR	→							.21	.21	.40	.23	.95		.31	.71	1.79	.007	NR	.019	.019	.040	.057
3-558	11.9	1.28	A	—	NR	→							.20	.19	.22	.13	1.30		NR	NR	NR	.007	.003	.010	.005	.052	.034
4-559	12.0	1.25	B	—	NR	→							.53	.08	.28	.19	.99		.15	.46	1.69	.007	NR	.052	.005	.019	.034
5-560		1.27	E	—	NR	→							.42	.38	.42	.38	.49		.46	.62	2.14	.025		.023	.027	.047	.043
6-561		1.28	B	—	NR	→							.62	.08	.104	.23	1.05		1.08	NR	NK	.010		.065	.005	.057	.037
7-562		1.3	C	NR	4.8	3.0	3.4	4.9	6.0	3.5	2.6	1.5	.40	.06	.79	.30	1.20		.46	.46	NR	.007		.032	.000	.060	.043
8-563		1.3	F	4.4	2.8	4.1	5.0	3.2	3.9	3.6	2.6	1.5	.18	.42	.22	.30	1.76		.89	.58	NR	.029		.017	.030	.055	.067
9-564		1.3	C	4.5	4.5	2.8	3.1	3.9	3.7	3.3	2.5	1.0	NR	→					NR	NR	NK	.010		.032	.005	.044	.043
10-565	↓	1.25	D	5.1	3.8	3.7	4.4	6.6	4.3	3.9	2.9	1.8	.64	.21	1.28	.48	1.37		.37	.59	2.23	.032		.059	.019	.052	.043
11-566	11.8	1.25	H	4.3	3.5	6.4	3.9	2.6	5.5	3.8	1.6	0.9	.68	.13	1.23	.29	1.57		.62	.31	2.09	.032		.052	.019	.044	.051
12-567	11.3	1.25	D	4.4	3.5	3.3	4.1	4.9	4.3	3.6	2.6	1.3	.51	.21	1.12	.46	1.24		NR	NR	NK	NR	→				
13-568	12.1	1.3	E	2.3	2.8	2.8	5.3	5.8	3.5	3.2	NR	NR	NR	→					.72	.44	2.38	.032	↓	.022	.030	.035	.067
14-569	12.0	1.3	B	4.8	5.4	6.1	3.4	3.4	4.2	3.9	1.8	1.0	NR	→					.29	.62	1.75	.019	.003	.074	.008	.059	.061
15-570		1.3	E	5.0	5.6	6.2	5.8	7.1	6.0	4.7	1.3	0.7	NR	→					NR	NR	NR	.032	NR	.032	.033	.044	.091
16-571		1.24	F	5.6	3.2	4.4	5.5	3.1	4.5	5.1	1.6	0.9	.22	.36	.26	.38	1.37		1.00	.43	NR	.029		.029	.033	.060	.094
17-572		1.24	A	4.4	NR	→					1.5	0.9	.22	.17	.20	.10	1.32		.77	.52	2.09	.010		.026	.011	.060	.042
18-573	↓	1.25	F	5.0	2.5	3.7	4.4	2.6	2.6	2.9	1.6	0.7	.20	.23	.26	.32	1.01	↓	NR	NR	NK	.032	↓	.032	.027	.055	.073

Structural Response Program

Compiled By RLH

Date 12-2-69; 12-15-69
House W-4

Phase 2-A 12-14-64 Run				Pressure (PSF)	1	2	3	4	5	6	7	8	Displacement (10^{-2}) in 1	2	3	4		6	1	2	3	Acceleration (g) 1	2	3	4	5	6
19-574	12.0	1.3	H	4.3	3.1	6.4	3.6	2.0	3.7	4.1	1.4	0.4	.66	.06	1.23	.30	.63	NK	.60	.41	NK	.025	.003	.091	.005	.032	.067
20-575		1.2	D	4.4	3.4	3.0	4.1	5.8	4.2	3.6	1.5	0.6	.85	.17	1.4	.36	1.07		.24	.54	NR	.033	NR	.061	.011	.049	.067
21-576		1.3	H	4.2	3.0	5.0	3.1	2.6	3.1	3.0	1.8	0.7	.60	.04	1.07	.27	.63		NK	NK	NK	.022		.091	.008	.029	.057
22-577		1.3	H	4.6	5.1	4.1	3.3	3.6	4.2	3.1	NR	NR	.22	.19	.22	.17	1.34		.60	.31	1.92	NR	→				
23-578		1.3	F	4.8	3.1	4.2	5.6	4.1	3.9	3.3	1.6	0.9	.11	.40	.22	.32	1.41		.51	.59	2.44	.032		.029	.027	.064	.077
24-579	↓	1.3	H	4.2	5.4	4.1	2.9	3.6	4.8	4.5	1.5	0.9	.22	.17	[illegible]	.17	1.41		NR	NR	NK	.019		.023	.005	.063	.061
25-580	11.5	1.22	B	4.3	4.9	5.5	2.7	2.6	[illegible]	[illegible]	1.3	0.9	.44	.11	.66	.17	1.05		.22	.59	1.91	.007		.052	.005	.055	.037
26-581	12.0	1.25	E	4.9	2.5	2.7	5.0	4.6	3.9	3.2	1.5	0.7	.64	.36	.66	.53	.40		.54	.62	NR	.032		.032	.027	.032	.061
27-582		[illegible]	C	5.2	4.5	5.5	3.3	2.4	4.3	3.9	1.8	1.0	.44	.15	.62	.19	1.26		NR	NR	NR	.015		.059	.005	.047	.071
28-583		1.24	C	3.9	5.8	3.1	2.7	4.6	3.9	3.3	1.5	0.9	.44	.40	.44	.21	1.15		1.03	.48	1.79	.007		.042	.008	.055	.027
29-584		1.25	F	4.5	2.8	4.4	5.5	3.4	6.0	4.5	1.6	0.7	[illegible]	.36	.37	.36	1.26		.42	.52	2.08	.034		.032	.027	.067	.075
30-585	↓	1.26	C	4.9	1.5	2.8	2.4	3.7	3.9	3.3	1.3	0.7	.42	.08	.66	.19	1.24		NR	NR	NR	.010		.032	.008	.058	.040
[illegible]	11.8	1.26	D	4.7	[illegible]	[illegible]	3.8	4.6	4.9	3.0	1.5	0.7	.66	.06	1.14	.42	.65		.69	.51	2.14	.014		.065	.005	.029	.052
[illegible]	11.6	[illegible]	H	[illegible]		6.1	4.6	2.4	3.5	3.6	1.8	0.6	[illegible]	.11	1.10	.19	.48		.63	.46	2.16	.010		.094	.005	.079	[illegible]
[illegible]	11.4	[illegible]	[illegible]	4.2		[illegible]	[illegible]	5.1	[illegible]	3.5	1.6	0.6	[illegible]	.11	1.14	.21	.65		NR	NR	NK	.015		.059	.005	.079	[illegible]
[illegible]		1.26	[illegible]	[illegible]		2.5	5.3	[illegible]	[illegible]	3.9	4.5	[illegible]	.53	[illegible]	.66	[illegible]	.95		.57	.74	NR	.008		.032	.022	.041	[illegible]
[illegible]		[illegible]		1.[illegible]		[illegible]	[illegible]	2.6	5.5	4.1	1.5	0.7	.53	.11	.73	.11	.84		.12	.42	1.35	.010		.059	.008	.055	[illegible]
[illegible]	↓		E	[illegible]	↓	[illegible]	[illegible]	[illegible]	4.7	4.7	1.6	0.6	.79	.51	.70	.30	1.11	↓	NR	NR	NC	.032	↓	.036	.027	[illegible]	[illegible]

Structural Response Program

Compiled By RLH

House W-4

Phase 2-A 12-15-64 Run	[illegible]	[illegible]	Vx	Fire Field 0	Pressure (P.F) 1	2	3	4	5	6	7	8	Displacement (10^{-2}) in 1	2	3	4	5	6	Floor 1	2	3	Acceleration (g) 1	2	3	4	5	6
1-592	12.0	1.15	F	NR	—	—	—	—	—	—	—	—	.05	.05	.22	.15	.86	NR	.34	.42	1.73	.007	NR	.011	.005	.055	.022
2-593	12.0	1.17	A	NR	—	—	—	—	—	—	—	—	.36	.07	.24	.13	1.3	↓	.31	.31	2.00	.007	↓	.011	.005	.050	.024
3-594	11.5	1.5	F	NR	—	—	—	—	—	—	—	—	.24	.24	.38	.19	1.05	↓	NR	NR	NR	.016		.026	.008	.065	.139
4-595	10.5	1.3	D	NR	—	—	—	—	—	—	—	—	.67	NR	1.51	.34	1.20	.50	1.25	1.08	NR	.015		.085	.010	.025	.067
5-596		1.3	H	NR	—	—	—	—	—	—	—	—	.96	.24	1.42	.38	1.45	.98	NR	NR	NR	.025		.044	.013	.058	.101
6-597		1.3	D	NR	—	—	—	—	—	—	—	—	.60	.05	1.39	.25	NR	NR	NR	NR	NR	.012		.074	.005	.088	.053
7-598		1.21	H	NR	7.3	5.9	4.3	4.3	5.6	4.8	2.4	1.0	.44	.24	.41	.19	1.58		.42	.59	2.08	.010		.026	.018	.108	.047
8-599		1.23	F	NR	3.4	4.3	7.1	4.3	5.5	5.0	1.6	0.7	.22	.38	.43	.30	NR		NR	NR	NR	.019		.081	.026	.058	.063
9-600	↓	1.26	H	NR	7.7	6.2	3.9	3.0	5.6	5.7	2.2	1.2	.31	.22	.36	.19	1.89		↓	↓	↓	NR	→				→
10-601	12.0	1.22	B	4.6	6.7	5.9	3.5	3.0	4.0	4.1	2.4	0.7	.53	NR	.94	.13	1.05					.010		.028	.021	.116	.081
11-602	10.5	1.20	E	5.6	3.6	3.4	7.4	6.3	5.5	4.4	1.6	0.9	.72	.38	.96	.32	1.05					.029		.040	.024	.067	.077
12-603	10.5	1.20	B	6.0	7.7	7.8	4.1	4.2	4.8	5.2	2.6	0.7	.82	.22	1.20	.19	1.47					.007		.082	.021	.088	.057
13-604	10.5	1.20	C	5.8	7.0	3.3	3.9	7.5	6.4	5.0	2.2	1.0	.24	.24	.84	.17	.84					.019		.048	.021	.062	.057
14-605	10.4	1.20	F	5.3	3.9	5.3	8.1	4.3	5.8	5.2	2.8	1.4	.19	.24	.48	.21	1.69					.032		.084	.025	.108	.084
15-606	10.5	1.21	C	6.0	7.4	3.4	3.5	7.0	6.6	5.4	1.9	0.6	.43	.24	.86	.19	.84					.010		.058	.021	.055	.061
16-607	10.5	1.15	D	7.-	NR	—	—	—	—	→	2.2	0.9	.74	.24	1.22	.32	.88					.012		.068	.013	.032	.043
17-608	10.4	1.16	H	5.5	NR	—	—	—	—	→	2.1	0.9	.84	NR	1.51	.76	NR					.015			.005	.030	.057
18-609	10.5	1.26	D	5.6	4.3	3.7	4.6	5.5	3.9	4.8	1.6	0.7	.79	.22	1.37	.32	1.05	↓	↓	↓	↓	.019	↓	.068	.016	.055	.073

Structural Response Program

Compiled By RLH

Date 12-2-69; 12-15-69

House W-4

Phase 2-A 12-15-64 Run	[illegible]	[illegible]	Vx	Fire Field 0	Pressure (psf) 1	2	3	4	5	6	7	8	Displacement (10^{-2} in) 1	2	3	4	5	6	Floor 1	2	3	Acceleration (g) 1	2	3	4	5	6
19-610	10.5	1.27	E	6.0	3.6	3.6	8.3	6.3	2.9	5.3	1.9	0.9	NR	—	—	—	—	→	NR	NR	NR	.032	NR	.052	.026	.052	.067
20-611		1.25	B	5.8	7.4	2.4	3.4	2.7	2.3	5.2	1.9	1.0	NR	—	—	—	—	→				.012		.072	.021	.089	.063
21-612		1.25	E	5.9	4.3	3.7	10.3	8.5	5.3	6.1	1.8	0.7	NR	—	—	—	—	→				.032		.048	.026	.073	.073
22-613		1.21	F	4.4	3.6	4.3	6.0	3.8	4.5	4.8	1.6	0.9	.48	.29	.41	.10	1.13	NR				.012		.024	.026	.067	.071
23-614		1.2	A	7.0	2.3	6.7	3.9	4.0	4.3	5.0	1.6	1.0	.26	.22	.48	.12	1.56					.015		.031	.008	.031	.061
24-615	↓	1.21	F	3.0	3.7	4.9	6.7	3.0	3.9	5.0	1.8	0.9	.48	.29	.46	.10	1.32	↓	↓	↓	↓	.019	↓	.034	.026	.073	.077
END																											

Structural Response Program

Coupled
By [illegible]

Dated 1-15-65
House W-9

Phase 2-B 1-15-65 Run	Alt (1000)	Ch	Ve	W	Pressure 1 N Wall N	2 E Wall E	3 S Wall S	4 W Wall W	5 W Roof	6 E Roof	7 Big Room	8 Small Room	Displacement 1	2	3	4	5	6	Acceleration (g) 1	2	3	4	5	6 Roof V
1-1	1.2	1.27	A			No Record							231	129	276	062	1770	171	.009	.003	.017	.022	.186	.042
2-2	1.2	1.22	F										314	245	334	145	1516	239	.012	.005	.028	.032	.171	.056
3-3	1.2	1.26	A										150	142	174	154	533	051	.012	.003	.020	.022	.192	.062
4-4	1.2	1.25	B										534	155	435	062	1063	359	.014	.005	.024	.040	.103	.040
5-5	1.5	1.23	E										5[illegible]	297	449	185	124	428	.018	0	.034	.040	.124	.056
6-6	1.2	1.26	B										462	191	435	154	956	034	.014	.003	.024	.035	.103	.042
7-7	1.2	1.26	C										802	322	638	185	584	.496	.020	.003	.034	.056	.185	.058
8-8	1.2	1.27	G										680	[illegible]	[illegible]	157	616	376	.014	.006	.031	.043	.111	.042
9-9	1.2	1.28	C										[illegible]	322	725	304	602	584	.023	.003	.034	.062	.101	.058
10-10	1.2	1.11	X										815	245	711	231	1015	014	.020	.003	.034	.059	.118	.068
11-11	1.2	1.12	H										917	142	603	123	124	010	.012	.003	.020	.054	.083	.066
12-12	1.2	1.20	D										530	271	319	154	506	068	.018	.003	.031	.028	.094	.062
13-13	1.8	1.21	E	5.7	.4	1.5	5.5	.4	4.5	5.5	4.4	4.0	3[illegible]	214	290	293	248	.017	.023	.003	.041	.043	.156	.082
14-14	1.9	1.24	B	6.6	2.8	.2	1.4	2.7	.5	2.0	2.1	4.6	514	181	435	154	1418	051	.014	0	.020	.046	.192	.040
15-15	1.2	1.26	E	[illegible]	[illegible]	2.1	[illegible]	5.6	[illegible]	4.2	.0	2.3	245	374	232	762	863	.017	.028	0	.034	.032	.109	.068
16-16	1.2	1.26	F	4.1									313	258	290	1.4	357	034	.018	.003	.027	.038	.167	.028
17-17	1.2	1.25	A	5.6							5.4		401	348	176	154	402	017	.018	.003	.024	.042	.319	.056
18-18	1.2	1.25	F	4.7							.4		284	206	240	108	1019	034	.014	.003	.028	.030	.151	.052
19-19	1.2	1.26	G	5.0							.6		815	[illegible]	464	.139	.771	015	.012	.006	.021	.054	.103	.066

Structural Response Program

Coupled
By [illegible]

Dated 1-15-65
House W-9

Phase 2-B 1-15-65 Run	Alt (1000)	Ch	Ve	W	Pressure (psi) 1 N Wall N	2 E Wall E	3 S Wall S	4 W Wall W	5 W Roof	6 E Roof	7 Big Room	8 Small Room	Displacement (10^{-3} in) 1	2	3	4	5	6	Acceleration (g) 1	2	3	4	5	6 Roof V
20-20	1.2	1.23	C	6.2		No Record					4.4	.1	563	258	290	216	711	.051	.020	.003	.041	.043	.272	.066
21-21	1.2	1.24	G	6.1							2.2	2.5	735	129	580	154	.924	.012	.012	.003	.028	.045	.106	.066
22-22	1.88	1.26	A	4.2							1.9	2.6	680	.142	566	077	1410	068	.012	.003	.013	.057	.123	.058
23-23	1.9	1.26	X	5.6							4.4	2.5	.626	.335	.406	150	1235	065	.014	.005	.034	.051	.112	.034
24-24	1.2	1.28	H	[illegible]							2.6	2.4	953	245	783	.154	1682	683	.016	.006	.018	.085	.177	.024
25-25	1.2	1.22	G	[illegible]							2.3	.1	.418	[illegible]	203	.150	2.121	171	.020	.003	.028	.027	.274	.048
26-26	1.25	[illegible]	[illegible]	5.0							5	.1	.256	245	216	150	NA	256	.018	.003	.028	.030	.169	.048
27-27	1.5	[illegible]	A	[illegible]							2.5	.4	521	755	181	170	2964	171	.020	.003	.028	.027	.342	.066
28-28	[illegible]	[illegible]	[illegible]	[illegible]	4.6	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	.1	514	[illegible]	163	154	1.631	325	.020	.003	.028	.040	.219	.042
29-29	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	150	.32	.145	154	[illegible]	015	.012	0	.020	.022	.176	.046

Structural Response Program

Compiled By [illegible]

Date 1-15-65; 1-20-65
House W-6

Phase 2-B — 1-16-65

Run	Alt. (ft)	Mach	Vec.	Field Cold W	Pressure (p.s.f.) 1 N Wall N	2 E Wall	3 S Wall S	4 W Wall W	5 W Roof	6 E Roof	7 Big Room	8 Small Room	Displacement (10⁻² in.) 1 N Wall N Cor E-W	2 N Wall E Cor N-S	3 E Wall S Cor E-W	4 S Wall W Cor N-S	5 Inter Wall N-S	6 S Wall Center E-W	Acceleration (g) 1 N Wall W Cor N-S	2 E Wall N Cor E-W	3 S Wall E Cor N-S	4 W Wall S Cor E-W	5 Inter Wall N-S	6 Roof V	
1-31	11.5	1.21	G					Nd											.013	0	.020	.014	.139	.014	
2-32	11.8	1.22	G	6.1	2.1	8.1	6.6	3.4	6.7	6.6	2.4	[illegible]	.648	.196	.536	.146	.903	.394	.018	.003	.024	.050	.112	.063	
3-33	11.5	1.26	C	6.0	8.2	3.6	3.8	6.0	2.0	6.2	3.7	2.8	.480	.244	.522	.146	1.274	.292	.022	.003	.035	.039	.180	.050	
4-34	12	1.25	D	6.0	3.6	3.6	4.1	4.3	5.1	4.1	3.5	2.8	.496	.473	.559	.248	.562	.394	.026	.003	.038	.044	.106	.059	
5-35	12	1.25	H	6.0	3.9	7.1	4.1	3.4	5.5	5.3	2.3	2.2	.744	.174	.777	.132	.592	.531	.018	.003	.024	[illegible]	.071	.067	
6-36	12	1.26	D	6.5	3.3	3.0	4.7	2.7	5.5	4.1	3.4	3.1	.496	.467	.496	.230	.592	.367	.026	0	.038	.044	.103	.067	
7-37	11.7	1.20	E	6.5	3.3	4.1	6.6	6.0	5.5	5.9	3.7	2.3	.372	.489	.375	.190	.888	.272	.026	.003	.035	.042	.133	.087	
8-38	12	1.21	B	5.6	5.1	6.6	3.1	2.1	3.7	3.8	2.9	3.4	.409	.196	.576	.146	1.629	.381	.026	.003	.028	.042	.218	.047	
9-39	12	1.24	E	6.2	3.6	3.6	5.9	6.0	4.8	3.8	3.4	2.3	.372	.489	.348	.277	.746	.014	.030	.003	.038	.044	.122	.027	
10-40	11.7	1.26	E	6.8	3.9	4.1	6.9	3.4	2.0	4.4	NR	NR	.360	.342	.402	.146	1.540	.010	.026	.003	.038	.026	.210	.069	
11-41	11.6	1.26	A	9.0	6.7	3.6	3.4	2.6	4.4	4.7	NR	NR	.469	.310	.293	.209	2.679	NR	.026	0	.031	.028	.237	.063	
12-42	12	1.26	F	5.4	3.3	3.6	5.9	3.5	5.9	5.3	NR	2.9	.349	.359	.402	.161	1.480	NR	.030	.003	.025	.042	.127	.047	
13-43	12	1.28	G	2.6	3.6	5.6	5.6	3.0	5.1	4.7	NR	2.5	.868	.326	.710	.190	.962	.010	.026	.003	.042	.061	.152	.100	
14-44	12	1.27	C	7.3	4.0	4.1	3.1	4.3	4.8	4.7	NR	3.4	.496	.375	.402	.261	2.960	NR	.030	0	.035	.031	.329	.047	
15-45	25	1.35	E	4.0	2.4	3.0	3.1	3.0	2.6	2.5	3.2	1.8	.236	.165	.268	.044	.681	NR	.018	0	.014	.022	.096	.040	B-58
16-46	25	1.35	E	5.1	2.4	3.6	3.8	0.7	2.9	2.5	2.9	2.0	.245	.165	.308	.059	.240	NR	.013	0	.014	.028	.123	.037	B-58
17-47	25	1.35	E	4.5	3.0	3.0	5.6	3.0	3.7	3.1	3.4	2.2	.124	.243	.228	.117	.244	NR	.018	0	.020	.022	.096	.047	B-58
18-48	25	1.35	E	4.0	4.7	2.5	3.7	2.6	2.6	2.8	3.1	2.0	.234	.179	.262	.130	.240	NR	.018	0	.018	.025	.126	.049	B-58
19-49	25	1.35	E	2.9	2.1	3.0	3.7	0.7	1.8	2.2	3.1	1.7	.236	.147	.295	.059	.637	NR	.018	0	.014	.025	.096	.030	B-58

Structural Response Program

Compiled By p.c.c.

Date 1-15-65; 1-20-65
House W-6

Phase 2-B — 1-16-65

Run	Alt. (ft)	Mach	Vec.	Field Cold W	Pressure (p.s.f.) 1 N Wall N	2 E Wall E	3 S Wall S	4 W Wall W	5 W Roof	6 E Roof	7 Big Room	8 Small Room	Displacement (10⁻² in.) 1 N Wall N Cor E-W	2 N Wall E Cor N-S	3 E Wall S Cor E-W	4 S Wall W Cor N-S	5 Inter Wall N-S	6 S Wall Center E-W	Acceleration (g) 1 N Wall W Cor N-S	2 E Wall N Cor E-W	3 S Wall E Cor N-S	4 W Wall S Cor E-W	5 Inter Wall N-S	6 Roof V
20-50	12	1.24	H	5.5	3.3	5.6	3.1	2.1	2.9	2.4	2.2	2.6	.396	.179	.670	.132	.858	NR	.022	.003	.014	.056	.100	.047
21-51	11.9	1.23	D	8.7	3.3	3.6	4.4	5.6	5.5	4.7	NR	2.2	.530	.342	.496	.175	.577	NR	.026	.003	.031	.044	.106	.053
22-52	12	1.26	H	6.4	3.9	9.2	2.8	2.6	4.0	4.1	NR	3.1	.496	.163	.563	.146	.814	.028	.022	0	.011	.047	.184	.057
23-53	12	1.23	A	5.5	5.1	3.0	2.8	3.4	2.9	2.8	2.2	3.1	.347	.212	.161	.146	2.022	NR	.022	0	.020	.025	.196	.047
24-54	12	1.21	F	6.0	3.3	5.1	6.2	4.7	4.4	4.4	NR	2.1	.360	.147	.415	.146	1.629	NR	.030	.003	.028	.042	[illegible]	.063
25-55	12	1.24	A	5.4	5.1	3.6	3.1	2.6	4.0	3.8	NR	3.2	.372	.228	.187	.146	2.220	NR	.026	0	.020	.022	.265	.043
26-56	12	1.26	B	5.0	3.0	8.6	3.8	4.3	5.5	5.9	NR	4.7	.521	.179	.603	.146	1.990	NR	.022	.003	.031	.056	.332	.073
27-57	12	1.27	E	8.3	2.7	4.1	6.6	4.8	7.0	6.2	NR	2.8	.360	.359	.294	.292	.873	NR	.034	0	.042	.039	.139	.069
28-58	12	1.28	B	5.8	5.8	6.1	2.8	3.4	4.0	2.4	3.1	3.1	.496	.163	.455	.132	2.518	NR	.018	.003	.024	.044	.284	.063
29-59	12	1.29	C	6.2	8.5	3.6	3.1	6.4	7.0	7.8	4.3	3.1	.496	.228	.388	.290	1.656	[illegible]	.030	.003	.035	.033	.261	.100
30-60	12	1.28	G	5.8	4.8	6.6	4.7	3.0	6.1	5.9	3.1	2.6	.645	.147	.536	.146	1.065	.010	.018	.003	.024	.050	.117	.081
31-61	12	1.30	C	6.2	5.5	3.6	2.5	3.4	4.0	3.8	3.4	2.9	.496	.179	.214	.161	2.719	NR	.026	0	.028	.022	.310	.065
32-62	12	1.29	D	6.0	3.9	3.6	4.2	6.0	6.2	5.6	2.6	1.8	.583	.277	.670	.175	.740	NR	.026	0	.028	.056	.103	.063
33-63	11.8	1.27	H	4.4	3.3	5.6	3.1	2.6	3.7	NR	2.2	2.3	.496	.163	.576	.132	[illegible]	[illegible]	.018	0	.018	.050	.096	.053
34-64	11.6	1.26	D	2.6	5.0	4.1	5.0	9.4	6.6	4.7	3.1	2.6	.720	.294	.804	.761	.555	[illegible]	.030	.003	.035	.070	.136	.100
End.																								

Structural Response Program

Compiled By: [illegible]

Date: 15:15:120 65
House: W-6

Phase 2-B 1-17-65 Run	Alt	[illegible]	[illegible]	Wind W	Pressure (psf) 1 N Wall N	2 E Wall E	3 S Wall S	4 W Wall W	5 W Roof	6 E Roof	7 Big Room	8 Small Room	Displacement 1 N Wall N Cor E-W	2 N Wall E Cor N-S	3 E Wall S Cor E-W	4 S Wall W Cor N-S	5 Inter Wall N-S	6 [illegible]	Acceleration (g) 1 N Wall W Cor N-S	2 E Wall N Cor E-W	3 S Wall E Cor N-S	4 W Wall S Cor E-W	5 Inter Wall N-S	6 Roof V
1-65	1.19	1.21	E	6.7	2.0	2.6	6.7	1.9	1.4	4.8	1.8	1.3	546	316	489	146	701	429	.012	.002	.022	.021	.181	.048
2-66	1.2	1.19	B	6.8	6.0	2.5	2.8	1.9	2.1	4.2	1.2	1.4	508	316	506	117	1182	410	.014	0	.029	.042	.119	.037
3-67	1.20	1.20	E	6.0	2.7	2.6	5.9	4.5	3.2	3.8	2.8	2.3	384	216	359	146	701	315	.014	0	.022	.031	.083	.048
4-68	1.2	1.22	E	7.0	3.3	3.5	6.5	2.5	2.5	4.5	1.4	1.2	120	316	107	190	1021	110	.014	0	.029	.015	.122	.055
5-69	1.2	1.24	A	7.6	6.2	4.4	3.4	2.5	2.6	5.1	1.4	1.2	261	249	163	146	876	157	.015	0	.022	.013	.119	.048
6-70	1.2	1.23	F	6.9	3.3	3.5	6.2	3.8	2.9	4.2	1.2	1.1	149	316	131	278	1021	129	.016	0	.034	.015	.127	.052
7-71	1.10	1.26	G	8.1	3.0	5.7	5.2	1.6	2.1	4.8	1.4	1.4	700	183	.522	146	759	401	.016	0	.029	.048	.108	.044
8-72	1.2	1.26	C	6.6	2.2	3.1	3.1	4.5	2.9	3.8	1.1	1.2	732	349	799	263	.744	687	.019	0	.031	.061	.111	.051
9-73	1.2	1.28	G	5.8	2.7	5.7	4.3	1.6	2.1	4.2	1.1	1.2	700	199	.506	146	716	429	.014	0	.029	.041	.086	.068
10-74	1.14	1.25	H	7.5	3.9	6.1	3.7	1.3	2.1	3.8	Vo	d	995	316	.783	.190	770	.640	.016	0	.036	.063	.080	.068
11-75	1.2	1.22	D	5.6	4.2	3.1	4.0	4.1	2.8	3.5	Vo	d	.979	.349	930	219	.598	830	.023	0	.038	.073	.070	.071
12-76	1.2	1.26	H	5.8	4.8	7.9	4.0	2.5	4.3	5.8	1.1	1.2	893	299	652	146	730	558	.016	0	.034	.063	.083	.092
13-77	1.18	1.21	A	5.3	5.1	4.4	3.4	2.9	3.9	3.3	1.5	1.5	285	183	179	.146	1.09	143	.019	0	.019	.017	.122	.037
14-78	1.19	1.20	F	7.3	3.3	4.0	5.2	2.5	3.6	3.2	1.2	1.2	124	.183	065	146	1051	029	.012	.002	.022	.013	.143	.043
15-79	1.2	1.22	A	4.8	2.6	4.4	5.4	2.9	6.4	5.4	2.6	2.1	223	166	.065	.133	1037	.129	.014	0	.014	.015	.165	.043
16-80	1.2	1.26	B	5.5	6.0	5.1	2.8	1.6	2.1	4.8	1.2	1.2	422	.166	473	146	.759	.386	.027	0	.029	.040	.133	.068
17-81	1.2	1.26	E	7.0	2.4	3.2	5.3	3.5	3.2	3.8	1.2	1.1	.595	.282	326	232	744	.401	.023	0	.034	.033	.127	.068
18-82	1.2	1.25	B	6.8	6.3	6.1	2.5	1.6	3.5	4.2	1.2	1.2	.397	.183	392	.175	1359	286	.025	.002	.026	.040	.158	.068
19-83	1.2	1.21	C	7.0	3.9	2.2	2.8	1.9	3.5	3.5	2.3	2.3	.608	282	538	278	968	.501	.019	0	.029	.052	.111	.051

Structural Response Program

Compiled By: [illegible]

Date: 15:15:120 65
House: W-6

Phase 2-B 1-17-65 Run	Alt	[illegible]	[illegible]	Fire Card W	Pressure (psf) 1 N Wall N	2 E Wall E	3 S Wall S	4 W Wall W	5 W Roof	6 E Roof	7 Big Room	8 Small Room	Displacement 1 N Wall N Cor E-W	2 N Wall E Cor N-S	3 E Wall S Cor E-W	4 S Wall W Cor N-S	5 Inter Wall N-S	6 [illegible]	Acceleration (g) 1 N Wall W Cor N-S	2 E Wall N Cor E-W	3 S Wall E Cor N-S	4 W Wall S Cor E-W	5 Inter Wall N-S	6 Roof V
20-84	1.2	1.24	G	5.7	2.4	4.0	4.0	1.6	2.1	3.5	1.5	1.7	620	149	473	146	759	429	.014	.004	.026	.046	.106	.057
21-85	1.19	1.24	C	6.6	5.1	2.6	2.8	2.9	2.5	3.2	2.2	2.0	.595	249	489	.232	700	.472	.019	0	.031	.050	.127	.060
22-86	1.195	1.21	D	7.2	2.1	0.8	2.5	2.2	1.4	1.7	1.8	1.8	.608	219	457	.161	833	.410	.021	0	.031	.045	.095	.145
23-87	1.20	1.24	H	5.8	4.8	2.5	4.9	2.8	2.8	5.1	1.4	1.7	930	.199	783	.219	876	658	.123	.007	.036	.071	.099	.060
24-88	1.20	1.24	D	8.5	3.3	2.6	4.6	2.8	2.9	4.2	1.2	1.1	1041	.332	.532	263	.598	858	.025	.022	.043	.078	.092	.092
25-89	1.19	1.25	E	5.5	3.3	3.1	8.9	1.3	5.0	6.1	1.4	1.4	740	.332	506	.292	1.300	558	.027	0	.043	.046	.155	.076
26-90	1.17	1.25	B	6.2	6.0	2.3	2.8	2.2	2.5	3.8	1.2	1.7	.972	166	431	.015	.891	.321	.012	0	.026	.046	.147	.055
27-91	1.2	1.26	E	6.4	2.4	2.6	5.9	4.1	2.5	3.5	1.2	1.5	.608	.266	.441	.190	.833	429	.026	0	.034	.038	.121	.060
28-92	1.2	1.20	F	6.9	3.9	4.9	6.2	3.2	2.5	3.2	1.5	1.2	120	.166	107	146	.920	.110	.021	.004	.022	.019	.186	.048
29-93	1.2	1.20	A	8.4	5.7	4.0	3.4	3.2	3.9	4.8	1.4	1.4	.351	116	.101	.175	1139	.157	.023	0	.026	.027	.160	.043
30-94	1.2	1.20	F	7.1	5.3	4.0	6.7	3.2	3.6	4.8	1.4	0.8	120	149	131	.112	876	110	.014	.002	.022	.017	.027	.055
End																								

Structural Response Program

Coupled By R C C

Date 1-5-65: 1-28-65

House W-0

Phase 2-R				Pressure (p.s.f.)										Displacement (in.)						Acceleration (g)							
1-18-65				Free Field	1 N Wall N	2 E Wall E	3 S Wall S	4 W Wall W	5 W Roof	6 K Roof	7 Elk Room	8 Control Room		1 N Wall N Cor E-W	2 E Wall E Cor N-S	3 S Wall S Cor E-W	4 W Wall W Cor N-S	5 Inter Walls N-S	6 Inter Floors E-W		1 N Wall W Cor N-S	2 E Wall N Cor E-W	3 S Wall E Cor N-S	4 W Wall S Cor E-W	5 Inter Walls N-S	6 Roof V		
Run	Alt	Mach No.	Veh																								
1-95	120	1.20	G	4.5	2.7	5.2	6.2	2.8	4.8	4.7	NR	1.1		447	136	533	151	800	231		014	004	029	042	109	061		
2-96	12.	1.26	C	5.6	4.9	2.0	2.5	2.0	3.8	3.2	NR	0.8		447	248	691	226	675	529		019	002	026	042	090	053		
3-97	122	1.25	G	7.4	2.4	4.0	5.3	1.6	3.8	4.1	NR	0.8		(No Record)							012	003	028	042	116	058		
4-98	12.	1.25	H	6.4	4.3	3.2	4.4	2.4	3.2	4.6	NR	0.8		1.044	236	806	211	869	616		023	004	034	089	085	067		
5-99	12.	1.23	D	6.4	2.7	2.0	4.1	3.2	3.5	3.5	NR	2.3		(No Record)							021	002	036	053	109	066		
6-100	119	1.25	H	5.1	(No Record)						NR	0.8									016	002	034	057	083	064		
7-101	12.	1.20	A	5.4	6.1	2.6	3.6	3.6	4.4	4.4	1.4	1.5		-	-	-	-	-	-		019	002	034	019	138	058		
8-102	121	1.22	F	5.8	3.6	3.6	6.8	3.6	4.7	4.4	1.6	1.1		145	186	173	136	941	139		016	002	019	019	152	056		
9-103	12.	1.25	A	6.3	6.1	2.8	3.4	3.6	5.1	4.7	1.4	1.5		383	136	158	151	926	185		019	002	024	017	147	053		
10-104	119	1.21	A	4.8	6.4	5.2	2.8	2.4	4.1	4.7	1.1	1.7		423	136	447	136	800	385		019	002	024	038	115	053		
11-105	12.	1.23	E	5.1	2.7	2.4	5.0	6.9	3.2	3.2	1.4	0.8		670	260	547	181	785	520		021	004	036	036	127	058		
12-106	12.	1.23	A	5.3	4.8	5.2	3.1	2.8	4.4	4.7	1.2	1.8		542	223	576	151	785	446		025	002	031	048	115	056		
13-107	12.	1.25	C	5.6	5.5	2.0	2.8	4.9	3.8	3.2	1.6	0.9		872	384	835	272	753	755		025	002	036	067	099	064		
14-108	12	1.25	G	4.5	4.8	2.8	2.8	2.0	1.9	2.3	0.9	0.7		555	129	417	091	503	339		009	006	022	036	070	048		
15-109	12	1.27	C	4.7	(No Record)						1.2	0.9		792	360	720	257	753	677		023	002	031	052	112	080		
16-110	12.	1.26	H	5.1							3.1	2.2		898	248	770	151	942	646		016	004	029	059	120	074		
17-111	12.	1.25	D	5.4							1.2	1.2		929	372	935	166	690	729		023	002	038	067	083	058		
18-112	12.	1.29	H	5.1							1.6	1.5		990	298	898	257	852	770		023	002	038	073	094	065		
19-113	118	1.20	E	4.5							1.6	0.6		624	372	562	257	1 042	569		023	002	038	038	139	058		

Structural Response Program

Coupled By _____

Date 1-5-65: 1-28-65

House W-0

Phase 2-R				Pressure (p.s.f.)										Displacement (in.)						Acceleration (g)							
1-18-65				Free Field	1 N Wall N	2 E Wall E	3 S Wall S	4 W Wall W	5 W Roof	6 K Roof	7 Elk Room	8 Control Room		1 N Wall W Cor N-S	2 E Wall N Cor E-W	3 S Wall E Cor N-S	4 W Wall S Cor E-W	5 Inter Walls N-S	6 Inter Floors E-W		1 N Wall W Cor N-S	2 E Wall N Cor E-W	3 S Wall E Cor N-S	4 W Wall S Cor E-W	5 Inter Walls N-S	6 Roof V		
Run	Alt	Mach No.	Veh																								
20-114	117	1.20	A	6.4							1.6	1.8		503	273	562	151	1068	816		021	002	034	046	150	065		
21-115	12.	1.20	E	9.7							1.6	0.6		766	384	576	257	942	616		027	002	036	040	122	058		
22-116	12.	1.24	F	5.2							1.6	1.2		132	179	144	136	942	123		016	004	014	017	123	053		
23-117	121	1.25	A	6.6							1.2	NR		330	136	173	151	800	169		021	0	019	017	127	048		
24-118	12	1.25	F	6.2							1.6	1.2		145	260	207	151	1535	139		021	004	024	023	026	058		
25-119	12.	1.28	G	6.6							1.2	1.2		681	197	509	151	957	446		014	008	029	052	114	067		
26-120	119	1.30	C	6.2							1.6	0.6		779	348	706	272	963	677		023	0	029	059	099	029		
27-121	121	1.31	G	5.1							1.2	0.9		647	211	489	151	800	416		014	004	024	048	087	052		
28-122	118	1.22	D	8.0							1.2	1.2		806	372	564	257	502	847		021	002	034	062	065	058		
29-123	12.	1.21	H	4.7							1.6	1.5		912	360	818	272	942	756		023	004	036	073	087	068		
30-124	12.	1.20	D	4.2							1.6	1.5		753	372	763	166	487	739		021	002	034	061	0	038		
End																											

STRUCTURAL RESPONSE PROGRAM

COMPILED BY G.L.C.C.

DATE HS-65:1-20-65

HOUSE W-6

PHASE 2-B				PRESSURE (p.s.f.)										DISPLACEMENT (in.²)						ACCELERATION (g)								
1-19-65				Free Field	1 N Wall N	2 E Wall E	3 S Wall S	4 W Wall W	5 W Roof	6 E Roof	7 Bdrm Room	8 Bdrm Room		1 N Wall N Cor E-W	2 N Wall E Cor N-S	3 E Wall S Cor E-W	4 W Wall S Cor N-S	5 Inter Wall N-S	6 Inter Wall E-W		1 N Wall W Cor N-S	2 E Wall N Cor E-W	3 S Wall E Cor N-S	4 W Wall S Cor E-W	5 Inter Wall N-S	6 Roof V			
Run	Ref	Hour	Veh	W	N	E	S	W																					
1-125	12	125	F	6.4	3.3	4.5	6.8	2.5	4.2	4.1	2.4	1.6		120	179	33	130	847	113		012	004	002	009	158	048			
2-126	288	162	F	2.0	1.2	1.5	1.5	1.7	1.7	1.2	0.6	0.5		048	048	109	029	345	042		007	0	010	010	038	016			
3-127	30	143	A	2.2	2.1	1.5	1.2	0.8	2.0	1.6	N	R		096	020	085	010	823	010		007	0	010	008	047	016			
4-128	12	126	A	8.1	6.4	7.0	3.1	2.9	2.3	5.3	N	R		360	012	502	003	1.359	310		009	002	017	042	158	059			
5-129	12	125	E	4.8	2.7	3.0	5.9	4.6	2.3	4.4	N	R		450	310	387	216	1.118	353		021	002	034	029	100	057			
6-130	11	125	A	5.2	6.4	6.0	3.3	1.7	2.7	3.8	N	R		480	131	618	130	700	923		016	002	019	048	148	055			
7-131	12	125	C	4.2	6.4	2.5	2.8	4.2	2.7	4.1	1.9	1.6		600	262	642	288	1.095	569		023	002	024	056	130	078			
8-132	12	126	G	6.0	3.0	6.0	4.6	2.5	2.3	4.6	2.5	1.3		496	250	726	317	961	677		019	002	029	050	130	071			
9-133	12	129	C	8.1	2.6	3.0	7.8	6.3	4.0	6.2	1.9	1.6		(	V	.	(| . |)		023	0	024	054	183	104			
10-134	12.1	125	D	6.9	3.0	2.5	3.7	5.5	3.3	4.1	1.6	1.3		684	333	775	259	589	677		025	002	036	061	074	064			
11-135	119	129	H	4.0	3.0	5.0	3.1	2.8	2.0	3.1	1.3	0.9		612	210	710	158	716	550		019	002	022	052	077	041			
12-136	118	120	D	6.5	3.3	2.5	4.3	5.0	3.4	4.1	1.9	1.6		720	357	847	274	613	705		025	002	036	063	094	087			
13-137	25	133	F	4.7	3.0	3.5	4.3	2.5	2.3	3.1	NR	1.9		240	095	230	029	220	115		012	0	014	021	083	030		13-5B	
14-138	25	129	F	3.4	3.0	4.0	4.0	2.5	2.1	4.1	2.8	2.5		252	121	228	058	922	169		009	002	014	027	123	032		13-5B	
15-139	116	122	E	10.8	3.0	4.0	7.7	8.4	4.7	6.2	2.1	1.6		468	381	472	303	876	923		027	002	043	038	158	084			
16-140	25	135	E	3.1	2.7	3.5	4.0	2.5	1.7	3.1	2.5			228	155	230	130	1.077	155		014	0	019	021	118	041		13-5B	
17-141	12	125	B	5.1	4.3	4.0	2.5	2.5	2.0	2.5	2.4	2.2		264	107	375	115	499	296		009	002	014	035	148	037			
18-142	25	135	F	3.1	2.4	3.0	3.3	2.1	1.7	2.5	2.5	2.5		216	107	245	091	524	141		012	0	017	017	100	032		13-5B	
19-143	12	122	E	6.0	2.4	3.0	4.6	4.2	2.0	2.8	1.9	0.6		480	333	387	259	589	423		023	002	031	037	130	051			

STRUCTURAL RESPONSE PROGRAM

COMPILED BY _____

DATE HS-65:1-20-65

HOUSE W-6

PHASE 2-B				PRESSURE (p.s.f.)										DISPLACEMENT (in.²)						ACCELERATION (g)								
1-19-65				Free Field	1 N Wall N	2 E Wall E	3 S Wall S	4 W Wall W	5 W Roof	6 E Roof	7 Bdrm Room	8 Bdrm Room		1 N Wall W Cor N-S	2 N Wall E Cor N-S	3 E Wall S Cor E-W	4 W Wall S Cor N-S	5 Inter Wall N-S	6 Inter Wall E-W		1 N Wall W Cor N-S	2 E Wall N Cor E-W	3 S Wall E Cor N-S	4 W Wall S Cor E-W	5 Inter Wall N-S	6 Roof V			
Run	Ref	Hour	Veh	W	N	E	S	W																					
20-144	25	135	F	3.5	2.7	3.0	3.3	2.5	1.7	2.5	2.8	2.3		216	119	.	056	599	155		012	0	019	021	110	030		13-5B	
21-145	30	140	F	2.0	0.6	4.0	1.5	0.8	1.7	0.9	0.6	0.5		048	029	073	010	307	042		004	0	007	010	038	011			
22-146	30	13	F	1.4	0.7	4.0	1.2	0.8	0.3	0.6	0.6	0.5		096	029	020	010	282			007	0	007	010	044	011			
23-147	30	16	F	2.2	0.9	4.5	1.8	0.8	0.7	1.2	0.6	0.5		1120	036	107	041	307	099		004	0	012	013	054	016			
24-148	12	128	A	5.6	4.6	4.5	2.5	2.9	2.7	3.8	1.9	1.6		432	407	133	130	1.225	099		016	0	020	013	148	058			
25-149	119	121	G	4.1	2.4	5.0	4.3	2.5	2.3	3.1	1.1	1.5		1	(	W	.	.	)		014	004	034	031	152	047			
26-150	121	121	C	5.9	6.2	3.5	3.3	5.5	2.7	3.8	2.7	1.6		- -							025	002	036	044	148	059			
27-151	122	122	G	6.7	3.0	7.0	5.6	2.8	2.7	4.4	3.1	1.3		629	357	605	259	1.605	536		023	006	034	058	249	081			
28-152	12	125	H	4.4	4.3	6.0	3.2	2.8	2.7	4.4	N	R		598	179	703	199	993	607		019	002	022	059	087	021			
29-153	12	65	D	6.4	3.0	2.5	3.3	6.3	2.0	4.1	1.6	1.6		620	345	763	289	730	696		023	002	036	063	094	059			
30-154	12	125	H	5.4	4.0	6.5	3.3	3.4	2.3	3.4	1.6	2.4		600	760	807	173	700	082		016	004	022	059	082	059			
31-155	12	120	A	4.1	4.0	3.5	2.5	2.9	1.7	2.2	2.5	2.4		132	119	133	086	1.183	099		014	0	014	033	166	032			
32-156	12	123	F	7.4	2.7	4.0	5.9	3.8	3.0	3.5	2.5	1.6		226	235	310	173	1.620	282		019	004	002	027	208	057			
33-157	12	125	A	6.4	6.1	3.5	4.1	4.2	4.4	4.1	2.1	2.5		168	167	157	155	1594	155		019	012	032	019	033	062			
Grid																													

STRUCTURAL RESPONSE PROGRAM

COMPILED BY PACC

DATE: 5-15-1200 62

HOUSE W-6

PHASE 2-A				PRESSURE (psf)									DISPLACEMENT (in.)						ACCELERATION (g)					
1-20-65				FREE FIELD	1 N WALL N	2 E WALL E	3 S WALL S	4 W WALL W	5 W ROOF	6 E ROOF	7 BIG ROOM	8 SMALL ROOM	1 W WALL MID E-W	2 W WALL E COR N-S	3 E WALL E COR E-W	4 E WALL S COR N-S	5 INTER WALL N-S	6 INTER WALL E-W	1 W WALL MID E-W	2 E WALL S COR E-W	3 S WALL MID N-S	4 W WALL S COR E-W	5 INTER WALL N-S	6 ROOF V
RUN	ALT	HEAD	VEL	psf																				
1-158	118	126	R	5.7	6.0	5.6	2.8	1.8	3.2	3.1	2.1	2.1	.976	.150	.581	.117	1.209	.308	.011	.002	.019	.002	.143	.066
2-159	12.	128	C	10.0	6.6	3.1	2.5	2.8	5.5	6.6	IV	K*	.773	.136	.609	.132	.845	.602	.019	0	.019	.005	.087	.051
3-160	12	13	G	7.4	4.1	3.0	2.5	2.9	8.0	7.0	/	<	.960	.408	.826	.278	1.139	.560	.025	.004	.031	.003	.167	.125
4-161	12.	13	C	5.3	4.7	2.6	2.5	3.6	2.6	2.8	/	/	.610	.150	.439	.146	.936	.420	.019	0	.023	.002	.077	.043
5-162	30	14	F	2.0	0.9	1.5	1.6	1.1	2.6	1.1	0.8	0.6	.122	.068	.118	.132	.076	.010	.004	0	.007	.002	.024	.009
6-163	30	13	F	1.6	0.6	0.7	0.9	0.4	0.2	0.6	0.6	0.9	.097	.027	.826	.015	.438	.010	.007	0	.005	.006	.049	.014
7-164	46	14	F	0.9	0.6	0.7	0.9	0.7	0.6	0.6	0.9	0.5	.097	.027	.963	.014	.787	.010	.004	0	.007	.010	.036	.009
8-165	119	121	D	4.5	3.2	2.0	2.8	1.8	2.9	2.5	1.9	1.9	.598	.136	.508	.117	.570	.390	.016	0	.014	.038	.068	.055
9-166	121	126	H	2.8	2.2	1.6	1.8	1.8	4.2	3.4	2.8	2.8	.859	.272	.826	.239	.554	.588	.016	.002	.024	.058	.160	.078
10-167	12.	120	D	4.7	3.2	2.0	2.5	3.6	2.9	2.0	1.6	1.5	.892	.245	.708	.146	.493	.602	.019	0	.020	.060	.058	.048
11-168	11.9	139	E	9.3	7.2	3.1	5.8	5.0	5.8	5.0	2.8	2.5	1.027	.408	.708	.448	1.209	.588	.027	0	.036	.058	.153	.109
12-169	12	130	A	8.1	5.5	6.1	7.2	5.5	4.2	3.9	2.1	2.1	.443	.231	.136	.175	2.059	.392	.013	0	.014	.040	.228	.046
13-170	115	130	E	4.1	1.9	1.9	2.5	2.9	2.9	2.5	1.6	1.2	.610	.258	.460	.214	.740	.420	.019	0	.019	.036	.068	.045
14-171	12.	128	F	4.7	2.5	4.1	4.1	2.5	2.9	2.2	2.2	2.5	.700	.258	.226	.146	1.223	.140	.013	0	.019	.022	.132	.048
15-172	12	128	A	5.5	5.0	4.1	2.3	1.6	4.2	2.9	2.5	1.9	.766	.150	.234	.230	1.510	.252	.023	0	.014	.018	.165	.063
16-173	117	130	F	4.7	(NO	RE	CO	RD	)		2.5	1.2	.708	.408	.234	.292	1.660	.154	.019	.002	.029	.020	.162	.059
17-174	12	125	G	5.5	2.5	5.6	4.7	2.9	3.2	2.8	2.5	1.2	.697	.391	.590	.248	1.660	.420	.019	.002	.019	.042	.162	.059
18-175	12.	130	C	5.6	6.2	3.0	3.2	2.4	4.5	4.5	2.2	1.5	.903	.254	.826	.292	.876	.420	.027	0	.013	.069	.097	.057
19-176	12	126	G	2.8	2.8	1.04	2.8	3.6	2.5	2.6	2.5	1.2	1.100	.408	.826	.292	1.209	.602	.023	.004	.029	.058	.132	.076

STRUCTURAL RESPONSE PROGRAM

COMPILED BY PACC

DATE: 5-15-1200 65

HOUSE W-6

PHASE 2-A				PRESSURE psf									DISPLACEMENT (x 10^{-2} in.)						ACCELERATION *g*					
1-21-65				FREE FIELD	1 N WALL N	2 E WALL E	3 S WALL S	4 W WALL W	5 W ROOF	6 E ROOF	7 BIG ROOM	8 SMALL ROOM	1 W WALL MID E-W	2 W WALL E COR N-S	3 E WALL E COR E-W	4 E WALL S COR N-S	5 INTER WALL N-S	6 INTER WALL E-W	1 W WALL MID E-W	2 E WALL S COR E-W	3 S WALL MID N-S	4 W WALL S COR E-W	5 INTER WALL N-S	6 ROOF V
RUN	ALT	HEAD	VEL	psf																				
1-177	12.	130	H	5.2	5.2	8.9	5.0	3.0	4.9	4.9	1.5	1.6	.833	.554	.811	.302	1.072	.598	.021	0	.002	0	.090	0
2-178	12.	128	D	4.1	2.5	2.5	6.0	4.1	3.5	2.4	1.5	1.2	.843	.397	.667	.453	.969	.706	.019	0	.002	.002	.027	0
3-179	12.	130	H	6.8	7.4	11.0	4.0	3.7	5.9	6.7	1.8	1.9	.952	.384	.899	.317	1.232	.735	.023	0	.005	.002	.123	0
4-180	12.	130	A	6.7	6.5	8.6	4.0	4.1	5.6	4.6	1.5	1.6	.957	.151	.208	.151	.938	.279	.019	0	0	.002	.167	.062
5-181	12	131	F	4.6	3.4	4.3	6.7	4.5	2.7	5.5	1.5	1.2	.119	.288	.208	.187	1.849	.147	.016	0	0	.002	.120	.082
6-182	12	130	A	4.9	2.7	4.3	3.7	3.7	5.6	6.1	1.5	1.6	.957	.137	.222	.151	1.796	.294	.019	0	.014	.002	.167	.060
7-183	12.1	130	A	5.3	5.5	5.7	5.0	2.6	3.8	3.7	1.5	1.6	.583	.151	.813	.151	1.408	.294	.019	0	.007	0	.112	.052
8-184	12.1	130	E	4.8	2.5	2.9	6.4	3.4	5.2	4.3	1.5	1.6	.466	.397	.384	.187	1.232	.426	.021	0	.005	.002	.114	.044
9-185	12.1	131	B	4.3	4.6	5.7	3.0	1.9	3.8	3.3	1.2	1.6	.476	.137	.347	.151	1.40*	.294	.014	0	.007	0	.127	.044
10-186	12.0	130	C	5.6	4.9	3.2	3.4	3.4	3.1	3.0	1.2	1.6	.833	.302	.611	.226	1.056	.647	.023	0	.006	.035	.130	.041
11-187	12.	130	G	4.2	2.5	7.1	7.1	4.1	4.5	4.6	1.5	1.2	.595	.345	.500	.151	1.235	.382	.016	0	.009	.004	.114	.054
12-188 R-50	12	130	C	7.4	7.4	3.2	5.0	5.2	6.3	5.2	1.5	1.6	.900	.311	.901	.187	1.446	.135	.023	0	.006	.065	.166	.067
13-189	25	136	F	2.5	1.8	3.6	3.7	2.9	2.4	2.4	1.2	0.9	.143	.123	.151	.060	.568	.118	.009	0	.004	.016	.012	.025
14-190 N-58	12.	129	D	5.3	3.8	2.5	3.4	2.6	3.8	3.0	1.5	1.2	.918	.391	.751	.187	.565	.750	.023	0	.029	.064	.052	.057
15-191	25.	130	A	2.9	4.0	2.8	2.7	3.0	2.8	2.7	1.5	1.6	.138	.123	.264	.121	.109	.166	.011	0	.004	.002	.065	.027
16-192 R-58	12.	131	H	3.5	3.4	6.8	4.0	3.2	4.9	4.6	1.2	1.2	.114	.553	.272	.121	.567	.527	.016	0	.004	.049	.053	.073
17-193	25.	130	F	3.1	2.8	5.3	5.0	6.0	4.2	3.7	1.5	1.2	.126	.137	.609	.014	.556	.101	.009	0	.014	.021	.058	.051
18-194 R-58	12.	130	D	4.9	4.3	3.2	4.4	5.6	5.2	4.6	1.5	1.6	1.035	.411	.713	.262	.556	.582	.023	.002	.037	.026	.010	.061
19-195	25.	136	A	2.9	2.8	2.1	2.4	2.2	2.8	2.4	1.2	1.6	.202	.137	.115	.076	.516	.166	.011	0	.012	.018	.058	.035

D-35

STRUCTURAL RESPONSE PROGRAM

COUPLED
BY _____

DATE HS-65:1-20-65
HOUSE 41-6

PHASE 2-B				PRESSURE psf									DISPLACEMENT ($\times 10^{-2}$ IN)						ACCELERATION "g"					
1-21-65				FREE FIELD	1 N WALL N	2 E WALL E	3 E WALL S	4 W WALL W	5 W ROOF	6 E ROOF	7 E&W ROOF	8 CENTER ROOF	1 W WALL N COR E-W	2 E WALL S COR N-S	3 E WALL S COR E-W	4 W WALL S COR N-S	5 INTER WALL N-S	6 W WALL INTER E-W	1 W WALL N COR N-S	2 E WALL N COR E-W	3 E WALL S COR N-S	4 W WALL S COR E-W	5 INTER WALL N-S	6 ROOF V
RUN	ALT	MACH	VAC																					
20-196 A-58	25	1.31	F	2.6	2.5	2.2	4.0	1.9	2.5	2.3	1.2	1.2	.093	.151	.139	.076	.528	.088	.087	0	.010	.012	.060	.043
21-197 A-58	25	1.35	A	2.5	4.3	2.9	2.4	2.4	2.8	2.4	1.2	1.6	.143	.137	.139	.151	.810	.132	.014	0	.014	.016	.092	.062
22-198 B-58	25	1.36	F	3.2	2.5	2.9	5.0	2.2	3.1	2.7	1.2	0.9	.119	.137	.139	.091	.709	.132	.007	0	.012	.016	.022	.051
23-199	12.1	1.31	E	6.8	2.5	7.6	7.1	5.2	5.6	4.9	1.5	1.6	.107	.5?4	.278	.302	1.584	.371	.027	0	.044	.027	.142	.076
24-200	12	1.30	A	2.9	4.6	5.2	2.0	3.7	2.5	3.3	1.5	1.9	.476	.758	.542	.272	.880	.559	.025	0	.026	.043	.120	.054
25-201 A-58	12	1.30	E	5.3	2.5	9.2	6.7	5.6	5.2	2.7	1.5	1.2	.785	.411	.528	.302	.650	.632	.023	0	.035	.045	.105	.076
26-202 A-58	25	1.35	F	4.6	3.4	4.6	7.4	2.2	3.8	4.0	1.5	1.6	.131	.206	.181	.151	.898	.132	.014	0	.032	.023	.117	.067
27-203 B-58	12.1	1.30	D	4.9	4.3	7.0	4.4	4.1	5.9	4.6	1.5	1.2	.976	.411	.931	.302	.913	.867	.021	0	.035	.058	.077	.053
28-204 B-58	25	1.32	A	...	(NO		RECO	RD)						(NO					.021	0	.026	.058	.085	.051
29-205	12	1.30	A	3.7	5.7	6.6	3.4	2.2	4.4	4.3	1.5	1.2	.773	.348	.695	.191	.915	.647	.007	0	.012	.016	.070	.030
30-206 B-58	25.	1.35	F	2.8	1.5	2.5	2.9	1.3	1.9	1.7	1.2	1.2	.107	.123	.125	.076	.616	.058	.009	0	.010	.012	.107	.035
31-207 B-58	24.5	1.33	A	3.8	4.0	2.7	3.2	2.2	2.2	2.6	1.5	1.6	.279	.110	.139	.060	.880	.162	.014	0	.029	.005	.138	.098
32-208 B-58	25.5	1.35	F	1.1	4.3	5.2	4.9	3.2	4.1	4.4	1.8	1.6	.119	.270	.250	.226	1.232	.132	.009	0	.010	.016	.055	.032
33-209 B-58	24.5	1.32	A	2.6	4.5	2.1	2.4	2.4	4.5	2.2	0.9	1.6	.119	.110	.125	.076	.598	.118	.003	.002	.037	.086	.095	.058
34-210 A-58	12	1.33	H	8.5	4.8	6.6	4.9	2.5	4.9	4.6	1.5	1.9	1.228	.621	1.112	.272	1.021	1.014	.011	0	.022	.025	.114	.067
35-211 A-58	25.3	1.36	E	3.1	2.2	3.7	4.2	2.0	5.0	3.7	1.5	1.6	.167	.176	.222	.091	1.072	.167	.023	0	.037	.028	.053	.044
36-212 A-58	12.	1.28	D	3.6	3.1	2.7	2.4	3.9	3.2	3.0	1.2	1.2	.752	.411	.241	.302	.704	.735	.011	0	.012	.016	.065	.021
37-213 A-58	25.	1.36	A	2.9	3.2	2.0	1.8	1.1	2.6	2.3	0.9	1.2	.155	.110	.139	.045	.616	.132	.007	0	.016	.025	.090	.041
39-215 A-58	25.	1.32	E	1.1	3.2	4.6	2.9	2.2	4.2	3.2	1.5	2.8	.191	.123	.181	.045	.880	.167	.016	0	.024	.056	.102	.067

STRUCTURAL RESPONSE PROGRAM

COUPLED
BY _____

DATE HS-65:1-20-65
HOUSE 41-6

PHASE 2-B				PRESSURE psf									DISPLACEMENT ($\times 10^{-2}$ IN)						ACCELERATION "g"					
1-21-65				FREE FIELD	1 N WALL E	2 E WALL S	3 E WALL S	4 W WALL W	5 W ROOF	6 E ROOF	7 E&W ROOF	8 CENTER ROOF	1 W WALL N COR E-W	2 E WALL S COR N-S	3 E WALL S COR E-W	4 W WALL S COR N-S	5 INTER WALL N-S	6 W WALL INTER E-W	1 W WALL N COR N-S	2 E WALL N COR E-W	3 E WALL S COR N-S	4 W WALL S COR E-W	5 INTER WALL N-S	6 ROOF V
RUN	ALT	MACH	VAC																					
40-214	12.	1.3	G	6.0	2.8	6.4	6.4	3.2	5.6	4.3	1.5	0.9	.714	.411	.556	.181	1.034	.559	.021	0	.024	.043	.132	.037
41-217	11.9	1.28	C	5.2	4.6	3.0	3.2	3.2	4.0	3.3	1.5	1.6	.714	.274	.444	.166	1.408	.573	.019	0	.022	.009	.083	.043
42-218	12	1.31	G	5.2	2.5	4.3	3.7	3.0	3.0	2.6	1.2	0.6	.821	.302	.556	.151	.880	.573	.027	0	.035	.028	.095	.082
43-219	12	1.31	H	7.9	4.9	9.1	4.9	3.5	5.4	5.5	1.5	1.6	1.072	.439	.834	.187	1.232	.735	.021	0	.035	.046	.050	.044
44-220	11.9	1.30	D	4.8	2.8	2.7	3.9	3.2	5.0	3.8	1.2	1.2	.845	.397	.695	.302	.704	.735	.025	0	.044	.046	.088	.062
45-221	11.7	1.31	H	8.8	4.5	7.5	3.9	2.2	5.2	4.9	1.5	1.6	.834	.411	.806	.787	1.021	.647	(NO RECORD)					
END																								

STRUCTURAL RESPONSE ROSTROLL

COUPLED BY _____

DATE 4-15-1 TO 1-5

HOUSE WJ-6

PHASE 2-R — 1-22-65

RUN	REF	WIND	VEL	PRESSURE psf: FREE FIELD	1 N WALL	2 E WALL	3 S WALL	4 W WALL	5 W ROOF	6 E ROOF	7 S ROOF	8 CENTER ROOF	DISPLACEMENT (X10⁻² IN): 1	2	3	4	5	6	ACCELERATION "g": 1	2	3	4	5	6
													WALL COR E-W	WALL COR N-S	E COR E-W	E COR N-S	INTER WALL N-S	INTER ROOF E-W	WALL COR N-S	E COR E-W	E COR N-S	WALL COR E-W	INTER WALL N-S	ROOF V
1-224	12	1.1	A	.1N	5.2	5.2	2.5	2.5	5.9	4.7	1.5	1.6	253	.24	151	220	1683	1.6		(NO	RECORD)			
2-225	12	131	F	3.5	2.6	3.1	2.9	2.1	3.2	3.0	1.2	1.2	203	214	220	147	984	166	.016	0	.022	.015	.126	.025
3-226	12	132	N	1.6	4.6	4.0	3.0	2.3	6.1	3.5	1.2	1.6	267	198	170	137	1422	166	.016	0	.017	.013	.127	.059
4-225	12	127	A	.01	4.3	9.0	3.2	2.5	6.0	6.3	1.2	1.6	622	171	371	147	1071	.342	.019	0	.019	.036	.087	.046
5-226	12	126	E	.09	2.9	3.4	6.8	4.8	5.1	4.7	1.5	1.6	624	028	.348	.294	1723	.478	.021	0	.041	.028	.137	.055
6-227	12	127	A	3.1	(NO	RECORD)					1.5	1.6	301	193	510	191	071	513	.016	0	.017	.018	.103	.027
7-228	119	1.3	C	4.3	3.8	3.2	2.9	2.1	3.6	3.2	1.5	1.2	825	321	330	279	1.578	604	.023	0	.026	.052	.197	.098
8-229	12	131	G	3.7	4.3	4.7	3.8	3.5	2.8	2.9	1.5	1.6	788	310	568	147	780	445	.014	0	.024	.046	.083	.048
9-230	121	133	C	1.1	3.2	1.8	1.7	1.9	3.2	3.0	0.9	1.2	508	214	360	147	765	378	.011	0	.014	.031	.044	.030
10-231	6-21	10-12	F	1.6	1.2	1.6	1.7	1.0	1.3	1.2	0.6	0.3	178	107	114	143	993	136	.007	0	.017	.011	.019	.021
11-232	6-22	14-1	A	1.6	1.7	1.6	1.1	1.2	1.0	0.8	0.3	0.6	114	096	193	098	597	106	.004	0	.004	.008	.066	.027
12-233	6-20	14-14	F	2.2	1.8	1.1	0.9	0.8	0.5	0.8	0.3	0.6	140	054	176	049	543	091	.004	0	.001	.008	.038	.011
13-234	6-20	14-11	A	1.9	2.8	2.2	1.5	1.4	1.9	1.7	0.9	1.2	242	107	162	118	857	151	.009	0	.012	.015	.081	.043
14-235	119	135	E	4.5	2.3	3.4	6.8	5.0	5.1	4.2	NO	RE	517	224	345	264	1729	317	.019	0	.043	.027	.137	.076
15-236	1195	135	B	1.9	5.2	6.7	3.5	2.9	2.5	3.0	1.5	1.6	1.102	.300	469	299	1959	606	.023	0	.029	.053	.176	.043
16-237	12.0	131	E	4.4	1.8	2.0	4.0	2.9	2.5	2.4	1.4	0.8	292	219	129	147	918	166	.014	0	.024	.015	.107	.052
17-238	12	129	F	6.2	3.1	6.5	6.1	5.3	5.2	5.7	1.4	1.1	330	221	255	177	1.361	372	.019	0	.028	.038	.146	.087
18-239	10	1.3	N	3.9	(NO	RECORD)					1.4	1.4	381	225	237	220	1928	781	.021	0	.028	.017	.204	.066
19-240	11.0	115	F	2.3	5.7	9.4	13.2	9.3	8.5	8.6	2.3	1.6	381	529	464	382	2.414	372	.027	0	.043	.052	.297	.105

STRUCTURAL RESPONSE ROSTROLL

COUPLED BY _____

DATE 4-15-1 TO 1-5

HOUSE WJ-6

PHASE 2-R — 1-22-65

RUN	REF	WIND	VEL	PRESSURE psf: FREE FIELD	1 N WALL	2 E WALL	3 S WALL	4 W WALL	5 W ROOF	6 E ROOF	7 S ROOF	8 CENTER ROOF	DISPLACEMENT (X10⁻² IN): 1	2	3	4	5	6	ACCELERATION "g": 1	2	3	4	5	6
													WALL COR E-W	WALL COR N-S	E COR E-W	E COR N-S	INTER WALL N-S	INTER ROOF E-W	WALL COR N-S	E COR E-W	E COR N-S	WALL COR E-W	INTER WALL N-S	ROOF V
20-241	16	191	G	3.1	1.5	2.7	2.3	2.1	1.6	1.7	0.6	0.5	394	219	336	167	690	302	.009	0	.017	.029	.056	.021
21-242	16.5	1.61	C	1.4	1.4	0.7	0.9	1.7	0.8	0.8	0.5	0.3	229	107	116	118	887	151	.009	0	.012	.010	.010	.019
22-243	20.	12	G	0.9	NR	0.5	0.5	0.6	0.5	0.5	0.5	0.3	250	107	170	070	306	151	.004	0	.007	.011	.034	.011
23-244	3-21	16	F	2.6	1.4	2.0	2.6	1.7	1.4	2.0	0.8	0.6	127	193	116	132	459	065	.009	0	.017	.011	.026	.019
24-245	3-20	19	A	2.1	2.0	1.4	1.2	1.4	1.2	1.5	0.5	0.5	127	096	093	088	526	121	.009	0	.018	.008	.041	.032
25-246	3-26	16	F	1.6	1.2	2.0	2.3	1.4	1.3	1.7	0.6	0.6	110	139	116	118	470	091	.009	0	.012	.011	.058	.021
26-247	3-25	16	N	1.5	1.2	1.4	1.3	1.0	1.3	1.4	0.5	0.6	119	096	109	070	765	106	.009	0	.013	.010	.068	.025
27-248	25	191	A	1.5	1.1	1.1	0.9	1.4	1.6	1.2	0.3	0.3	119	096	093	059	420	091	.009	0	.010	.008	.049	.016
28-249	25	1.4	F	1.4	1.1	1.6	1.7	1.9	1.4	1.4	0.6	0.6	119	096	093	029	520	091	.007	0	.014	.015	.038	.016
29-250	25	1.4	A	1.6	1.5	1.1	0.8	1.0	1.1	1.2	0.3	0.3	127	096	093	069	470	166	.007	0	.010	.008	.047	.019
30-251	249	16	F	2.3	0.9	1.4	1.7	1.0	1.6	1.2	0.5	0.3	110	096	093	059	003	095	.007	0	.010	.010	.049	.021
31-252	25	1.5	A	0.6	1.4	1.2	0.6	0.8	0.6	0.6	0.1	0.4	140	045	116	029	199	136	.007	0	.010	.021	.017	.014
32-253	25	1.6	E	1.6	0.6	0.5	1.1	0.4	0.6	0.6	0.2	0.2	091	012	135	029	322	015	.004	0	.007	.010	.021	.014
33-254	25	1.5	R	1.1	0.8	0.9	0.5	0.4	0.5	0.5	0.3	0.3	121	054	116	049	522	136	.011	0	.012	.011	.030	.016
End																								

STRUCTURAL RESPONSE PROGRAM

COMPILED BY _____

DATE: HS-65: 1-20-65
HOUSE W-6

PHASE 2-R — 1-23-65

PRESSURE psf

RUN	Ref	Wind Vel	Dir	Free Field NW	1 N Wall N	2 E Wall E	3 E Wall S	4 W Wall W	5 W Roof	6 E Roof	7 Bed Room	8 Bath Room
1-255	119	125	C	NR	NO	RECORD					1.8	2.0
2-256	119	125	G	6.9							1.8	1.8
3-257	1193	129	C	4.6	2.9	2.0	2.0	2.9	2.8	2.1	1.6	1.6
4-258	113	130	D	4.1	3.0	2.6	2.8	3.3	3.2	3.1	2.6	1.8
5-259	12.	129	H	6.0	3.2	6.1	3.3	3.5	3.6	4.1	1.5	1.6
6-260	12	130	D	3.1	2.9	3.9	3.0	3.9	4.1	3.9	2.7	2.0
7-261	12.	128	E	6.7	3.0	3.4	2.6	6.2	4.9	4.7	1.5	1.2
8-262	12.	127	B	4.3	3.8	5.1	2.9	1.9	3.2	3.0	0.9	1.2
9-263	12	128	E	2.9	2.1	2.6	4.6	3.7	2.4	2.3	1.1	0.9
10-264	12	130	B	3.7	4.7	4.6	2.4	1.9	2.8	3.0	0.9	1.4
11-265	119	130	F	4.9	2.6	4.3	6.4	2.3	2.8	3.3	1.5	0.9
12-266	119	131	A	4.0	5.3	3.7	2.6	3.1	3.2	2.1	1.4	1.5
13-267	119	130	E	2.1	1.8	3.1	4.3	2.7	3.2	2.1	0.6	0.6
14-268 B-58	25	136	F	3.8	4.8	2.7	2.0	1.4	1.7	1.1	1.2	1.2
15-269 B-58	12	128	G	2.1	2.3	4.6	3.2	2.5	2.4	2.7	1.2	1.1
16-270 B-58	25	135	A	NR	4.9	4.4	3.3	3.3	3.2	3.3	1.6	1.8
17-271 B-58	124	129	C	3.8	5.6	3.4	2.0	3.9	2.8	3.0	1.6	1.6
18-272 B-58	25	136	F	4.1	3.7	4.3	4.7	2.9	4.0	3.9	1.5	1.3
19-273	12	126	G	5.7	2.4	5.4	4.7	3.9	4.4	5.1	1.6	1.4

DISPLACEMENT ($\times 10^{-2}$ in)

RUN	1 N Wall N-S	2 E Wall E-W	3 E Wall S-N	4 S Wall W-E	5 Inter Walls N-S	6 Inter Walls E-W
1-255	.590	.220	.538	.150	.349	.417
2-256	.718	.258	.560	.150	.760	.432
3-257	.626	.224	.571	.200	.178	.462
4-258	.720	.359	.672	.293	.914	.566
5-259	.900	.336	.784	.277	.775	.596
6-260	.826	.336	.590	.308	.775	.582
7-261	.718	.325	.448	.308	.485	.402
8-262	.590	.235	.437	.277	.471	.343
9-263	.672	.235	.310	.169	.775	.298
10-264	.472	.146	.448	.150	.224	.298
11-265	.118	.246	.213	.293	.085	.199
12-266	.354	.314	.224	.242	.708	.149
13-267	.236	.220	.191	.150	.956	.1
14-268 B-58	.236	.112	.220	.092	.62	.8
15-269 B-58	.531	.213	.459	.159	.775	.358
16-270 B-58	.236	.237	.112	.231	.488	.130
17-271 B-58	.180	.448	.852	.385	.885	.891
18-272 B-58	.165	.168	.224	.123	.791	.100
19-273	.499	.269	.560	.150	.806	.497

ACCELERATION "g"

RUN	1 N Wall COR N-S	2 E Wall COR E-W	3 E Wall COR N-S	4 S Wall COR E-W	5 Inter Walls N-S	6 Roof V
1-255	.012	0	.019	.036	.127	.058
2-256	.012	0	.029	.036	.088	.058
3-257	.013	0	.026	.042	.120	.074
4-258	.016	0	.034	.050	.101	.072
5-259	.013	0	.026	.050	.078	.058
6-260	.019	0	.029	.042	.073	.065
7-261	.023	0	.036	.029	.137	.061
8-262	.021	0	.025	.038	.150	.045
9-263	.012	0	.024	.019	.058	.049
10-264	.019	0	.017	.031	.125	.033
11-265	.016	0	.026	.015	.118	.065
12-266	.019	0	.024	.019	.152	.061
13-267 B-58	.012	0	.024	.017	.103	.045
14-268 B-58	.010	0	.044	.019	.068	.016
15-269 B-58	.013	0	.022	.038	.082	.033
16-270 B-58	.019	0	.026	.011	.152	.058
17-271 B-58	.029	0	.038	.021	.152	.077
18-272 B-58	.019	0	.019	.023	.097	.041
19-273	.012	0	.024	.008	.103	.061

STRUCTURAL RESPONSE PROGRAM

COMPILED BY _____

DATE: HS-65: 1-20-65
HOUSE W-6

PHASE 2-R — 1-23-65

PRESSURE psf

RUN	Ref	Wind Vel	Dir	Free Field NW	1 N Wall N	2 E Wall E	3 E Wall S	4 W Wall W	5 W Roof	6 E Roof	7 Bed Room	8 Bath Room
20-274 B-58	25	130	A	2.1	3.0	2.6	2.1	2.1	2.1	2.5	1.4	1.5
21-275 B-58	25	135	F	1.8	2.6	2.6	2.7	1.9	1.2	2.3	1.1	0.8
22-276 B-58	25	136	G	1.6	3.0	2.0	1.8	2.1	1.9	1.7	0.8	1.2
23-277 B-58	25	136	F	1.3	1.7	1.9	1.7	1.6	1.7	NR	0.8	0.6
24-278 B-58	24.6	135	A	2.1	2.7	2.0	1.8	1.9	1.6	1.9	0.8	1.3
25-279	12	126	H	4.2	4.9	4.5	4.3	6.0	6.6	6.6	1.5	1.5
26-280	12.	131	D	2.2	2.7	1.9	2.7	3.9	2.5	2.5	1.2	0.9
27-281	12	128	H	4.1	4.6	6.8	4.4	4.1	3.8	3.9	1.5	0.9
28-282 B-58	12	128	D	2.2	3.7	3.2	6.4	6.6	4.3	4.4	1.8	1.5
29-283 B-58	25	136	F	2.9	3.8	3.6	4.1	3.5	3.3	3.1	1.5	1.2
30-284 B-58	25	136	A	2.1	2.3	1.7	1.7	1.9	1.6	1.9	0.9	1.2
31-285 B-58	12	129	A	2.3	3.2	5.1	2.3	3.1	2.6	3.9	1.5	1.5
32-286 B-58	25	136	F	2.6	2.4	2.6	2.1	2.3	2.4	1.9	1.2	1.2
33-287 B-58	12.05	129	E	6.6	3.3	4.3	8.7	5.0	6.5	7.5	1.3	1.5
34-288 B-58	25	137	H	2.1	2.3	1.9	1.7	1.9	1.6	1.7	1.2	1.5
35-289 B-58	12.	129	B	4.2	4.6	5.4	2.6	3.9	3.3	3.0	1.5	1.5
36-290 B-58	25	137	F	0.9	0.9	1.2	1.2	1.7	1.4	1.2	0.6	1.2
37-291 B-58	25	137	A	4.6	7.5	3.6	2.6	3.7	5.2	5.0	1.5	1.5
38-292 B-58	25	136	F	3.1	3.1	3.9	4.3	3.5	3.2	3.0	1.5	1.2

DISPLACEMENT ($\times 10^{-2}$ in)

RUN	1 N Wall COR N-S	2 E Wall COR E-W	3 E Wall COR N-S	4 S Wall COR E-W	5 Inter Walls N-S	6 Inter Walls E-W
20-274 B-58	.106	.112	.112	.139	.709	.115
21-275 B-58	.118	.224	.078	.462	.140	.093
22-276 B-58	.212	.123	.112	.150	.085	.087
23-277 B-58	.189	.112	.224	.077	.372	.149
24-278 B-58	.142	.134	.112	.150	.059	.130
25-279	.323	.448	.852	.358	.078	.779
26-280	.1008	.336	.571	.277	.760	.596
27-281	.1197	.459	.1008	.308	.885	.779
28-282 B-58	.1261	.560	.896	.1112	.785	.1033
29-283 B-58	.236	.112	.224	.077	.620	.149
30-284 B-58	.118	.112	.056	.092	.791	.529
31-285 B-58	.826	.728	.635	.185	.1101	.762
32-286 B-58	.118	.101	.146	.051	.513	.552
33-287 B-58	.768	.595	.445	.305	.795	.497
34-288 B-58	.118	.056	.112	.077	.527	.074
35-289 B-58	.142	.235	.195	.116	.1117	.516
36-290 B-58	.111	.101	.112	.231	.516	.612
37-291 B-58	.236	.224	.112	.154	.1004	.149
38-292 B-58	.201	.224	.146	.169	.115	.151

STRUCTURAL RESPONSE PROGRAM

COMPILED

BY ______

DATE 1-15-65: 1-24-65

HOUSE W-6

PHASE 2-B 1-23-65 RUN	Alt	Hgt	Vic	Free Field	Pressure psf 1 N Wall N	2 E Wall E	3 S Wall S	4 W Wall W	5 W Roof	6 E Roof	7 Big Room	8 Small Room	Displacement (×10⁻² in) 1 W Wall N Cor E-W	2 N Wall E Cor N-S	3 E Wall S Cor E-W	4 S Wall W Cor N-S	5 Inter Wall N-S	6 N Wall Center E-W	Acceleration "g" 1 N Wall W Cor N-S	2 E Wall N Cor E-W	3 S Wall E Cor N-S	4 W Wall S Cor E-W	5 Inter Wall N-S	6 Roof V
39-293	12	129	C	6.3	4.6	3.6	3.3	7.4	7.1	7.8	1.8	1.5	1012	539	1120	667	131	998	.029	0	.046	.097	.130	.121
40-294	25	132	A	0.9	4.3	3.2	3.7	3.1	3.3	3.4	1.5	1.5	.123	124	112	154	1.550	159	.016	0	.017	.011	.147	.045
41-295	12	130	G	2.7	0.8	1.2	1.1	0.6	0.6	0.5	0.3	0.6	354	112	246	139	.165	208	.012	0	.014	.023	.041	.027
42-296	25	137	F	2.3	2.6	2.7	2.4	2.1	2.4	2.7	1.5	1.5	142	112	232	.046	570	130	.010	0	.014	.019	.054	.022
43-297	12	125	C	2.2	4.9	2.7	2.7	4.3	3.0	3.3	1.5	1.2	1244	408	896	.308	1240	890	.026	0	.038	.011	.103	.069
44-298	12	126	G	7.3	5.8	9.7	9.4	6.8	7.3	7.0	2.4	1.8	1.553	728	1120	400	1.550	968	.034	.006	.055	.092	.193	.104
45-299	12	126	H	[illegible]	3.8	6.8	4.1	3.9	3.0	3.1	1.8	1.5	1972	.560	1368	.339	1131	1158	.029	0	.043	.090	.101	.050
46-300	121	125	D	2.8	2.4	2.7	4.1	3.9	4.7	5.0	0.9	0.6	1062	357	683	293	609	670	.021	0	.031	.061	.054	.022
47-301	12	126	H	1	2.0	4.6	7.2	3.7	3.2	3.1	1.2	1.2	1169	359	806	217	775	670	.021	0	.029	.061	.069	.041
48-302	12	129	E	4.2	2.4	2.6	4.7	4.1	2.2	3.1	1.2	1.5	718	.547	370	277	930	521	.023	0	.041	.034	.093	.085
49-303	12	130	B	4.2	6.2	6.1	7.7	4.1	4.4	4.4	1.5	1.5	593	235	570	169	961	947	.023	0	.024	.048	.101	.068
50-304	12	130	E	11.7	3.3	3.4	8.7	8.7	7.7	7.5	1.8	1.5	838	560	538	356	1246	581	.031	0	.053	.042	.152	.085
End																								

STRUCTURAL RESPONSE PROGRAM

COMPILED

BY ______

DATE 1-15-65: 1-24-65

HOUSE W-6

PHASE 2-B 1-21-65 RUN	Act	Hgt	Vic	Free Field	Pressure (psf) 1 N Wall N	2 E Wall E	3 S Wall S	4 W Wall W	5 W Roof	6 E Roof	7 Big Room	8 Small Room	Displacement (×10⁻² in) 1 W Wall N Cor E-W	2 N Wall E Cor N-S	3 E Wall S Cor E-W	4 S Wall W Cor N-S	5 Inter Wall N-S	6 N Wall Center E-W	Acceleration (g) 1 N Wall W Cor N-S	2 E Wall N Cor E-W	3 S Wall E Cor N-S	4 W Wall S Cor E-W	5 Inter Wall N-S	6 Roof V
1-305	12	122	F	44	(No Record)								(No Record)						.012	0	.017	.019	.051	.052
2-306	12	123	A	46															.012	0	.017	.011	.092	.032
3-307	12	120	F	42															.012	0	.019	.017	.115	.046
4-308	11.95	125	A	3.8															.014	0	.017	.013	.102	.032
5-309	12.2	122	G	4.9															.012	0	.019	.040	.068	.041
6-310	12	122	C	44															.019	0	.024	.052	.113	.050
7-311	12	120	G	4.5															.014	0	.019	.046	.052	.050
8-312	12	120	C	44															.021	0	.022	.043	.126	.043
9-313	12	125	H	48															.019	0	.024	.058	.068	.055
10-314	12	125	D	50															.023	0	.021	.061	.062	.076
11-315	12	125	H	42															.014	0	.026	.059	.068	.050
12-316	12	125	D	45															.023	0	.031	.047	.056	.059
13-317	12	120	A	44															(No Record)					
14-318	12	120	F	4.5															.017	0	.024	.025	.138	.048
15-319	12	126	H	3.6															.017	0	.019	.015	.102	.093
16-320	12	121	B	61															.017	0	.019	.049	.219	.057
17-321	121	120	E	5.1															.017	0	.029	.035	.106	.055
18-322	1195	120	B	4.1															.014	0	.014	.038	.157	.043
19-323	12	122	E	34															.023	0	.031	.021	.138	.063

Structural Response Program

Compiled By ______

Date 1-5-65; 1-24-65
House W-6

Phase 2-B 1-24-65 Run	Alt	Nom	Vec	[illegible] psi	Pressure (psi) 1 N Wall N	2 E Wall E	3 S Wall S	4 W Wall W	5 W Roof	6 E Roof	7 Bld Roof	8	Displacement (in.) 1 N Wall N COR E-W	2 E Wall E COR N-S	3 S Wall S COR E-W	4 W Wall W COR N-S	5 Inter Wall N-S	6 N Wall Center E-W	Acceleration (g) 1 N Wall W COR N-S	2 E Wall N COR E-W	3 S Wall E COR N-S	4 W Wall S COR E-W	5 Inter Wall N-S	6 Roof V
20-324	12	123	C	6.1															.017	.002	.026	.052	.214	.063
21-325	12.	123	G	5.4															.021	0	.029	.025	.115	.043
22-326	12	120	C	NR															.012	0	.019	.038	.155	.043
23-327	12.	120	G	4.3															.023	0	.028	.025	.121	.063
24-328	12	1.0	H	2.4															.019	.004	.026	.077	.132	.050
25-329	12	121	D	4.6															.021	0	.029	.050	.177	.046
26-330	12	121	H	NR															.016	0	.022	.065	.092	.041
27-331	12	120	D	6.5															.021	0	.024	.048	.017	.059
28-332	12	121	E	4.6															.025	0	.031	.031	.123	.059
29-333	12	120	B	.0															.046	0	.017	.038	.155	.043
30-334	12	123	E	3.1															.023	0	.024	.035	.102	.046
31-335	12	125	B	4.1															.012	0	.014	.036	.128	.036
32-336	119	12	F	4.2															.014	0	.017	.029	.123	.043
33-337	12	12	A	NR															.016	0	.012	.036	.085	.025
34-338	12	121	F	NR															.014	0	.019	.027	.115	.050
35-339	12	121	A	2.4															.011	0	.017	.036	.192	.043
36-340	12.	121	G	3.0															.018	0	.022	.048	.059	.043
37-341	12	120	C	4.9															.019	0	.026	.044	.147	.041
38-342	12	122	G	4.4															.016	.002	.022	.052	.094	.052
39-343 End	12	122	C	3.9															.019	0	.017	.027	.113	.043

Structural Response Program

Compiled By ______

Date 11-20-64 12-6-64
House 2-S-S

Phase 2-A				Displacement (10^{-3} in)							
12-4-64				Fire Field	1	2	3		1	2	3
Run	[illegible]	[illegible]	[illegible]	V	[illegible]	[illegible]	[illegible]		[illegible]	[illegible]	[illegible]
1-289	17.0	1.45	11	NK	(NK)				(NK)		
2-289	17.2	1.4	V		.21	.25	.66		.04	.12	.17
3-290	17.1	1.4	H		(NK)				(NK)		
4-291	17.0	1.3	A			↓				↓	
5-292	17.5	1.42	F								
6-293	18.0	1.25	G								
7-294	[illegible]	1.35	1.3		.09	.46	.26		.02	.07	.06
					.14	.37	.56		.02	.13	.14
9-29[illegible]					(NK)				(NR)		
[illegible]					.02	.44	.41		.02	.12	.21
11-			4		(NK)				(NR)		
12-29[illegible]		[illegible]			(NK)						
13-300	21.0	1.4	V		.04	.60	.65				
14-301	21.0	1.4	H		.09	.68	.45				
15-302	23.0	1.5	V		(NK)						
16-303	23.0	1.45	[illegible]		(NR)						
17-304	24.2	1.45	.3		.07	.53	.41			↓	
End											

Structural Response Program

Compiled By ______

Date 11-20-64 12-6-64
House 2-S-S

Phase 2-A				Displacement (10^{-3} in)							
12-5-64				Fire Field	1	2	3		1	2	3
Run	[illegible]	[illegible]	[illegible]	V	[illegible]	[illegible]	[illegible]		[illegible]	[illegible]	[illegible]
1-305	12.0	1.2	F	NK	(NR)				(NR)		
2-306	11.75	1.2	A	NK		↓				↓	
3-307	12.0	1.2	F	6.2							
4-308	12.0	1.25	G	4.8	.26	1.25	1.05		.10	.21	.45
5-309	12.0	1.25	C	NK	.21	1.11	.72		.10	.22	.29
6-310	12.3	1.21	G	5.6	(NK)				(NR)		
7-311	12.0	1.2	1.1	5.5	.22	1.40	1.01		.08	.42	.25
8-312	12.0	1.2	V	5.3	.13	1.45	.60		.14	.28	.39
9-313	12.0	1.2	A	2.0	(NK)				(NK)		
10-314	12.0	1.21	A	NK	.40	1.9	.83		.10	.21	.23
11-315	12.2	1.2	F	5.9	.16	.65	.66		(NR)		
12-316	12.0	1.2	A	4.8	(NK)					↓	
13-317	12.0	1.24	[illegible]	7.6	.24	.89	.79				
14-318	12.2	1.26	[illegible]	5.5	(NK)						
[illegible]-319	12.0	1.22	[illegible]	7.0	(NK)						
16-320	12.0	1.21	C	7.3	.09	.65	.64		.12	.15	.35
17-321	12.0	1.2	G	4.2	.34	1.02	.81		.12	.24	.29
18-322	12.25	1.2	C	6.5	(NK)				(NK)		
19-323	12.0	1.2	V	7.0	.13	1.45	.47		.13	.14	.1

Structural Response Program

Compiled By _____

Date 11-20-64 12-16-64
House 2-5-5

Phase 2-A					Displacement (10^{-2} in)							
12-5-64					Final Field	1 OD 1-25 in-s	2 OD 2-50	3 OD 4-25 V		1 Lo 1-25 in-s	2 Lo 2-50	3 Lo 4-25 V
Run	Wt	Vo	Loc									
20-324	12.9	12.1	H	SW	5.6	.24	.40	.81		.12	.41	.27
21-325	12.0	12	D		6.2	(NR)				(NR)		
22-326	12.2	12	E		5.9	.24	.84	.70		.10	.21	.31
23-327	12.0	12	B		5.3	.18	.80	.86		.19	.27	.41
24-328	12.0	12	E		5.9	(NR)				(NR)		
25-329	12.0	12.1	F		5.6							
26-330	11.79	12	A		5.3							
27-331	11.9	12.1	E		6.2							
28-332	12.0	1.18	G		5.1	.42	.32	.96		.17	.31	.39
29-333	12.0	12	C		4.9	.11	.84	.62		.19	.26	.41
30-334	12.0	12.1	G		5.6	(NR)				(NR)		
End												

Structural Response Program

Compiled By _____

Date 11-20-64 12-16-64
House 2-5-5

Phase 2-A					Displacement (10^{-2} in)							
12-6-64					Final Field	1 OD 1-25 in-s	2 OD 2-50	3 OD 4-25 V		1 Lo 1-25 in-s	2 Lo 2-50	3 Lo 4-25 V
Run	Wt	Vo	Loc									
1-335	12.3	12	H	NR	20	.59	.52		.06	.34	.39	
2-336	12.0	12	D	NR	(NR)				.17	.13	.41	
3-337	12.0	12	H	4.9	(NR)				(NR)			
4-338	12.0	12	A	5.2	.23	.22	.93		.06	.08	.33	
5-339	12.0	12.1	F	4.9	(NR)				(NR)			
6-340	11.7	12	A	6.0	(NR)				(NR)			
7-341	12.1	12.2	B	NR	.13	.82	.67		.06	.20	.27	
8-342	11.9	12.1	C	6.3	.22	.82	.66		.11	.21	.31	
9-343	12.0	12	B	4.4	(NR)				(NR)			
10-344	12.0	12	C	6.0	.11	.27	.72		.08	.12	.33	
11-345	12.0	12.2	G	4.4	.25	.09	.27		.08	.21	.21	
12-346	12.2	12	C	4.4	(NR)				(NR)			
13-347	11.9	12.1	D	5.5	.09	.50	.67		.12	.27	.31	
14-348	12.0	12.1	H	4.6	.22	.45	.44		.12	.43	.23	
15-349	12.2	12	D	4.4	(NR)				(NR)			
16-350	12.0	12.1	E	6.0	.29	.70	.79		.13	.11	.33	
17-351	12.0	12.5	B	6.5	.13	.65	.86		.11	.17	.33	
18-352	12.0	12.2	E	5.7	(NR)				(NR)			
19-353	12.0	12	F	5.2	.36	.20	1.00		.08	.27	.31	

Structural Response Program

Compiled By ____

Date [illegible]
House 2-5-5

Phase 2-A 12-6-64 Run	[illegible]	[illegible]	[illegible]	Free Field [illegible]	Displacement (10^{-2} in) 1	2	3	-	1	2	3
20-354	11.0	12	A	4.9	.16	.25	.86		.21	.25	.65
21-355	12.0	1.2	E	5.7	(NR)				(NR)		
22-356	12.0	1.2	G	4.9							
23-357	11.9	1.23	C	8.2							
24-358	11.8	12	G	NR							
25-359	12.0	1.21	H	5.7	.22	1.45	.82		.11	.40	.29
26-360	11.8	1.21	D	6.5	.13	1.57	.65		.13	.38	.31
27-361	11.2	1.24	H	4.4	(NR)				(NR)		
28-362	12.1	1.2	A	NR	.32	.24	.85		.13	.11	.29
29-363	12.0	1.2	E	4.6	.11	.46	.21		.25	.17	.46
30-364	12.0	1.2	A	8.7	(NR)				(NR)		
End											

Structural Response Program

Compiled By ____

Date [illegible]
House 2-5-5

Phase 2-A 12-7-64 Run	[illegible]	[illegible]	[illegible]	Free Field [illegible]	Displacement (10^{-2} in) 1	2	3	-	1	2	3
1-365	9.0	12	A	NR	.20	.38	1.10		.19	.18	.69
2-366	9.0	12	E	7.6	.39	1.45	.23		.12	.52	.62
3-367	8.9	12	A	8.1	(NR)				(NR)		
4-368	9.0	12	C	NR	.29	1.45	.64		.12	.43	.64
5-369	9.0	1.2	E	NR	(NR)				(NR)		
6-370	9.0	12	C	9.8							
7-371	9.0	1.15	D	4.6					.14	.26	.41
8-372	9.2	1.22	A	8.1					.12	.23	.62
9-373	9.3	12	C	9.2					(NR)		
10-374	9.0	1.24	E	6.2					.12	.14	.50
11-375	8.8	1.22	A	4.9					.3	.14	.48
12-376	9.0	1.2	E	7.1					(NR)		
13-377	9.0	1.21	F	10.6	.63	.43	1.56				
14-378	9.0	1.21	A	5.7	.20	.43	1.05				
15-379	9.1	1.2	F	17.5	(NR)						
16-380	9.0	1.23	A	5.4	.20	.40	.98				
17-381	9.0	12	F	8.9	.67	.44	1.43				
18-382	9.0	1.24	A	10.0	(NR)						
19-383	9.0	1.2	E	15.9	.36	1.45	.65		.10	.24	.25

Structural Response Printout

Coupled By _____

Date: 12-14-64
House 2-S-S

Phase 2-A

12-7-64

Pin				Free Field	1 (0.03 sec)	2 (0.05 sec)	3 (0.07 sec)		1 (0.03 sec)	2 (0.05 sec)	3 (0.07 sec)
				.W	in.	in.	in.		in.	in.	in.
20-384	90	12	W	4.38	.33	4.28	5.5		.12	.53	.25
21-385	91	12	E	6.28	(NR)				(NR)		
End											

Structural Response Printout

Coupled By _____

Date: 12-14-64
House 2-S-S

Phase 2-A

12-8-64

Pin				Free Field	1 (0.03 sec)	2 (0.05 sec)	3 (0.07 sec)		1 (0.03 sec)	2 (0.05 sec)	3 (0.07 sec)
				.W	in.	in.	in.		in.	in.	in.
1-390	75	12.3	A	11.0	.36	.32	1.51		.15	.66	1.31
2-391	75	11.7	F	11.2	.81	.60	1.62		.24	.15	.38
3-392	72	12.1	A	9.1	(NR)				(NR)		
4 393	75	12.1	C	9.1	.23	1.52	1.28		.16	.40	.25
5-394	76	12.4	E	9.1	.81	1.43	1.68		.24	.15	.36
6-395	70	12	C	10.2	(NR)				(NR)		
7-396	75	12	W	4.7	.22	NR	85		.18	.66	.56
8-397	75	12	A	14.7	.45	.45	2.10		.31	.36	1.23
9-398	75	12	W	11.2	(NR)				(NR)		
10-399	75	12	E	10.2	.54	1.93	1.17		.19	.45	.32
11-400	79.5	12	A	12.1	1.46	.34	2.19		.21	.31	.87
12-401	75	12	E	9.9	(NR)				(NR)		
13-402	75	12.1	F	11.8	.76	.45	1.86		.19	.13	.39
14-403	75	12	A	11.6	.39	.32	2.16		.21	.30	.91
15-404	75	12.2	F	11.2	(NR)				(NR)		
16-405	75	12	C	8.8	.27	1.92	1.30		.08	.31	.59
17-406	75	12	A	14.3	.45	.47	2.19		.21	.29	1.17
18-407	75	12	F	10.7	.74	.42	1.71		.25	.18	.41
19-408	75	12	A	11.1	(NR)				(NR)		

Structural Response Program

Compiled By ______

Date 11-2-64 - 12-10-64
House 2-S-S

Phase 2-A 12-8-64				Displacement (10⁻³ in)							
Run	[illegible]	[illegible]	[illegible]	Free Field	1	2	3	–	1	2	3
20-409	75	121	E	13.1	.61	NR	1.38		.20	.47	.60
21-410	75	1.2	D	11.8	.39	NR	.96		.21	.68	.64
22-411	75	121	E	7.6	(NK)				(NK)		
End											

Structural Response Program

Compiled By ______

Date 11-2-64 - 12-10-64
House 2-S-S

Phase 2-A 12-9-64				Displacement (10⁻³ in)							
Run	[illegible]	[illegible]	[illegible]	Free Field	1	2	3	–	1	2	3
1-416	70	1.2	A	14.0	.41	.46	2.13		.27	.95	1.66
2-417	70	1.2	F	10.3	.77	.35	3.44		.23	.13	.58
3-418	7.0	1.2	A	11.7	(NR)				(NR)		
4-419	6.9	1.2	C	14.2	.40	.48	1.97		.42	.76	1.45
5-420	7.0	1.2	F	10.3	.26	.29	2.70		.21	.13	.48
6-421	7.0	1.2	D	13.7	.27	2.26	.29		.20	.81	.97
7-422	7.0	1.2	A	12.0	.63	.59	2.68		.33	.30	1.31
8-423	7.0	1.2	D	11.2	(NR)				(NK)		
9-424	7.0	1.25	E	14.9	.41	1.80	1.60		.21	.38	.76
10-425	6.9	1.22	A	16.7	.34	.42	2.44		.51	.53	1.50
11-426	7.0	1.2	E	9.5	(NR)				(NK)		
12-427	7.0	1.15	F	15.6	.77	.39	1.82		.21	.12	.63
13-428	7.1	1.2	A	18.1	.57	.49	2.66		.78	.93	1.85
14-429	7.2	1.2	F	10.6	(NK)				(NR)		
15-430	7.0	1.2	C	15.6	.50	1.49	2.51		.87	.61	1.65
16-431	7.0	1.2	D	12.9	.34	NK	1.80		.19	.85	.98
17-432	7.0	1.19	C	6.5	(NK)				(NK)		
18-433	7.0	1.2	A	12.3	.53	.58	2.98		.57	.55	1.35
19-434	7.0	1.21	F	11.2	.86	NK	1.97		.23	.60	.73

STRUCTURAL RESPONSE PROGRAM

Compiled By ______

Date 12-9-64 12-16-64
House 2-S-5

Phase 2-A 12-9-64 Run	[illegible]	[illegible]	[illegible]	Free Field	Displacement (10^{-2} in) 1	2	3	–	1	2	3
20-435	70	12	A	11.2	(NR)				(NR)		
21-436	70	12	E	15.3	34	NR	147		17	96	97
22-437	70	117	D	117	(NR)				(NR)		
23-438	70	118	E	167	(NR)				(NR)		
End											

STRUCTURAL RESPONSE PROGRAM

Compiled By ______

Date 12-12-64 12-15-64
House 2-S-5

Phase 2-A 12-12-64 Run	[illegible]	[illegible]	[illegible]	Free Field	Displacement 1	2	3
1-496	17.0	13	E	3.5	.11	.46	.51
2-497		13	G	3.1	.07	.63	.49
3-498		1.38	E	NR	(NR)		
4-499		1.3	F	3.1	.23	.21	.83
5-500		1.38	A	3.3	.01	.30	.53
6-501		1.3	F	3.9	(NR)		
7-502		1.29	Y	3.1	.13	.92	.71
8-503		1.29	D	3.9	.11	1.18	.58
9-504	6.9	1.3	H	4.3	(NR)		
10-505	17.0	1.26	A	2.3	.04	1.2	.43
11-506		1.26	F	2.1	.16	.13	.55
12-507		1.26	A	4.7	(NR)		
13-508		1.28	B	3.7	.06	.68	.52
14-509		13	E	3.1	.15	.48	.64
15-510		1.3	B	2.3	(NR)		
16-511		13	C	NR	.13	.65	.40
17-512		1.3	F	1.8	.04	.21	.32
18-513		13	C	1.4	(NR)		
19-514		1.28	D	3.9	.16	.97	.32

Structural Response Program

Coupled
By _____

Diffraction 12-15-69
House 2-5-5

House 2-A
12-13-64

Pin	Hr.	Min.	Sec.	Freq.	Comp. 1	Comp. 2	Comp. 3
20-515	17	13	21	4.7	.18	108	.81
21-516			51	3.7	(NR)		
22-517			52	3.9	.13	46	.45
23-518			53	2.9	.11	68	.56
24-519			54	7.7	(NR)		
25-520			55	4.5	.22	31	.67
26-521			56	1.6	.07	12	.26
27-522		13	1	NR	(NR)		
28-523		13	2	2.3	.18	17	.66
29-524		13	3	1.6	.11	23	.70
30-525		13	4	2.5	(NR)		
End							

Structural Response Program

Coupled
By _____

Diffraction 12-15-69
House 2-5-5

House 2-A
12-13-64

Pin	Hr.	Min.	Sec.	Freq.	Comp. 1	Comp. 2	Comp. 3
1-526	20	14	5	2.9	.13	.43	.60
2-527		14	12	2.1	.07	.51	.83
3-528		14	13	2.3	(NR)		
4-529		14	15	2.9	.16	.23	.69
5-530		14	16	2.5	.07	.13	.41
6-531		14	17	2.3	(NR)		
7-532		14	18	2.9	.13	.94	.60
8-533			19	2.01	.07	1.63	.34
9-534			20	2.1	(NR)		
10-535			21	2.0	.07	1.9	.48
11-536			22	3.7	.22	.19	.21
12-537			23	2.1	(NR)		
13-538			24	1.8	.05	33	.44
14-539			25	3.7	.13	70	.62
15-540			26	2.1	(NR)		
16-541			27	3.1	.07	36	.44
17-542			28	3.3	.16	36	.73
18-543			29	2.1	(NR)		
19-544			30	3.1	.09	70	.41

Structural Response Program

Compiled By ______

Date 12-15-64
House 2-5-5

Phase 2-A 12-13-64 Run				Displacement Free Field	1	2	3
20-545	20.0	1.4	H	2.9	.16	.82	.49
21-546		1.4	▽	2.3	(NR)		
22-547		1.39	E	2.3			
23-548		1.4	B	2.3			
24-549		1.41	E	2.1			
25-550		1.4	F	2.9	.18	.25	.81
26-551			△	2.9	.07	.5	.02
27-552			E	6.0	(NR)		
28-553			H	3.3	.11	.82	.48
29-554			▽	2.3	(NR)		
30-555			H	6.4	(NR)		
End							

Structural Response Program

Compiled By ______

Date 12-15-64
House 2-5-5

Phase 2-A 12-14-64 Run				Displacement Free Field	1	2	3
1-556	12.0	1.29	A		.13	.22	1.02
2-557	12.0	1.28	F		.29	.42	1.08
3-558	11.9	1.28	A		(NR)		
4-559	12.0	1.25	B		.18	.87	1.11
5-560		1.27	E		.27	.92	.28
6-561		1.28	B		(NR)		
7-562		1.3	C		.18	.84	.88
8-563		1.3	E	4.4	.38	.32	.80
9-564		1.3	C	4.5	(NR)		
10-565		1.25	▽	5.1	.18	1.45	.34
11-566	11.8	1.25	H	4.3	.23	1.45	1.16
12-567	11.3	1.25	▽	4.4	(NR)		
13-568	12.1	1.3	E	3.7	.25	.70	.74
14-569	12.0	1.3	B	4.8	.16	.82	1.30
15-570		1.3	E	5.0	(NR)		
16-571		1.24	F	5.6	.40	.38	1.31
17-572		1.24	A	4.4	.14	.19	.83
18-573		1.25	F	5.0	(NR)		
19-574		1.3	H	4.3	.18	1.18	.86

Structural Response Program

Compiled By ______

Date 12-15-64
House 2-5-5

Phase 1-A 12-14-64				Displacement Free Field	1	2	3
Run							
20-575	12.5	128	D	44	.13	1.04	1.38
21-576	↓	13	H	48	(NR)		
22-577		13	A	46	.15	.22	.51
23-578		13	E	4.8	.38	.38	1.10
24-579	↓	13	A	43	(NR)		
25-580	11.5	122	C	4.3	.14	.89	1.12
26-581	12.0	125	E	4.3	.23	.22	.59
27-582	↓	13	E	5.2	(NR)		
28-583		124	C	3.9	.13	.87	.37
29-584		125	E	4.5	.36	.34	1.10
30-585	↓	126	C	3.9	(NR)		
31-586	11.8	126	D	44	.28	1.25	.38
32-587	11.8	126	H	4.8	.23	1.45	1.24
33-588	12.0	126	D	4.3	(NR)		
34-589		126	E	4.3	.22	.80	.66
35-590		127	C	4.4	.14	.84	1.16
36-591		13	E	4.4	(NR)		
End	↓						

Structural Response Program

Compiled By ______

Date 12-15-64
House 2-5-5

Phase 2-A 12-15-64				Displacement Free Field	1	2	3
Run							
1-592	12.0	115	E		.32	.30	.84
2-593	12.0	117	A		.16	.36	1.14
3-594	11.5	1.5	E		(NR)		
4-595	10.5	13	D		.34	1.57	1.75
5-596	↓	13	H		.29	1.33	1.08
6-597		13	D		(NR)		
7-598		121	D		.11	.92	1.18
8-599		123	E		.29	1.09	.95
9-600	↓	126	A		(NR)		
10-601	12.0	122	C		↓		
11-602	10.5	120	E				
12-603	12.5	120	C				
13-604	10.5	1.23	C	5.2	.50	.48	1.3[illegible]
14-605	10.4	120	E	5.7	.22	1.21	2.01
15-606	10.5	121	-	6.0	(NR)		
16-607	10.5	15	[illegible]	10	.4	1.72	1.17
17-608	10.4	[illegible]	[illegible]	[illegible]	(NR)		
18-609	12.5	1.26	[illegible]	6	(N		
19-610	12.5	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]

Structural Response Program

Coupled
By _____

Date Run 12-15-64
House 2-5-5

Phase 2-A — Displacement

12-15-64

Pin				Free Field	1	2	3			
20-611	10.5	125	S	5.8	.20	.43	.44			
21-612		125	E	5.9	(N.R.)					
22-613		12	F	4.4	.44	.38	.27			
23-614		12	A	7.0	.20	.40	.35			
24-615		121	E	3.0	(N.R.)					
End										

Structural Response Program

Coupled
By _____

Date Run 12-15-64
House 2-5-5

Phase 2-B — Displacement

12-15-64

Pin				Free Field	1	2	3			
1-1	12	12	A		.30	.24	.68		.20	.20	.15
2-2	12	123	F		.63	.20	.62		.16	.12	.39
3-3	12.1	126	A		.26	.48	.56		.17	.20	.29
4-4	120	125	B		.26	.64	.70		.14	.23	.29
5-5	115	123	E		.28	.36	.64		.22	.15	.14
6-6	12	126	B		.26	.80	.64		.15	.26	.26
7-7	12	126	C		.26	.56	.56		.12	.16	.23
8-8	12	127	C		(No Record)				(No Record)		
9-9	12	128	C		.48	.60	.56		.12	.15	.43
10-10	12	111	D		(N.R.)				(N.R.)		
11-11	12	123	H		.46	.90	.58		.12	.20	.31
12-12	12	120	D		.28	.60	.44		.14	.20	.02
	117	121	E	5.7	.30	.64	.24		.09	.20	.20
13-13	114	124	S	6.6	.18	.64	.50		.12	.17	.26
		126	E	4.5	.40	.32	.62		.15	.11	.80
		126	F	4.1	.47	.36	.64		.12	.12	.57
		125	A	5.6	.26	.50	.70		.25	.23	.40
		127	F	3.7	.20	.16	.50		.14	.12	.31
		124	V	4.0	.62	.64	.64		.09	.14	.15

STRUCTURAL RESPONSE PROGRAM

COMPILED BY ______

DATE 1-15-65
HOUSE 2-5-5

PHASE 2-B 1-15-65				DISPLACEMENT (10^{-3} in.)							
RUN				FREE FIELD	1	2	3		1	2	3
20-20	12	1.35	C	6.3	.30	.44	.90		.12	.14	.32
21-21	12.	1.24	G	6.1	.60	.80	.94		.11	.20	.15
22-22	11.84	1.26	H	4.3	.58	1.14	.70		.11	.29	.17
23-23	11.9	1.26	D	5.4	.24	.54	1.46		.11	.26	.85
24-24	12.	1.28	H	9.3	1.10	1.44	1.16		.22	.40	.62
25-25	12.	1.35	A	5	.40	.60	.78		.19	.19	.42
26-26	12.5	1.35	F	5.0	.50	.38	.96		.14	.12	.57
27-27	11.8	1.34	A	8.1	.30	.44	.86		.15	.15	.29
28-28	12.	1.23	B	5.5	.24	.54	.34		.14	.15	.31
29-29	12.	1.2	E	4.3	.30	.58	.24		.06	.14	.14
30-30	12.	1.33	B	—	.30	.62	.50		.23	.23	.42
End.											

STRUCTURAL RESPONSE PROGRAM

COMPILED BY ______

DATE 1-16-65
HOUSE 2-5-5

PHASE 2-B 1-16-65				DISPLACEMENT (10^{-3} in.)									
RUN				FREE FIELD	1	2	3		1	2	3		
1-31	11.5	1.21	C	—	—	—	—		(NO RECORD)				
2-32	11.8	1.23	G	6.1	.56	.64	.64		↓				
3-33	11.9	1.26	C	6.0	.30	.54	.46						
4-34	12.	1.25	D	6.0	.20	.28	.22						
5-35	12.	1.25	H	6.0	.42	.90	.56		.14	.15	.23		
6-36	12.	1.26	D	6.5	.18	.74	.38		.15	.19	.26		
7-37	11.7	1.20	G	6.5	.38	.64	.34		(N.R.)				
8-38	12.	1.21	B	5.6	.20	.60	.60		.12	.23	.48		
9-39	12.	1.21	G	6.2	.38	.58	.58		.08	.19	.23		
10-40	11.7	1.24	F	6.8	(NO RECORD)				.15	.11	.39		
11-41	11.6	1.26	A	4.0	↓				.19	.26	.57		
12-42	12.	1.26	=	5.4					.11	.08	.14		
13-43	7.	1.30	G	7.6					(NO RECORD)				
14-44	[illegible]	1.27	C	7.3					↓				
15-45	25	1.35	F	4.9					.06	.06	.20	13	1.8
[illegible]	25	1.30	F	5.1								[illegible]	1.8
[illegible]	25.	1.35	F	4.5								13	1.8
[illegible]	25.	1.30	=	4.0								13	1.8
[illegible]	25.	[illegible]	=	2.1	↓								.8

STRUCTURAL RESPONSE PROBE

COMPILED BY ———

DATE(S): 1-17-65

HOUSE 2-S-2

PHASE 7-B

1-16-65

DISPLACEMENT (10⁻³) in

PIN	X	Y	G	FREQ (CPS)	1	2	3	1	2	3
20-58	12.	1.24	H	5.5				.14	.25	.20
21-59	11.9	1.23	D	8.7				.08	.14	.15
22-52	12.	1.26	H	4.4				.08	.15	.11
23-53	12.	1.23	A	5.5				.14	.15	.37
24-54	12.	1.21	F	6.0				.12	.09	.15
25-55	12.	1.24	A	8.4				.14	.15	.31
26-56	12.	1.26	B	5.0				.21	.15	.23
27-57	12.	1.27	C	8.2				.11	.14	.19
28-58	12.	1.28	B	5.0				.14	.23	.23
29-59	12.	1.29	C	6.2				(N.C.)		
30-60	12.	1.28	G	5.0				.12	.19	.15
31-61	12.	1.30	C	6.2				.11	.15	.20
32-62	12.	1.26	D	6.0				.33	.16	.22
33-63	11.8	1.27	H	4.4				.11	.23	.19
34-64	11.6	1.26	D	7.6				.09	.20	.15
End										

STRUCTURAL RESPONSE PROBE

COMPILED BY ———

DATE(S): 1-17-65

HOUSE 2-S-2

PHASE 7-B

1-17-65

DISPLACEMENT (10⁻³) in

PIN	X	Y	G	FREQ (CPS)	1	2	3	1	2	3
1-65	11.9	1.20	C	6.2	(N.R.)				(N.R.)	
2-66	12.	1.19	B	6.8						
3-67	12.5	1.24	C	6.0						
4-68	12.	1.22	A	7.0	.56	.18	.66			
5-69	12.	1.24	A	7.6	.34	.26	.90			
6-70	12.	1.23	B	6.9	.56	.14	.64			
7-71	11.9	1.26	G	8.1	.60	.22	.68			
8-72	12.	1.26	C	6.6	.28	.68	.56			
9-73	12.	1.28	G	6.8	.62	.24	.68			
10-74	11.9	1.25	H	7.5	(N.R.)				1	
11-75	12.	1.23	B	5.6	.22	.80	.38	.12	.15	.20
12-76	12.	1.24	H	5.8	.48	.94	.44	.11	.25	.19
13-77	11.8	1.21	A	5.3	.26	.16	.54	.12	.23	.62
14-78	11.9	1.20	F	7.3	.46	.14	.54	.14	.12	.25
15-79	12.	1.22	A	4.8	.22	.14	.36	.15	.19	.37
16-80	12.	1.24	B	5.2	.20	.60	.60	.14	.16	.25
17-81	12.0	1.24	C	7.0	.58	.40	.46	.11	.14	.20
18-82	12.0	1.25	B	6.8	.36	.56	.26	.15	.20	.28
19-83	12.	1.21	C	7.8	.20	.70	.42	.09	.07	.20

Structural Response Program

Compiled By ____

Date [illegible]-29-65
House [illegible]

Phase 2-B — 1-17-65

Run				Free Field	Displacement (10^{-2} in) 1	2	3		1	2	3
20-84	12.	1.24	G	5.2	(N.R.)				.11	.19	.17
21-85	11.9	1.24	G	6.6					.15	.12	.22
22-86	11.9	1.21	D	3.2					.06	.15	.12
23-87	12.0	1.26	H	5.2					.12	.20	.20
24-88	12.0	1.24	D	8.5					.06	.14	.14
25-89	11.9	1.25	E	5.5					.08	.17	.55
26-90	11.7	1.25	B	6.2					.14	.19	.26
27-91	12.	1.24	G	6.4					.09	.15	.23
28-92	12.	1.20	F	6.9					(N.R.)		
29-93	12.	1.20	A	8.4					.26	.26	.54
30-94	12.	1.20	F	7.1					.15	.11	.25
End											

Structural Response Program

Compiled By ____

Date [illegible]-29-65
House 2-5-3

Phase 2-B — 1-18-65

Run				Free Field	Displacement (10^{-2} in) 1	2	3		1	2	3
1-95	12.	1.24	G	6.5	(N.R.)				.12	.15	.32
2-96	12.	1.26	C	5.6					.11	.12	.20
3-97	12.2	1.25	G	7.4					.11	.15	.20
4-98	12.	1.25	H	6.6					.12	.26	.42
5-99	12.	1.25	D	5.4					.06	.25	.54
6-100	11.9	1.25	H	5.1					.11	.25	.20
7-101	12.	1.24	A	5.4	.26	.18	.58		.15	.19	.31
8-102	12.1	1.22	F	5.8	.44	.18	.54		.11	.11	.17
9-103	12.	1.26	A	6.3	.26	.16	.58		.15	.19	.31
10-104	11.9	1.21	E	4.8	.19	.10	.74		.15	.20	.25
11-105	12	1.23	E	5.1	.56	.46	1.16		.08	.19	.23
12-106	12.	1.23	B	5.3	.20	.10	.78		.14	.20	.22
13-107	12.	1.25	C	5.6	(N.R.)				(N.R.)		
14-108	12.	1.25	G	4.5	.64	.24	1.06		.12	.19	.20
15-109	12.	1.27	C	4.7	.54	.46	.24		.11	.11	.25
16-110	12	1.26	H	5.1	(N.R.)				.11	.25	.15
17-111	12.	1.25	D	5.4					.08	.29	.46
18-112	12.	1.29	H.	5.1					.15	.29	.26
19-113	11.8	1.20	E	4.5	.40	.10	.76		.11	.17	.57

Structural Response Program

Compiled By ______

Date [illegible] 1-29-65
House 2-5-5

Phase 2-B 1-18-65 Run	W.T	[illegible]	L/C	Fire Field AV	Displacement 10^{-2} (in.) 1	2	3		1	2	3
20-114	11.7	1.20	B	6.4	26	84	84		.20	.26	.34
21-115	12.	1.24	E	8.7	46	60	1.50		.14	.29	.52
22-116	12.	1.24	F	5.2	60	.14	1.08		.09	.17	.62
23-117	12.1	1.25	A	6.6	40	.24	1.14		.34	29	.54
24-118	12.	1.25	E	6.2	76	.14	1.40		15	.20	.66
25-119	12.	1.28	G	6.6	(NR)				.14	.20	.25
26-120	11.9	1.34	C	6.2		↓			.14	.15	.34
27-121	12.1	1.31	G	5.1					.08	.19	.12
28-122	11.8	1.22	P	8.0					.12	.29	.7
29-123	12.0	1.21	H	5.7					.12	.26	.23
30-124	12.	1.24	R.	4.7		↓			.05	.15	.08
End.											

Structural Response Program

Compiled By ______

Date [illegible] 1-29-65
House 2-5-5

Phase 2-B 1-19-65 Run	W.T	[illegible]	L/C	Fire Field AV	Displacement 10^{-2} (in.) 1	2	3		1	2	3	
1-125	12	1.25	E	6.4	.52	.20	.58		.11	.09	.29	
2-126	20.0	1.42	F	2.0	.16	.08	.24		.03	.05	.05	
3-127	30	1.45	A	2.2	12	.06	.028		.05	.08	.08	
4-128	12.	1.26	B	6.1	.26	.66	.56		.20	.29	.60	
5-129	12.	1.25	E	4.8	.26	.46	.32		.08	.17	.17	
6-130	11.	1.25	B	5.7	.26	70	.96		.11	.20	.20	
7-131	12.	1.25	C	6.2	28	.48	.48		.14	.14	.34	
8-132	12.	1.26	G	6.0	(NR)				(N.C)			
9-133	12.	1.29	C	8.1		↓				↓		
10-134	12.1	1.25	P	4.9	.20	.26	.78		.12	.15	.35	
11-135	11.9	1.29	H	5.0	.44	.90	.52		.11	.26	.22	
12-136	11.8	1.24	O	6.5	.18	.22	.28		.08	.17	.14	
13-137	25	1.33	F	3.7	.32	.36	1.70		.08	.11	.17	13-5B
14-138	25	1.29	F	3.4	.24	.26	.28		.06	.06	.15	13-5B
15-139	11.6	1.22	E	10.8	40	.60	.40		.11	.20	.23	
16-140	25.	1.35	F	3.7	.24	.24	.30		.05	.05	.17	13-5B
17-141	12	1.25	B	5.1	.24	.58	.50		.14	.17	.23	
18-142	25.	1.35	F.	3.1	.28	.32	.26		.08	.06	.23	13-5B
19-143	12.	1.22	E	6.0	.40	.48	.36		.11	.19	.17	

Structural Response Program

Compiled By ____

Date [illegible]-29-65
House 2-5-3

Phase 2-B 1-19-65 Run				Displacement (10⁻² in) Free Field V	1	2	3	—	1	2	3	
20-144	25	1.35	F	3.5	.22	.22	.28		.05	.05	.5	B-5B
21-145	30	1.42	F	2.0	(NR)				(NC)			
22-146	30	1.30	F	1.4	↓				↓			
23-147	30	1.4	F	2.2								
24-148	12.	1.24	A	5.6	.30	.18	1.02		.17	.20	.45	
25-149	11.9	1.21	G	5.1	(NR)				(NR)			
26-150	12.1	1.21	C	5.9	.40	.58	2.00		.20	.19	.57	
27-151	13.2	1.22	G	6.7	.60	.74	1.20		.15	.20	.23	
28-152	12	1.25	H	4.4	(NR)				(NR)			
29-153	12.	1.25	D	6.4	.16	.66	.26		.08	.19	.14	
30-154	12.	1.25	H	5.4	.3[illegible]	.90	.44		.12	.20	.15	
31-155	12.	1.2	A	5.2	.20	.18	.44		.15	.15	.22	
32-156	12.	1.25	F	7.4	(NR)				.12	.09	.16	
33-157	12.	1.25	A	6.4	.24	.22	.50		.20	.22	.20	
End												

Structural Response Program

Compiled By ____

Date [illegible]-29-65
House 2-5-3

Phase 2-B 1-20-65 Run				Displacement 10⁻² in. Free Field V	1	2	3	—	1	2	3
1-158	11.8	1.26	B	5.7	.12	.58	.68		.12	.26	.60
2-159	12.	1.28	E	10.0	.56	.68	1.64		.22	.20	.37
3-160	12	1.3	G	7.4	.26	.84	1.20		.15	.23	.51
4-161	12.	1.3	C	5.3	.30	.50	.40		.12	.14	.25
5-162	30.	1.4	F	7.0	(NR)				(NR)		
6-163	30.	1.3	F	1.6	.06	.04	.14		.03	.03	.05
7-164	46.	1.4	F	0.9	.10	.04	.12		.03	.02	.05
8-165	11.9	1.21	D	4.5	.22	.26	.40		.06	.12	.14
9-166	12.1	1.26	H	7.0	.38	.24	.80		.15	.23	.19
10-167	12.	1.24	D	4.7	.20	.90	.50		.08	.15	.17
11-168	11.9	1.30	E	13.3	.40	.78	.62		.11	.28	.20
12-169	12.	1.30	B	6.1	.16	.58	.88		.15	.20	.32
13-170	11.5	1.30	E	4.1	.22	.48	.32		.05	.15	.14
14-171	12.	1.28	F	4.7	(NR)				(NR)		
15-172	12.	1.30	A	5.5	.24	.30	.64		.14	.17	.25
16-173	11.7	1.30	F	4.7	.54	.18	.58		.08	.05	.09
17-174	12.	1.25	G	5.5	.58	.56	.68		.09	.17	.12
18-175	12.	1.30	C	5.6	.36	.64	.70		.09	.15	.19
19-176	12.	1.26	G	7.0	.66	.84	.74		.14	.20	.25
End											

Structural Response Program

Coupled By ______

Date [illegible]-65
House 2-5-3

Phase 7-B 1-21-65 Run				Field mV	Displacement 10^{-2} (in.) 1	2	3		1	2	3		
1-177	12.	1.30	H	5.2	.20	.44	.86		.11	26	40		
-178	12.	1.28	D	4.1	(NR)				(N.R)				
-179	12.	1.30	F	6.8	.56	1.00	.84		.26	.29	.29		
4-180	12.	1.30	A	4.2	28	.26	.56		.15	20	.40		
5-181	12	1.31	E	4.6	64	.24	28		.11	.11	.17		
6-182	12	1.30	A	4.4	.32	20	.88		.14	17	26		
7-183	12.1	1.30	B	5.3	20	56	.84		19	.23	.42		
8-184	12.1	1.31	E	4.6	.54	.42	.24		.09	.12	.17		
9-185	12.1	1.31	E	4.3	.24	[illegible]	.00		.12	.17	.28		
10-186	12.	1.30	C	[illegible]			1.00		.19	.20	.29		
11-187	12.	1.30	G		(NR)				(N.R.)				
12-188	12.	1.30	G		.34	.64	1.20		.17	23	28		
13-189	25.	1.36	F	2.5	.26	32	.58		.11	.09	.39	12	55
14-190	12.	1.29	D	5.3	(NR)				(N.R.)				
15-191	25	1.30	A	2.9	.27	.29	.52		.11	.14	.31	12	28
16-192	12.	1.31	H	3.6	.46	.74	82		.12	.25	.15		
17-193	25.	1.34	F		(NR)				(N.R.)			13	58
18-194	12.	1.30	O	4.0	.32	82	1.02		.09	.17	25		
19-195	25.	1.36	A	2.8	(NR)				(N.R.)			13	58

Structural Response Program

Coupled By ______

Date [illegible]-65
House 2-5-3

Phase 7-B 1-21-65 Run				Field mV	Displacement 10^{-2} (in.) 1	2	3		1	2	3		
20-196	25.	1.31	C	2.6	(NR)				.05	.06	.20	12	58
21-197	25.	1.35	A	2.5					.06	.12	.26	13	58
22-198	25.	1.36	F	3.2					(N.R.)			13	58
23-199	12.1	1.31	E	4.0					(N.R.)				
24-200	12.	1.34	B	4.9					.20	.20	.28		
25-201	12.	1.30	E	5.3					.08	.19	.17		
26-202	25.	1.35	F	4.6					(N.R.)			13	58
27-203	12.1	1.30	D	4.4					(N.R.)				
28-204	25.	1.37	A		.14	.18	.42		.11	.17	.39	13	58
29-205	12.	1.30	A	2.7	.46	.86	.65		.20	.26	.35		
30-206	25.	1.33	F	2.8	(NR)				(N.R.)			13	58
31-207	25.5	1.33	A	3.0	.16	.20	[illegible]		.11	.11	.45	13	58
32-208	25.5	1.35	F		.56	.14	1.2		.08	.12	.26	12	[illegible]
33-209	26.5	1.37	A	2.6	(NR)				.11	.09	.19	13	[illegible]
34-210	12.	1.23	H	2.5					(N.R.)				
35-211	25.5	1.36	F	3.1					.09	.08	.19	5	[illegible]
36-212	12.	1.28		3.6					.06	16	.4		
37-213	25.	1.36	A	2.9					.11	.12	[illegible]	13	[illegible]
39-215	25.	1.37	F						.05	.06	[illegible]		

STRUCTURAL RESPONSE PROGRAM

COMPILED BY _____

DATE 1-21-65 : 1-29-65

HOUSE 2-S-3

PHASE 2-R				DISPLACEMENT 10^{-2} in							
1-21-65				Free Field	1	2	3		1	2	3
PIN	X	Y	Z/C	N			V				
40-216	12.	130	G	(-)	L	N.R.	)		(N.R.)		
41-217	11.9	128	C	5.2					.15	.15	.31
42-218	12.	131	G	5.2					.15	.25	.17
43-219	12.	131	H	7.9	.62	.110	.80		.14	.34	.35
44-220	11.9	134	D	4.0	.20	.38	.62		.06	.14	.11
45-221	11.7	131	H	8.8	(N.R.)				.19	.31	.26
End											

STRUCTURAL RESPONSE PROGRAM

COMPILED BY _____

DATE 1-21-65 : 1-29-65

HOUSE 2-S-3

PHASE 2-R				DISPLACEMENT 10^{-2} in							
1-22-65				Free Field	1	2	3		1	2	3
PIN	X	Y	Z/C	N			V				
1-222	12.	130	A		.32	.28	.80		.34	.21	.65
2-223	12.	130	F	.35	.44	.34	.40		.09	.11	.09
3-224	12.	132	A	4.6	.28	.30	.62		.12	.20	.22
4-225	12.	127	B	10.7	.24	.112	.58		.19	.26	.46
5-226	12.	126	E	12.9	.70	.60	.84		.20	.32	.37
6-227	12.	127	B	5.1	.16	.64	.46		.06	.17	.20
7-228	11.9	133	C	4.3	(N.R.)				(N.R.)		
8-229	12.	131	G	3.7	.44	.68	.60		.09	.17	.14
9-230	12.1	132	C	7.1	.46	.34	.54		.11	.19	.17
10-231	30-21	44-12	F	1.6	.20	.26	.26		.05	.06	.06
11-232	30-8	44-12	A	1.6	.28	.16	.50		.05	.07	.11
12-233	30-20	44-10	F	2.2	-	.2	)		(	N.R.	)
13-234	30-0	44-11	A	5.9							
14-235	11.98	135	E	4.5	.41	.50	.110		.11	.12	.19
15-236	11.9	136	B	5.9	.24	.84	.96		.22	.12	.32
16-237	12.	131	G	4.2	.12	.31	.48		.09	.12	.12
17-238	12.	129	F	6.2	.36	.48	.80		.08	.10	.11
18-239	12.	134	H	3.7	.16	.24	.60		.11	.19	.22
19-240	11.	135	F	7.2	.56	.46	.64		.12	.11	.19

STRUCTURAL RESPONSE RECORD

COMPILED BY _____

DATE 6-6-65 : 6-29-65
HOUSE 2-5-5

PHASE 2-A				DISPLACEMENT (10⁻³ in.)								
1-22-65				FREQ FREQ	1	2	3		1	2	3	
PIN												
20-246	16.	1.41	C	2.	(N/R)				(N/R)			
21-262	16.5	1.41	C	1.9								
22-263	20.	1.2	G	0.9								
23-264	18.2	1.4	E	2.6								
24-265	20.2	1.4	A	2.1								
25-266	18.5	1.6	F	4.6								
26-267	18.5	1.6	A	1.8								
27-268	25.	1.41	A	1.5								
28-269	25.	1.4	F	2.4								
29-250	25.	1.4	A	1.6								
30-251	24.9	1.4	E	2.3								
31-252	25.	1.5	B	0.4								
32-253	25	1.4	G	1.6								
33-254	25	1.5	B									
End												

STRUCTURAL RESPONSE RECORD

COMPILED BY _____

DATE 6-6-65 : 6-29-65
HOUSE 2-5-5

PHASE 2-B				DISPLACEMENT (10⁻³ in.)								
1 23-65				FREQ FREQ	1	2	3		1	2	3	
PIN												
1-255	11.9	1.25	C		.22	.56	.68		.15	.25	.31	
2-256	11.9	1.25	G	6.9	.42	.60	.46		.14	.14	.20	
3-257	11.93	1.25	C	4.6	.20	.42	.54		.06	.17	.17	
4-258	11.3	1.30	D	4.7	.10	.62	.46		.06	.15	.19	
5-259	12.	1.29	H	6.0	.38	.86	.66		.09	.23	.19	
6-260	12.	1.3	D	3.1	.18	.74	.60		.05	.17	.15	
7-261	12	1.28	G	6.7	.48	.58	.72		.14	.29	.54	
8-262	12.	1.27	B	4.3	.18	.73	.78		—	.19	.26	
9-263	12.	1.28	E	2.9	(N/R)				—	.11	.15	
10-264	12.	1.3	B	3.7					.11	.14	.20	
11-265	11.9	1.3	E	4.9					.15	.15	.20	
12-266	11.9	1.31	A	4.0					.15	—	.28	
13-267	11.9	1.34	E	3.1					.05	—	.19	
14-268	25.	1.34	E	2.8					(N/R)			B-5B
15-269	12.	1.29	G	3.1					.11	.11	.12	
16-270	25.	1.35	A						.06	.09	.20	B-5B
17-271	12.1	1.27	C	3.8					.11	.17	.32	
18-272	25.	1.32	E	4.1					.09	.09	.25	B-5B
19-273	12.	1.26	G	5.7					.16	.15	.25	

STRUCTURAL RESPONSE RECORD

COMPILED BY _____

DATE 1-23-65 thru 2-9-65

HOUSE 2-S-5

PHASE 7-B

1-23-65

PIN	N-S	E-W	S/C	FREQ (cps)	DISPLACEMENT 10^{-3} (in) 1	2	3	1	2	3	
20-276	25.	1.34	A	2.2	(N.R.)			.09	.14	.35	B-SB
21-277	25.	1.35	A	2.8				.11	.05	.25	B-SB
22-278	25.	1.36	A	2.6				.06	.08	.26	B-SB
23-277	25.	1.36	A	2.3				—	.09	.39	B-SB
24-278	24.6	1.35	A	3.1					(N.R.)		B-SB
25-279	12.	1.26	H	5.2					(N.R.)		
26-280	12.	1.31	D	2.2				—	.12	.06	
27-281	12.	1.28	N	7.1				.11	.31	.31	
28-282	12.	1.28	D	12.7				.14	.34	.28	
29-283	25.	1.36	A	2.9				.05	.06	.22	B-SB
30-284	25.	1.36	A	2.1				.05	.05	.20	B-SB
31-285	12.	1.29	B	3.1				.11	.25	.23	
32-286	25.	1.36	E	2.6				.08	.05	.19	B-SB
33-287	12.05	1.29	E	6.6				.14	.23	.23	
34-288	25.	1.37	A	2.1				.08	.03	.17	B-SB
35-289	12.	1.29	B	4.2				.29	.23	.49	
36-290	25.	1.37	A	9				.03	.02	.11	B-SB
37-291	25.	1.37	A	9				.08	.09	.31	B-SB
38-292	25.	1.36	A	18.1					(N.R.)		B-SB

STRUCTURAL RESPONSE RECORD

COMPILED BY _____

DATE 1-23-65 thru 2-9-65

HOUSE 2-S-5

PHASE 7-B

1-23-65

PIN	N-S	E-W	S/C	FREQ (cps)	DISPLACEMENT 10^{-3} (in) 1	2	3	1	2	3	
39-293	12.	1.25	C	5.3	(N.R.)			.19	.19	.25	
40-294	25.	1.37	A	2.9				.05	.11	.43	
41-295	12.	1.26	G	8.7				.05	.11	.06	
42-296	25.	1.37	E	2.2				.06	.05	.15	
43-297	12.	1.25	C	7.2					(N.R.)		
44-298	12.	1.26	G	7.3				.28	.34	.49	
45-299	12.	1.26	N	8.7				.11	.34	.26	
46-300	12.1	1.25	D	2.8				.03	.12	.09	
47-301	12.	1.26	N	8.1				.12	.29	.25	
48-302	12	1.29	B	4.2					(N.R.)		
49-303	12	1.34	B	4.2				.20	.25	.35	
50-304	12.	1.34	B	4.8				.11	.23	.29	
End											

Structural Response Program

Compiled By ______

Date 1-25-65 : 1-29-65
House 2-5-5

Phase 7-B 1-24-65				Displacement (10⁻² in)							
Run	W.F.	[illegible]	[illegible]	Far Field	1	2	3		1	2	3
1-305	12.	1.22	F	4.4	.42	.24	.68		.11	.08	.35
2-306	12.	1.22	A	4.6	.24	.32	.62		.15	.14	.37
3-307	12.	1.20	F	4.2	.48	.20	.68		.11	.14	.17
4-308	11.95	1.25	A	3.0	.20	.22	.40		.11	.09	.29
5-309	12.2	1.22	G	4.9	.36	.60	.56		.09	.15	.15
6-310	12	1.22	C	4.4	.18	.62	.60		.08	.11	.28
7-311	12	1.20	G	4.5	.40	.76	.60		.11	.17	.72
8-312	12.	1.20	C	4.4	.22	.56	.68		.17	.11	.37
9-313	12.	1.25	H	4.8	.34	1.10	.54		.12	.28	.34
10-314	12.	1.25	D	5.0	(NR)				.06	.15	.14
11-315	12.	1.25	H	4.2					.09	.26	.26
12-316	12.	1.25	D	4.5					.08	.14	.15
13-317	12.	1.24	A	4.4					.12	.14	.32
14-318	12.	1.24	F	5.3					.11	.01	.11
15-319	12.	1.26	A	3.6					.12	.11	.31
16-320	12.	1.21	B	6.1					.25	.19	.49
17-321	12.1	1.20	E	5.7					.09	.17	.23
18-322	11.95	1.20	B	4.1					.09	.16	.26
19-323	12.	1.22	E	3.9					.09	.14	.15

Structural Response Program

Compiled By ______

Date 1-25-65 : 1-29-65
House 2-5-5

Phase 7-B 1-24-65				Displacement (10⁻³ in)							
Run	W.F.	[illegible]	[illegible]	Far Field	1	2	3		1	2	3
20-324	12.	1.23	G	6.1	(NR)				.15	.15	.31
21-325	12.	1.23	G	5.4					.08	[illegible]	.26
22-326	12.	1.26	G						.11	.15	.28
23-327	12.	1.26	G	4.3					.09	.11	.14
24-328	12.	1.20	H	7.4					(N.R.)		
25-329	12.	1.21	D	4.6					.05	.14	.12
26-330	12.	1.21	H						.15	.26	.45
27-331	12.	1.20	D	6.5					.11	.14	.22
28-332	12.	1.21	E	4.6					.09	.15	.19
29-333	12.	1.24	B	3.8					.11	.14	.26
30-334	12.	1.23	A	8.1					.11	.20	.19
31-335	12.	1.25	B	4.1					.09	.12	.28
32-336	11.9	1.20	F	4.2					(N.R.)		
33-337	12.	1.2	A						.06	.06	.22
34-338	12.	1.21	F						.06	.06	.08
35-339	12.	1.21	A	3.9					.06	.09	.37
36-340	12.	1.21	G	3.0					.08	.20	.28
37-341	12.	1.20	C	4.9					.12	.12	.37
38-342	12.	1.22	G	4.4					.12	.23	.25
39-343	12.	1.22	C	3.9					.04	.04	.29

STRUCTURAL RESPONSE PROGRAM

COMPILED BY ______

DATE 1-25-65: 1-29-65
HOUSE 2-5-5

PHASE 7-B				DISPLACEMENT 10⁻² (in.)							
1-25-65				Free Field	1	2	3		1	2	3
RUN	[illegible]	[illegible]	[illegible]	AV	[illegible]	[illegible]	[illegible]		[illegible]	[illegible]	[illegible]
1-344	12.	1.34	H		(NR)				(N.R)		
2-345	12	1.30	D	-	.12	.52	.48		.02	.15	08
3-346	12.	1.30	H	-	.30	.76	.66		.12	.22	.31
4-347	12.0	1.26	A	-	.08	.26	.34		.02	.08	.11
5-348	12.	1.33	F	-	.44	.26	.48		.09	.08	.09
6-349	12.	1.31	A	-	.20	.18	.50		.08	08	.17
7-350	12.	1.32	S	-	.22	.92	.84		.09	.17	.20
8-351	12.	1.34	B	3.2	.26	.36	.38		.23	.08	.09
9-352	11.8	1.26	B	9.3	.24	.80	.90		.28	.28	62
10-353	12.5	1.3	C	3.2	(NR)				(N.R)		
11-354	12.1	1.31	G	2.6	.64	1.00	.74		15	.20	.19
12-355	13.	1.30	C	3.7			.50		.11	11	20
13-356	12.	1.25	D	2.9	(N.R)				(N.R)		
14-357	11.	1.15	H	12.9					15	.35	.72
15-358	16.	1.40	D	2.5					.05	.09	.09
16-359	13.	1.30	E	-					(N.R)		
17-360	11.9	1.35	B	4.1						↓	
18-361	12.9	1.33	E	2.9					.09	.11	.15
19-362	12.	1.26	F	3.0					.06	06	.06

STRUCTURAL RESPONSE PROGRAM

COMPILED BY ______

DATE 1-25-65: 1-29-65
HOUSE 2-5-5

PHASE 7-B				DISPLACEMENT 10⁻² (in)							
1-25-65				Free Field	1	2	3		1	2	3
RUN	[illegible]	[illegible]	[illegible]	AV	[illegible]	[illegible]	[illegible]		[illegible]	[illegible]	[illegible]
20-363	12.	[illegible]	[illegible]	3.2	(NR)				.19	.12	.32
21-364	12.	1.32	F	3.5					.06	.06	.09
22-365	12.	1.30	G	5.6					.11	.15	.16
23-366	12.	1.29	C	3.7					.06	.08	.15
24-367	14.8	1.39	G	2.5					.06	.11	.12
25-368	14.	1.35	C	3.2					.06	.12	.15
26-369	12.	1.35	H	6.6					.08	.22	.20
27-370	12.2	1.30	D	6.4					.08	.20	.12
28-371	11.7	1.26	H	—					.06	.15	.19
29-372	12.9	1.25	F	3.0					.06	.08	.09
30-373	12.8	1.31	A	5.3					.08	.09	.07
End											

STRUCTURAL RESPONSE PROFILE

COMPILED BY _____

DATE 6-6-65 : 7-29-65
HOUSE 2-5-5

PHASE 2-A				DISPLACEMENT 10⁻² (in.)								
1-26-65				Field	1	2	3		1	2	3	
PIN	H.F	Vib.	Loc	Δ								
1-376	12.	1.32	B	-	(NR)				.12	.15	.31	
2-375	12.05	1.36	E	4.0	.56	.80	.72		.11	.14	.28	
3-376	12.	1.33	B	4.1	.56	.44	.44		.11	.17	.20	
4-377	12.	1.31	C	5.0	.46	.74	.60		.11	.11	.34	
5-378	12.	1.32	G	-	.42	.48	.48		.11	.26	.20	
6-379	12	1.32	C	-	.80	.80	.87		.09	.09	.27	
7-380	12.05	1.33	D	4.5	.46	.58	.50		.05	.14	.15	
8-381	11.95	1.30	H	7.0	.56	.76	.62		.05	.26	.25	
9-382	11.95	1.31	D	4.8	.72	1.00	.44		.06	.12	.14	
10-383	12.	1.30	H	2.5	(NR)				.08	.26	.17	
11-384	12.	1.30	E	8.1	.40	.74	.44		.08	.12	.20	
12-385	12.	1.30	B	6.9	.68	.94	.44		.14	.15	.26	
13-386	12.	1.30	E	5.0	.54	.62	.42		.09	.14	.15	
14-387	12.	1.25	B	-	.46	.60	.54		.09	.15	.20	
15-388	25.	1.34	F	9.0	.52	.44	.54		.06	.08	.25	B-SB
16-389	25.	1.37	A	9.4	.34	.18	.46		.09	.08	.35	B-SB
17-390	12.	1.31	G	5.5	.66	.72	.56		.09	.22	.15	
18-391	25.	1.37	F	4.6	.56	.46	.42		.06	.12	.93	B-SB
19-392	12.	1.34	C	-	.26	.64	.90		.23	.20	.54	

STRUCTURAL RESPONSE PROFILE

COMPILED BY _____

DATE 6-6-65 : 7-29-65
HOUSE 2-5-5

PHASE 2-A				DISPLACEMENT 10⁻² (in.)								
1-26-65				Field	1	2	3		1	2	3	
PIN	H.F	Vib.	Loc	Δ								
20-393	25.	1.37	A	4.7	.60	.20	.56		.14	.15	.48	B-SB
21-394	12.	1.34	G	2.7	.70	.90	.60		.11	.20	.14	
22-395	25.	1.34	F	2.2	(NR)				.03	.06	.15	B-SB
23-396	12.	1.30	C	4.7	.42	.40	.40		.08	.11	.23	
24-397	25.	1.30	A	9.5	.40	.18	.34		.09	.08	.40	B-SB
25-398	25.	1.28	F	6.7	.50	.40	.40		.05	.11	.25	B-SB
26-399	25.	1.38	A	2.1	.48	.16	.42		.05	.09	.31	B-SB
27-400	12.	1.34	H	3.6	.58	.48	.74		.11	.20	.25	
28-401	11.9	1.25	D	2.0	.38	.86	.60		.02	.20	.19	
29-402	11.95	1.31	H	-	.62	.60	.56		.06	.19	.23	
30-403	12.	1.35	D	7.1	.48	.48	.66		.09	.15	.19	
31-404	25.	1.37	F	2.6	(NR)				(N.A.)			B-SB
32-405	25.	1.32	A	4.7	.72	.16	.70		.11	.12	.31	B-SB
33-406	25.	1.38	F	9.1	(NR)				(N.A.)			B-SB
34-407	12.	1.33	G	3.8	.70	.74	.54		.09	.20	.12	
35-408	25.	1.38	A	8.6	.34	.16	.56		.05	.08	.54	B-SB
36-409	12.	1.33	G	4.5	.34	.42	.48		.06	.08	.17	
37-410	25.	1.37	F	5.8	.86	.46	.60		.08	.11	.20	B-SB
38-411	11.9	1.35	G	7.3	.24	.40	.60		.19	.20	.17	

STRUCTURAL RESPONSE PROFILE

COMPILED BY _____

DATE 1-29-65

HOUSE 2-5-5

PHASE 7-B — DISPLACEMENT 10^{-2} in.

1-26-65

PIN	H.F.	Vel.	Loc.	Peak Value	1	2	3	1	2	3	
39-440	25.	1.37	A	2.8	.50	.14	.56	.05	.09	.20	13:58
40-441	25.	1.37	A	2.5	.22	.36	.08	.03	.09	.17	12:58
41-442	25.	1.38	A	–	.56	1.12	.56	.08	.11	.46	12:58
42-443	25.	1.38	A	3.7	(N.R.)			(N.R.)			12:59
43-446	25.	1.41	A	2.5	.38	.12	.32	.03	.03	.26	13:58
44-447	12.	1.28	H	6.0	.90	1.20	.90	.14	.26	.32	
45-448	12.	1.25	H	4.2	1.98	.46	.46	.05	.28	.20	
46-449	12.	1.20	D	3.5	.44	1.28	.46	.05	.28	.15	
47-450	12.	1.31	G	4.0	.48	.60	.40	.08	.17	.09	
48-451	12.	1.31	C	3.7	.48	.30	.32	–	.08	.11	
49-452	12.	1.33	G	7.6	.88	.74	.74	.14	.14	.14	
50-453	12.	1.26	H	7.2	.88	.56	.64	.14	.29	.31	
51-454	12.2	1.3	D	3.6	.56	.66	.38	.05	.12	.12	
52-455	22.	1.3	H	8.2	1.80	1.26	1.16	.14	.26	.29	
End											

STRUCTURAL RESPONSE PROFILE

COMPILED BY _____

DATE 1-29-65

HOUSE 2-5-5

PHASE 7-B — DISPLACEMENT 10^{-2} in.

1-27-65

PIN	H.F.	Vel.	Loc.	Peak Value	1	2	3	1	2	3	
1-426	12.	1.26	H	3.9	.50	1.00	.56	.14	.23	.29	
2-427	11.95	1.23	H	5.2	1.96	.12	.32	.08	.23	.20	
3-428	11.95	1.23	D	–	.60	.90	.80	.11	.20	.28	
4-429	12.	1.25	H	3.9	.62	.84	.60	.08	.23	.17	
5-430	11.95	1.25	G	4.6	.86	.58	.88	.11	.14	.29	
6-431	11.95	1.26	B	5.4	.46	.60	.90	.11	.20	.26	
7-432	12.	1.30	G	4.5	.64	.50	.52	.08	.15	.17	
8-433	12.	1.30	G	4.2	.28	.66	.70	.05	.20	.23	
9-434	12.	1.26	H	4.3	.70	.24	.50	.12	.09	.15	
10-435	11.8	1.26	A	4.6	.38	.26	.40	.12	.14	.25	
11-436	12.	1.31	H	–	.80	.20	.50	.12	.11	.19	
12-437	12.	1.26	A	–	.42	.40	.50	.14	.12	.29	
13-438	11.5	1.25	H	5.8	.66	.26	.40	.11	.09	.11	
14-439	12.0	1.32	A	6.1	.30	.50	.50	.08	.12	.23	
15-440	12.	1.28	G	7.0	.54	.76	.60	.09	.12	.11	
16-441	12.	1.25	C	4.8	.40	.60	.50	.11	.11	.20	
17-442	12.05	1.24	G	4.5	1.40	1.00	.90	.17	.20	.28	
18-443	12.	1.25	C	5.0	.66	.66	.60	.14	.12	.12	
19-444	12.	1.25	G	6.5	.74	.64	.74	.14	.12	.20	

STRUCTURAL RESPONSE PROGRAM

COMPILED
By ______

DATE 1-65: 1-29-65
HOUSE 2-5-5

PHASE 7-B 1-27-65				Displacement 10^{-2} (in)							
Run	W.T.	V	Loc	Fld	1	2	3		1	2	3
20-445	12.	1.25	H	-	.86	1.00	.52		.11	.23	.14
21-446	12.	1.25	D	3.7	.20	.82	.64		.02	.14	.09
22-447	12.	1.22	H	5.7	.60	1.04	.52		.09	.23	.12
23-448	12.	1.22	D	5.5	.64	1.08	.78		.06	.20	.12
24-449	12.0	1.25	H	5.6	.60	.92	.56		.08	.22	.12
25-450	12.	1.22	D	11.4	.58	1.06	.94		.06	.19	.14
26-451	12.	1.20	F	6.6	.64	.36	.74		.08	.06	.22
27-452	12.	1.20	A	3.8	.40	.18	.56		.06	.08	.12
28-453	12.	1.2	F	15.3	.70	.26	.56		.09	.09	.12
29-454	12.	1.15	A	4.4	.16	.52	.40		.06	.11	.12
30-455	12.	1.2	F	5.9	.86	.28	.64		.11	.11	.23
End											

STRUCTURAL RESPONSE PROGRAM

COMPILED
By ______

DATE 1-65: 1-29-65
HOUSE 2-5-5

PHASE 7-B 1-28-65				Displacement 10^{-2} (in)							
Run	W.T.	V	Loc	Fld	1	2	3		1	2	3
1-456	12	1.24	G	5.0	.48	.66	.74		.11	.17	.29
2-457	12.	1.22	C	5.7	.62	.52	.48		.11	.12	.14
3-458	12.	1.27	G	4.8	.46	.62	.74		.09	.15	.20
4-459	11.95	1.2	C	-	.52	.54	.56		.08	.20	.14
5-460	12.05	1.25	G	4.2	(N.R.)				(N.R.)		
6-461	12.	1.2	C	4.8	.44	.58	.72		.09	.14	.31
7-462	12.	1.29	G	4.9	.78	.74	.70		.12	.20	.20
8-463	12.	1.23	G	3.9	.70	.66	.48		.11	.15	.14
9-464	12.	1.22	C	5.2	.42	.52	.50		.08	.12	.22
10-465	12.	1.20	G	5.1	.78	.80	.54		.12	.19	.25
11-466	12.	1.22	C	5.2	.50	.54	.60		.09	.15	.31
12-467	12.	1.26	G	6.6	.84	.80	.86		.11	.23	.22
13-468	12.	1.25	C	5.0	.26	.60	1.40		.11	.14	.39
14-469	12.	1.26	G	4.9	.80	.80	.80		.12	.23	.19
15-470	12.	1.26	C	4.7	.72	.62	1.52		.11	.14	.35
16-471	12.	1.26	G	-	.76	.74	.60		.11	.17	.14
17-472	12.	1.26	C	12.1	.50	.50	.84		.09	.14	.29
18-473	11.95	1.26	G	3.3	.66	.70	.60		.11	.14	.14
19-474	12.	1.26	G	5.1	(N.R.)				(N.R.)		

Structural Response Program

Compiled By ______

Date 1-28-65 : 1-29-65
House 2-5-5

Phase 7-B 1-28-65				Displacement (10⁻² in)							
Run	[illegible]	[illegible]	[illegible]	Free Field	1	2	3	—	1	2	3
20-475	12	1.22	G	4.3	.80	.86	.28		.11	15	25
21-476	12.	1.26	C	3.5	.42	.44	.42		.19	.11	29
22-477	12.	1.25	G	6.0	.80	.98	.54		.14	.19	17
23-478	12.	1.22	C	4.8	.46	.54	.40		.05	.12	.15
24-479	12.	1.21	D	–	.54	.94	.98		.08	.20	.63
[illegible]-480	12	1.20	H	6.2	1.00	1.40	.80		.17	.26	22
26-481	12.0	1.21	D	–	.58	.86	.54		11	.17	.49
27-482	12.1	1.24	[illegible]	6.5	.74	1.10	.68		.11	.23	.14
28-483	12.	1.25	D	4.9	.58	.92	.78		.09	.20	.66
29-484	12.5	1.27	E	4.9	.66	.32	.10		.09	.08	21
30-485	12.	1.28	A	5.1	.42	.18	.58		.11	.11	.22
31-486	12.	1.27	F	4.7	.26	.30	.26		.08	.09	.28
32-487	12.	1.28	E	5.6	.60	.34	.60		.09	.09	.22
33-488	12.	1.2	[illegible]	5.1	.32	.70	.44		.06	.14	.12
34-489	12	1.22	E	3.0	.40	.50	1.16		.09	.08	.26
35-490	12.	1.24	[illegible]	4.2	.60	.76	.24		.15	23	.43
36-491	12.	1.22	E	–	.66	.42	.74		.12	.11	.49
37-492	12.	1.24	A	3.3	.40	.24	.58		.09	.14	.26
38-493	12.05	1.25	F	3.6	.60	.34	.64		.11	.04	.15
39-494	12.05	1.24	A	6.8	.46	.26	.78		.17	.11	.31

Structural Response Program

Compiled By ______

Date 1-28-65 : 1-29-65
House 2-5-5

Phase 7-B 1-29-65				Displacement (10⁻² in)							
Run	[illegible]	[illegible]	[illegible]	Free Field	1	2	3	—	1	2	3
1-495	12.	1.24	C	8.0	(N.R.)				(N.R.)		
2-496	12.	1.24	G	4.4	.86	.80	.28		.12	.19	.14
3-497	12.	1.24	C	5.0	.60	.52	.68		.12	.14	.29
4-498	12.	1.24	D	5.2	(N.R.)				(N.R.)		
5-499	12.	1.25	H	2.6	.58	1.00	.48		.08	.25	.12
6-500	12.	1.28	D	3.5	.28	.74	.34		.05	15	.12
7-501	12.	1.21	D	—	.32	.72	.64		.05	.12	.14
8-502	12.	1.26	H	4.2	.52	1.02	.42		.11	.29	.17
9-503	12.	1.25	D	4.0	.44	.60	1.14		.08	.15	25
10-504	12.05	1.22	E	6.1	.26	.40	.46		.11	.08	.39
11-505	12.05	1.24	A	3.6	.14	.14	.26		.11	.4	.10
12-506	12.	1.22	F	4.2	.26	.20	.66		.12	.09	.09
13-507	12.	1.23	A	4.9	.26	.14	.26		.09	.09	.17
14-508	12.	1.25	G	2.8	(N.R.)				(N.R.)		
15-509	12	1.23	C	5.8	.50	.58	[illegible]		.14	.17	.22
16-510	12.	1.25	G	4.6	(N.R.)				(N.R.)		
17-511	12.	1.25	C	6.1	.40	.44	.4		.04	.12	.15
18-512	12.	1.22	H	6.4	.74	1.48	.74		.12	.31	.23
19-513	11.8	1.20	D	5.0	.34	1.00	44		.04	.14	.20

STRUCTURAL RESPONSE PROFILE

COMPILED BY _____

DATE 1-29-65 to 1-30-65

HOUSE 2-S-9

PHASE 2-B 1-29-65				Free Field	DISPLACEMENT (in.)					
PIN					1	2	3	1	2	3
20-516	12.	1.24	H	5.2	.50	.34	.50	.11	.23	.19
21-515	12.	1.24	D	5.7	.34	.26	.44	.06	.15	.15
22-516	12.	1.21	A	4.4	.40	.18	.40	.11	.11	.15
23-517	12.	1.22	E	5.9	(N.R.)			(N.R.)		
24-518	12.	1.23	B	6.2	.44	.36	.28	.09	.14	.31
25-519	12	1.22	F	10.2	.92	.32	.60	.12	.09	.23
26-520	12.	1.24	B	-	.50	.64	.70	.14	.22	.25
27-521	12.	1.24	C	6.3	.54	.86	.50	.11	.14	.24
28-522	12.	1.24	B	7.6	.48	.80	.28	.14	.20	.28
29-523	12.1	1.26	E	3.4	.36	.30	.24	.05	.06	.12
30-524	12.02	1.23	C	6.2	(N.R.)			(N.R.)		
31-525	12.	1.26	G	3.3	.52	.82	.36	.09	.17	.11
32-526	12.05	1.25	C	-	.40	.44	.64	.09	.09	.12
33-527	11.95	1.15	D	5.9	.78	.86	.66	.06	.17	.19
34-528	12.	1.24	H	7.5	(N.R.)			.05	.17	.11
35-529	12.05	1.18	D	10.3	.82	1.80	.78	.15	.25	.37
End										

STRUCTURAL RESPONSE PROFILE

COMPILED BY _____

DATE 1-30-65 to 2-7-65

HOUSE 2-S-5

PHASE 2-B 1-30-65				Free Field	ACCELEROMETERS (g)												DISPLACEMENT (in.)					
PIN					1	2	3	4	5	6	7	8	9	10	11	12	1	2	3	1	2	3
1-530	12.	1.24	K	5.6	NR	NR	NR	NR	NR	NR	N/C	N/C	N/C	N/C	NR	N/C	.58	.38	.50	.09	.08	.14
2-531	12.	1.25	B	6.2													.36	.60	.64	.15	.15	.31
3-532	12.	1.25	G	4.7													.66	.46	.54	.11	.14	.20
4-533	12.	1.24	F	5.2													.76	.24	.54	.11	.11	.14
5-534	12.	1.24	A	4.7													.38	.20	.88	.14	.12	.26
6-535	11.94	1.25	F	4.7													.12	.26	.54	.11	.11	.14
7-536	12.	1.19	G	5.1													.72	.96	.48	.14	.20	.15
8-537	12.	1.23	C	5.2													.50	.58	.46	.11	.12	.23
9-538	12.05	1.22	G	4.5													.70	.70	.56	.14	.17	.14
10-539	12.0	1.25	H	4.3													.64	.98	.40	.12	.20	.20
11-540	12.0	1.25	D	3.7													.40	.70	.32	.03	.15	.11
12-541	12.0	1.25	H	4.3													.46	.12	.56	.11	.22	.12
13-542	12.0	1.20	A	5.2													.32	.24	.28	.09	.09	.31
14-543	12.0	1.20	F	4.9													.80	.22	.40	.09	.08	.19
15-544	11.9	1.18	A	4.5													.36	.16	.40	.09	.08	.20
16-545	12.0	1.21	E	NR													(N/A)			.12	.15	.25
17-546	12.0	1.23	E	5.2													.46	.44	.24	.14	.09	.20
18-547	12.	1.23	B	3.4													.42	.66	.46	.09	.15	.12
19-548	12.	1.23	C	3.1													.54	.44	.40	.06	.09	.20

Structural Response Program

Compiled By _____

Date 1-30-65 2-7-65
House 2-5-5

Phase 2-B

1-30-65

Accelerometers (g)

Displacement (10⁻³ in.)

Run	Hr	Min	Sec	Sw	Field	1	2	3	4	5	6	7	8	9	10	11	12	1	2	3	1	2	3
20-548	12.	1.24	G	7.8		NR	NR	NR	NR	NR	NR	NR	NR	NR	NR	NR	NR	49	68	46	.08	.11	.12
21-550	12.	1.24	C	4.4														.72	60	94	.08	.11	.37
22-551	12	1.20	D	4.4														(	V.L.	)	(	N.R.	)
23-552	12.	1.21	H	7.3														64	104	54	.12	.14	.22
24-553	12.	1.21	D	4.4														(	V.L.	)	.08	.15	.39
25-554	12.	1.19	E	7.6																	.11	.11	.45
26-555	12	1.19	B	NR																	.17	.20	.31
27-556	12.	1.20	E	8.3																	.09	.08	.36
28-557	12.	1.22	A	5.4																	.14	.11	.22
29-558	12.	1.7	A	5.0														.44	.44	.84	.15	.11	.32
30-559	12.	1.27	E	6.7														(	V.L.	)	.09	.08	.40
End																							

Structural Response Program

Compiled By _____

Date 1-30-65 2-7-65
House 2-5-5

Phase 2-B

1-31-65

Accelerometers (g)

Displacement (10⁻³ in.)

Run	Hr	Min	Sec	Sw	Field	1	2	3	4	5	6	7	8	9	10	11	12	1	2	3	1	2	3
1-560	11.97	1.25	E	7.6														(	V.L.	)	(	N.R.	)
2-561	12.	1.25	B	3.9														.42	.76	.80	.06	.17	.19
3-562	11.95	1.26	E	4.8														.52	.40	.58	.09	.11	.13
4-563	12.	1.26	B	4.5														.68	.40	.48	.09	.11	.22
5-564	12.	1.25	A	4.2														.34	.22	.40	.12	.11	.23
6-565	12.05	1.26	C	7.6														(	.26	.42	.11	.08	.11
7-566	12.	1.24	G	7.4														.5	.40	.62	.15	.17	.20
8-567	12.	1.22	C	4.8														.44	.40	.48	.08	.11	.20
9-568	12.	1.23	G	4.3														.64	.64	.60	.12	.15	.14
10-569	12.	1.23	H	NR														.40	1.14	.42	.C	.22	.19
11-570	12.	1.25	B	6.5														(	V.L.	)	(	N.R.	)
12-571	12.	1.23	D	5.7														.40	.18	.36	.03	.15	.15
13-572	12.	1.25	E	4.1														.26	.28	.44	.08	.09	.22
14-573	12.	1.22	H	6.1														.26	1.16	.70	.19	.23	.31
15-574	12.	1.26	E	4.0														.2	.16	.20	.11	.06	.12
16-575	12.	1.25	A	3.4														.3	.28	.40	.15	.09	.29
17-576	12.	1.27	E	4.0														.46	.14	.46	.11	.06	.11
18-577	12.	1.24	A	4.2														.24	.14	.42	.09	.09	.31
19-578	12.	1.26	B	4.7														.28	.11	.1	.09	.14	.20

NOT REDUCED

D-67

Structural Response Program

Compiled By____

Date 1-30-65 2-7-65
House 2-5-5

Phase 2-B 1-31-65 Run	kt	Hz	Loc	Free Field psi	Accelerometers (g) 1	2	3	4	5	6	7	8	9	10	11	12	Displacement (10⁻³ in.) 1	2	3	1	2	3
20-579	12.	1.25	E	NR	NOT REDUCED	NOT REDUCED	NOT REDUCED	NOT REDUCED	NOT REDUCED	NOT REDUCED	NOT REDUCED	NOT REDUCED	NOT REDUCED	NOT REDUCED	NOT REDUCED	NOT REDUCED	.76	.42	.6	.09	.08	.15
21-580	12.	1.26	B	4.5													40	.6	.50	.09	.14	.20
22-581	12.	1.22	C	6.6													.42	.66	.94	.11	.11	.25
23-582	12.	1.23	G	4.7													.60	.96	.50	.11	.15	.12
24-583	12.	1.22	E	5.6													.50	.26	.46	.17	.15	.35
25-584	12.	1.20	D	3.4													.26	.46	.42	.03	.14	.09
26-585	12	1.24	H	4.6													.80	1.00	.72	.09	.20	.20
27-586	12.	1.21	D	2.0													.20	.56	.18	.03	.12	.09
28-587	12.	1.22	E	NR													.48	.48	.40	.09	.09	.20
29-588	12.	1.25	B	4.9													(NR)			.15	.15	.35
30-589	12.	1.24	E	4.2																.15	.14	.29
End.																						

Structural Response Program

Compiled By____

Date 1-30-65 2-7-65
House 2-5-5

Phase 2-B 2-1-65 Run	kt	Hz	Loc	Free Field psi	Accelerometers (g) 1	2	3	4	5	6	7	8	9	10	11	12	Displacement (10⁻³ in.) 1	2	3	1	2	3
1-590	12.	1.24	G	5.2		NOT REDUCED	NOT REDUCED	NOT REDUCED	NOT REDUCED	NOT REDUCED	NOT REDUCED	NOT REDUCED	NOT REDUCED	NOT REDUCED	NOT REDUCED	NOT REDUCED	.28	.26	.22	.11	.15	.23
2-591	12.	1.23	C	NR													.40	.26	.48	.06	.11	.17
3-592	12.0	1.25	G	4.0													.66	.20	.50	.08	.17	.17
4-593	12.0	1.24	H	5.3													(NR)			(N.R.)		
5-594	12.05	1.25	D	4.5													.20	.92	.36	.08	.25	.23
6-595	12.05	1.25	H	5.1													.58	1.00	.50	.11	.22	.22
7-596	12.05	1.20	A	4.6													(NR)			(N.R.)		
8-597	12.05	1.23	F	4.0													(NR)					
9-598	12.05	1.22	A	3.9													.26	.28	.40	.12	.12	.28
10-599	12.0	1.21	B	6.2													.52	.72	.48	.09	.17	.37
11-600	12.	1.23	E	NR													.50	.54	.36	.08	.12	.17
12-601	12.0	1.24	B	8.0													(NR)			(N.R.)		
13-602	12.	1.23	E	3.2													(NR)					
14-603	12.	1.26	C	5.7													.32	.56	.44	.12	.09	.15
15-604	12.	1.26	E	3.9													.52	.34	.40	.14	.11	.20
16-605	12.	1.25	E	5.8													(NR)			.08	.08	.08
17-606	12.	1.24	B	NR																.17	.25	.51
18-607	12.	1.24	E	5.2																.11	.14	.14
19-608	12.	1.25	E	4.9																.17	.14	.31

STRUCTURAL RESPONSE PROBE

COMPILED BY _____

DATE 1-06 5-7-65
HOUSE 2-S-S

PHASE 2-B					ACCELEROMETERS (g)												DISPLACEMENT (10⁻³ in.)					
2-1-65					Fine Scale	1	2	3	4	5	6	7	8	9	10	11	12	1	2	3	1	2	3
RUN	WT	WIND	LOC	GW																			
20-608	12.	1.24	B	3.7	NOT REDUCED															.08	.05	.09
21-610	12.	1.22	A	4.7		NOT REDUCED														.11	.14	.29
22-611	12.	1.22	F	3.5			NOT REDUCED													.08	.05	.15
23-612	12.	1.22	A	5.5				NOT REDUCED												.20	.20	.68
24-613	12.	1.27	G	4.2					NOT REDUCED											.22	.15	.31
25-614	12.	1.19	C	4.1						NOT REDUCED										.09	.11	.31
26-615	12.05	1.27	G	4.6							NOT REDUCED									.12	.14	.16
27-616	12.05	1.28	C	4.6								NOT REDUCED								.08	.11	.42
28-617	12.05	1.26	G	6.6									NOT REDUCED							.12	.14	.34
29-618	12.05	1.22	H	6.7										NOT REDUCED						.05	.19	.12
30-619	12.1	1.22	D	5.0											NOT REDUCED					.06	.22	.17
31-620	12.	1.26	H	4.7												NOT REDUCED				.06	.19	.14
END																						

STRUCTURAL RESPONSE PROBE

COMPILED BY _____

DATE 1-06 5-7-65
HOUSE 2-S-S

PHASE 2-B					ACCELEROMETERS (g)												DISPLACEMENT 10⁻³ in.					
2-2-65					Fine Scale	1	2	3	4	5	6	7	8	9	10	11	12	1	2	3	1	2	3
RUN	WT	WIND	LOC	GW																			
1-621	12.05	1.27	A	4.1	NOT REDUCED													.32	.10	.42	.09	.08	.19
2-622	11.95	1.27	F	4.8		NOT REDUCED												.24	.24	.60	.11	.08	.09
3-623	12.	1.26	A	11.4			NOT REDUCED											.24	.12	.50	.14	.12	.35
4-624	12.	1.19	E	4.7				NOT REDUCED										.40	.80	.60	.08	.15	.23
5-625	12.	1.23	C	6.3					NOT REDUCED									.44	.52	.32	.06	.11	.12
6-626	12.	1.24	B	4.7						NOT REDUCED								.40	.68	.56	.14	.15	.42
7-627	12.	1.21	C	5.1							NOT REDUCED							.50	.16	.62	.11	.09	.37
8-628	12.	1.25	G	4.6								NOT REDUCED						.76	.80	.60	.11	.20	.16
9-629	12.	1.25	C	4.6									NOT REDUCED					.60	.54	.60	.09	.13	.09
10-630	12.	1.23	D	6.0										NOT REDUCED				.40	.68	.56	.05	.15	.15
11-631	11.95	1.27	H	4.4											NOT REDUCED			.58	.90	.58	.15	.23	.23
12-632	11.95	1.27	D	NR												NOT REDUCED		.28	.96	.24	.06	.17	.19
13-633	12.	1.16	E	3.8														1.28	1.48	1.20	.19	.31	.46
14-634	11.9	1.26	B	4.5														.24	.48	.44	.11	.12	.17
15-635	12.	1.26	F	4.8														(N.R.)			(N.R.)		
16-636	12.	1.21	A	5.6														.66	.72	.66	.11	.08	.10
17-637	12.	1.25	A	4.5														.76	.34	.12	.20	.15	.42
18-638	12.	1.24	F	3.0																	.05	.05	.06
19-639	11.95	1.26	G	3.7																	.11	.11	.19

STRUCTURAL RESPONSE PROGRAM

COMPILED By _____

DATE 10 & 2-7-65
HOUSE 2-S-S

PHASE 2-B — ACCELEROMETERS (g) — DISPLACEMENT (10⁻² in)

2-3-65

RUN	MPH	Wind	DIR	FREE FIELD	1	2	3	4	5	6	7	8	9	10	11	12	D 1	D 2	D 3	1	2	3
20-641	12.	1.24	N	3.4	NOT REDUCED													(NR)		.08	.26	.15
21-642	12.1	1.25	B	3.7		NOT REDUCED														.09	.09	.28
22-643	12.5	1.25	D	4.5			NOT REDUCED													.08	.15	.19
23-643	12.5	1.27	G	3.2				NOT REDUCED												.05	.09	.09
24-644	12.	1.26	H	NR					NOT REDUCED											.08	.20	.11
25-645	11.8	1.23	E	4.6						NOT REDUCED										.14	.17	.25
26-646	12.	1.21	A	4.3							NOT REDUCED									.17	.15	.37
27-647	12.	1.25	E	NR								NOT REDUCED								.09	.23	.55
28-648	12.	1.23	A	4.9									NOT REDUCED							.11	.09	.26
29-649	12.	1.29	B	4.2										NOT REDUCED						.11	.12	.26
30-650	12.	1.28	A	4.6											NOT REDUCED					.20	.14	.25
End																						

STRUCTURAL RESPONSE PROGRAM

COMPILED By _____

DATE 10 & 2-7-65
HOUSE 2-S-S

PHASE 2-B — ACCELEROMETERS (g's) — DISPLACEMENT

2-3-65

RUN	MPH	Wind	DIR	FREE FIELD	1	2	3	4	5	6	7	8	9	10	11	12	D 1	D 2	D 3	1	2	3
1-651	12.	1.23	G	4.9	.052	.104	.091	.141	.397	.062	.209	.186	NR	NR	.307	NR		(NR)			(NR)	
2-652	12.	1.26	C	4.8	.037	.056	.047	.113	.141	.064	.209	.130			.228			.28	.60	.20	.09	.09	.15
3-653	12.	1.24	G	5.0	.048	.102	.102	.141	.224	.077	.255	.18-			.43-			.30	.70	.56	.14	.17	.17
4-654	12.	1.25	C	4.7	.033	.060	.051	.089	.185	.050	.143	.135			.224			.30	.68	.20	.09	.11	.20
5-655	11.5	1.22	G	5.6	.078	.106	.110	.176	.442	.077	.229	.214			.418			.46	.60	.66	(NR)		
6-656	12.	1.25	E	5.7	.046	.071	.071	.103	.175	.035	.255	.124			.224			.50	.66	.36		↓	
7-657	11.95	1.20	B	4.8	.033	.060	.051	.102	.097	.050	.150	.094			.260			.44	.70	.66	.12	.15	.84
8-658	12.	1.25	E	4.5	.054	.099	.087	.127	.255	.039	.208	.152			.222			.46	.66	.30	.08	.11	.15
9-659	12.	1.22	A	6.0	.062	.081	.074	.087	.343	.058	.192	.068			.273				(NR)			(NR)	
10-660	12.	1.25	B	5.1	.052	.071	.063	.113	.107	.044		.285			.269			.46	.70	.66	.14	.16	.22
11-661	12.	1.20	A	5.1	.044	.064	.043	.141	.087	.042	.229	.056			.348			.40	.70	.48	.15	.11	.34
12-662	11.	1.15	A	3.0	.062	.079	.031	.015	.428	.046	.186	.079			.512				(NR)			(NR)	
13-663	12.	1.21	A	5.1	.046	.071	.029	.054	.073	.042	.202	.060			.341			.44	.70	.50	.12	.11	.25
14-664	12.	1.21	A	5.0	.058	.071	.035	.054	.904	.042	.192	.068			.397				(NR)		.08	.11	.15
15-665	12.	1.25	G	4.9	.050	.089	.031	.178	.248	.062	.209	.197			.369						.11	.19	.11
16-666	12.	1.20	A	4.9	.025	.044	.110	.164	.165	.050	.216	.175			.264						.07	.20	.19
17-667	11.95	1.26	C	4.6	.029	.049	.110	.113	.146	.062	.152	.135			.192						.06	.08	.12
18-668	12.	1.21	A	6.0	.037	.054	.102	.169	.097	.046	.179	.169			.196						.08	.14	.12
19-669	12.	1.25	G	5.7	.066	.106	.082	.199	.324	.060	.282	.186	↓	↓	.434	↓			↓		.12	.17	.12

Structural Response Program

Compiled By _____

Date 10 & 2-7-65

House 2-5-5

Phase 2-B

2-3-65

Accelerometers

Displacement (10⁻³ in.)

Run	Ref	Time	Loc	dv	1	2	3	4	5	6	7	8	9	10	11	12	1	2	3	1	2	3
10-670	12.	1.22	A	5.2	.046	.052	.130	.123	.364	.062	.229	.154	NR	NR	.212	NR		(VR)		.08	.22	.17
11-671	11.99	1.36	C	4.9	.028	.067	.087	.127	.131	.054	.136	.124			.234					.03	.1	.15
22-672	12.05	1.24	D	4.3	.046	.078	.102	.132	.027	.073	.216	.169			.175					.03	.17	.12
23-673	11.99	1.30	E	4.9	.050	.074	.066	.103	.089	.0[illegible]	.234	.065			.203					.08	.04	.29
24-674	12.05	1.23	A	3.3	.029	.049	.039	.042	.078	.031	.217	.045			.239					.05	.08	.19
25-675	12.	1.21	E	9.4	.070	.088	.091	.211	.394	.062	NR	.245			.234					.11	.15	.20
26-676	12.	1.23	E	4.6	.058	.021	.024	.042	.3-6	.056	.192	.062			.213					.11	.08	.12
27-677	12.	1.24	B	3.6	.032	.079	.095	.094	.117	.039	.272	.136			.252					.11	.12	.20
28-678	12.	1.25	A	2.1	.025	.014	.020	.042	.584	.039	.176	.051			.171					.06	.03	.17
29-679	12.	1.21	E	3.3	.044	.067	.059	.122	.187	.023	.179	.141			.128					.05	.11	.09
30-680	12.	1.24	E	4.8	.021	.116	.059	.075	.264	.026	.746	.094	↓	↓	.359	↓				.19	.06	.32

Structural Response Program

Compiled By _____

Date 10 & 2-7-65

House 2-5-5

Phase 2-B

2-4-65

Accelerometers

Displacement (10⁻³ in.)

Run	Ref	Time	Loc	dv	1	2	3	4	5	6	7	8	9	10	11	12	1	2	3	1	2	3
1-681	9.7	1.20	C	6.5	.059	.095	.066	.124	.183	.070	.165	.114	NR	NR	.291	NR		(NR)			(NR)	
2-682	9.7	1.18	D	6.3	.054	.092	.076	.171	.356	.044	.215	.194			.219					-	.23	.20
3-683	9.7	1.21	C	7.0	.064	.120	.103	.181	.484	.073	.192	.123			.422					.17	.28	.28
4-684	9.7	1.20	A	6.1	.059	.064	.093	.157	.379	.073	.206	.112			.242					.12	.20	.31
5-685	9.7	1.21	C	6.1	.054	.113	.069	.131	.200	.062	.232	.166			.287					.06	.05	.31
6-686	9.7	1.2-	D	6.4	.062	.092	.106	.200	.292	.029	.311	.124			.249					.15	.14	.15
7	9.7	1.20	A	6.7	.062	.145	.023	.076	.674	.091	.185	.067			.388					.15	.25	.31
8-688	9.91	1.19	C	5.8	.072	.109	.106	.214	.409	.052	.265	.229			.389					.15	.19	.27
9-689	9.7	1.20	A	7.6	.045	.095	.086	.105	.173	.062	.232	.079			.332					.12	.22	.37
10-690	9.7	1.20	C	5.7	.037	.081	.053	.114	.178	.046	.145	.100			.431					.14	.12	.15
11-691	9.7	1.20	C	6.3	.058	.127	.076	.057	.496	.070	.152	.055			.263					.09	.12	.20
12-692	9.7	1.21	C	6.1	.058	.120	.106	.200	.356	.031	NR	.155			.308					.17	.26	.17
13-693	9.7	1.19	C	6.4	.070	.116	.123	.244	.507	.081	.298	.183			.392					.20	.12	.27
14-694	9.7	1.18	A	6.6	.050	.135	.136	.206	.236	.037	.212	.200			.205					.08	.20	.32
15-695	9.7	1.21	C	-	.058	.131	.076	.147	.242	.085	.185	.161			.257					.08	.26	.39
16-696	9.7	1.19	D	6.3	.064	.141	.096	.214	.534	.058	.338	.228			.271			(VR)		.12	.26	.15
17-697	9.7	1.20	C	6.7	.070	.116	.104	.204	.662	.070	.N.	.166			.171					.15	.27	.31
18-698	9.7	1.21	A	5.3	.041	.076	.103	.225	.243	.062	.192	.183			.255					.08	.15	.22
19-699	9.7	1.18	B	6.0	.079	.060	.063	.100	.119	.050	.185	.105	↓	↓	.243	↓				.14	.24	.1

STRUCTURAL RESPONSE PROGRAM

COUPLED
By _____

DATE 30 LS 2-7-65
House 2-S-S

PHASE 2-B
2-4-65

ACCELEROMETERS

DISPLACEMENT (10^{-2} in.)

Run	Mph	Gear	Lane	Free Field	1	2	3	4	5	6	7	8	9	10	11	12	D 1	D 2	D 3	1	2	3
20-720	9.7	1.22	E	6.0	.057	.021	.059	.100	.140	.054	.270	.105	NR	NR	.320	NR		(N.R.)		.14	.14	.25
21-721	9.7	1.22	E	5.2	.070	.120	.080	.190	.294	.054	NR	.172			.844					.11	.19	.15
22-722	9.7	1.22	F	5.3	.070	.120	.017	.076	.267	.067	.240	.067			.287					.14	.08	.09
23-723	9.7	1.20	E	6.2	.062	.128	.042	.111	.183	.067	NR	.122			.443					.17	.17	.35
24-724	9.75	1.20	A	6.4	.054	.095	.036	.091	.327	.054	.152	.100			.405					.14	.15	.39
25-725	9.7	1.20	C	6.2	.033	.092	.023	.162	.145	.067	.199	.144			.266					.05	.12	.31
26-726	9.7	1.20	D	4.3	.045	.085	.026	.224	.129	.031	.202	.233			.194					.05	.20	.28
27-727	9.5	1.21	G	4.3	.045	.078	.080	.147	.246	.[illegible]	.152	.161			.246					.09	.21	.23
28-728	9.7	1.20	H	4.9	.045	.071	.116	.185	.[illegible]		.212	.172			.316					.11	.20	.26
29-729	9.7	1.20	G	6.7	.062	.102	.093	.171	.[illegible]		.270	.172			.257					.11	.15	.15
30-730	9.7	1.19	H	5.5	.037	.060	.120	.162	.10[illegible]		.062	.172	.133		.325					.09	.25	.20
End																						

STRUCTURAL RESPONSE PROGRAM

COUPLED
By _____

DATE 30 LS 2-7-65
House 2-S-S

PHASE 2-B
2-5-65

ACCELEROMETERS (9)

DISPLACEMENT (10^{-2} in.)

Run	Mph	Gear	Lane	Free Field	1	2	3	4	5	6	7	8	9	10	11	12	D 1	D 2	D 3	1	2	3
1-711	B.	1.22	E	9.7	.070	.068	.109	.254	.325	.080	NR	.274			.395			(N.A.)			(N.R.)	
2-712	B.	1.19	F	—	.042	.059	.012	.042	.083	.026	.060	.067			.224							
3-713	B.	1.22	E	12.1	.070	.122	.062	.215	.258	.026	NR	.199			.611		.60	1.00	.90	.35	.37	.85
4-714	B.	1.21	A	9.0	.066	.118	.062	.145	.218	.066		.148			.727		.32	.48	.92	.22	.29	.28
5-715	B.	1.21	E	9.7	.074	.078	.062	.352	.436	.084		.301			.478		.96	.92	.90	.17	.25	.28
6-716	B.	1.19	F	12.5	.098	.295	.052	.[illegible]	.518	.099		.136			.698		1.24	1.36	1.12	.19	.28	.39
7-717	B.	1.20	G	10.3	.098	.226	.164	.295	.669	.044		.321			.748		1.10	1.20	1.16	.29	.34	.46
8-718	B.	1.20	H	9.4	.074	.187	.152	.348	.465	.118		.238			.519		1.64	1.50	1.56	.23	.42	.48
9-719	B.	1.20	C	9.4	.057	.206	.089	.197	.394	.091		.216			.598		.80	1.18	.76	.19	.28	.57
10-720	B.	1.20	D	9.5	.066	.197	.122	.281	.562	.052		.390			.623		.64	.68	.80	.15	.34	.49
11-721	B.	1.20	G	9.9	.090	.212	.169	.299	.577	.095		.335			.752		1.06	1.34	1.24	.26	.39	.40
12-722	B.	1.21	H	11.1	.082	.157	.109	.267	.375	.116		.233			.466		.98	1.60	1.54	.23	.40	.54
13-723	7.95	1.19	A	10.7	.098	.177	.023	.134	.140	.044		.136			.686		.68	.56	.60	.28	.31	.82
14-724	9.7	1.21	B	9.2	.090	.187	.116	.276	.207	.091		.187			.724		.64	.82	1.00	.31	.32	1.08
15-725	B.	1.22	E	10.5	.114	.261	.042	.112	.189	.095		.102			.594		1.24	.[illegible]	1.66	.14	.17	.22
16-726	B.	1.21	E	10.6	.106	.302	.109	.309	.434	.087		.274			.581			(N.A.)			(N.R.)	
17-727	7.95	1.20	A	8.3	.061	.138	.[illegible]	.112	.131	.065		.091			.546		.52	.52	.[illegible]	.25	.19	.57
18-728	B.	1.22	B	10.0	.086	.157	.112	.286	.228	.[illegible]		.116			NR			(N.A.)		.42	.39	1.34
19-729	B.	1.20	C	8.9	.070	.162	.102	.191	.285	.087		.131			.392			(N.A.)		.17	.28	.54

Structural Response Program

Compiled By _____

Daniel-Jones 2-7-65

House 2-5-5

Phase 2-N

2-5-65

Accelerometers (g)

Displacement (10⁻³ in)

Pin	Elev.	Line	Free Field	1	2	3	4	5	6	7	8	9	10	11	12	Displacement 1	2	3	1	2	3
20-734	B.	120	H	7.0	.437	.153	.127	.268	.125	.048	.311	.222		.302					.06	.31	.31
21-735	B.	120	G	—	.684	.224	.116	.204	.427	.084	.462	.227		.561					.25	.29	.39
22-736	B.	120	F	9.4	.866	.132	.116	.226	.424	.129	N.R.	.227		.448					.26	.43	.63
23-737	B.	120	E	11.3	.886	.218	.139	.248	.228	.091		.227		.538					.25	.26	.68
24-734	B.	120	D	7.7	.857	.182	.132	.286	.561	.068		.315		.349					.09	.34	.26
25-735	B.	119	F	10.1	.886	.290	.238	.122	.512	.103		.102		.507					.19	.15	.39
26-736	B.	119	E	9.2	.119	.191	.139	.251	.584	.063		.261		.399					.14	.26	.40
27-737	B.	120	A	7.6	.076	.143	.063	.103	.114	.057		.125		.424					.19	.25	.59
28-738	B.	120	E	7.4	.084	.152	.029	.055	.174	.072		.148		.428					.23	.23	.57
29-739	B.	119	E	9.4	.060	.124	.122	.246	.658	.060	Y	.272		.391					.22	.39	.71
30-740	B.	120	A	8.8	.070	.182	.061	.112	.470	.091	.212	.136		.424					.15	.17	.20
End																					

Structural Response Program

Compiled By _____

Daniel-Jones 2-7-65

House 2-5-5

Phase 2-B

2-6-65

Accelerometers (g)

Displacement (10⁻³ in)

Pin	Elev.	Line	Free Field	1	2	3	4	5	6	7	8	9	10	11	12	Displacement 1	2	3	1	2	3
1-761	22	120	G	11.2			(NOT RECORDED)									(N.A.)			(N.A.)		
2-762	22	120	H	8.9												(N.A.)			↓		
3-763	23	123	C	11.3												.82	.94	.94	.39	.45	1.08
4-764	23	121	D	10.9												.46	1.68	.72	.12	.31	.37
5-765	23	120	G	10.8												1.18	1.68	1.40	.34	.37	.77
6-766	23	122	H	12.5												.96	1.34	1.64	.34	.40	.65
7-767	23	121	C	11.8												.40	1.06	.70	.22	.31	.54
8-768	23	120	D	9.7												.54	1.44	.80	.09	.29	.43
9-769	23	119	B	12.0												.50	1.20	.94	.31	.34	.66
10-750	22	119	E	12.3												1.40	.40	1.12	.20	.23	.20
11-751	23	119	G	10.9												.92	1.40	.94	.31	.26	.82
12-752	23	120	A	10.7												(N.A.)			.46	.31	1.00
13-753	23	120	B	9.7															.28	.55	.85
14-754	23	118	E	12.4															.20	.25	.22
15-755	23	119	E	10.5															.15	.31	.23
16-756	23	120	A	11.1															.43	.31	1.09
17-757	23	120	C	11.3															.23	.37	.77
18-758	23	119	D	12.2															.15	.34	.32
19-759	23	120	G	12.3															.38	.54	.71

STRUCTURAL RESPONSE PROFILE

COMPILED BY _____

DATE 1-30 LS 2-7-65

HOUSE 2-1-J

PHASE 2-B					ACCELEROMETERS (g)												DISPLACEMENT (10⁻³ in.)											
2-6-65					From Field	1	2	3	4	5	6	7	8	9	10	11	12	1	2	3	1	2	3						
RUN	A.F.	Hz	LOC	AM														(NR)											
20-264	7.3	1.19	M	8.7																	.20	.34	.13						
21-265	7.3	1.20	C	14.4																	.28	.26	.05						
22-263	7.2	1.19	D	10.1																	.12	.25	.31						
23-76	7.3	1.20	G	11.9																	.28	.39	.54						
24-268	7.3	1.19	M	11.7																	.26	.39	.65						
25-269	7.6	1.20	M	9.5																	.14	.12	.19						
26-266	7.3	1.20	G	–																	.17	.31	.49						
27-267	7.25	1.20	A	10.8																	.42	.31	.96						
28-268	7.3	1.20	B	–																	.35	.31	.85						
29-269	7.3	1.20	M	10.4																	.15	.15	.25						
30-270	7.25	1.20	G	11.4																	.23	.35	.54						
End																													

STRUCTURAL RESPONSE PROFILE

COMPILED BY _____

DATE 1-30 LS 2-7-65

HOUSE 2-1-J

PHASE 2-B					ACCELEROMETERS (g)												DISPLACEMENT (10⁻³ in.)											
2-7-65					From Field	1	2	3	4	5	6	7	8	9	10	11	12	1	2	3	1	2	3						
RUN	A.F.	Hz	LOC	AM														(NR)											
1-271	6.8	1.20	M	NR																	(NR)								
2-272	6.8	1.19	M																		↓								
6-273	6.8	1.20	M	15.2																	.22	.20	.29						
4-274	6.8	1.19	M	15.0																	.20	.15	.29						
5-275	6.8	1.20	M	11.6																	.20	.17	.20						
6-276	6.8	1.19	M	9.3																	.18	.12	.22						
7-277	6.8	1.20	M	12.6																	.17	.17	.37						
8-278	6.85	1.20	M	11.2																	.17	.14	.20						
9-279	6.6	1.19	A	12.9																	.54	.60	1.46						
10-280	6.75	1.19	A	14.3																	.39	.32	1.08						
11-281	6.8	1.20	M	13.2																	.17	.15	.26						
12-282	6.8	1.19	M	14.1																	.23	.22	.26						
13-283	6.8	1.20	A	10.3																	.31	.35	1.17						
14-284	6.75	1.19	A	13.7																	.62	.31	1.54						
15-285	6.7	1.20	M	14.3																	(N.R.)								
16-286	6.8	1.20	M	11.9																	.15	.19	.37						
17-287	6.4	1.19	A	14.5																	–	.68	1.85						
18-288	6.75	1.18	A	12.7																	–	.46	1.53						
19-289	6.8	1.20	M	13.7																	.14	.15	.22						

Structural Response Program

Compiled By ______

Date: 30 & 2-7-65

House 2-5-5

Phase 2-B					Accelerometers (g)												Displacement (10⁻³ in)					
2-7-65				Ave. Peak	1	2	3	4	5	6	7	8	9	10	11	12	1	2	3	1	2	3
Run	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]
20-790	68	1.20	A	163													(NK)			.70	.26	.49
21-791	68	1.20	A	114																.28	.22	.11
22-792	67.5	1.20	A	128																–	.77	1.93
End																						

STRUCTURAL RESPONSE PROFILE

COMPILED BY _____

DATE 12-9-66 / 12-10-66

HOUSE PE-6

PHASE 2-A 12-9-66				DISPLACEMENT					
				FREE FIELD	7	8	9	10
PIN	N.S.	Horiz.	Vert.					
1-416	7.0	1.2	A	6.1		25	16	1.35
2-417	7.0	1.2	F	7.2		37	18	1.70
3-418	7.0	1.2	A	8.5				1.39
4-419	6.9	1.2	C	9.6		48		1.58
5-420	7.0	1.2	F	7.5		162	144	1.60
6-421	7.0	1.2	D	9.7		52	20	.19
7-422	7.0	1.2	A	9.0		1.62	1.18	1.27
8-423	7.0	1.2	D	8.6		1.31	1.08	1.10
9-424	7.0	1.25	E	10.5		36	16	1.33
10-425	6.9	1.22	A	10.0		116	.96	.98
11-426	7.0	1.22	E	.71		.46	.29	2.48
12-427	7.0	1.15	F	9.1		.58	.32	1.91
13-428	7.1	1.20	A	11.7		.80	.50	1.28
14-429	7.2	1.2	F	7.9		1.67	1.62	1.28
15-430	7.0	1.2	C	10.7		1.18	.71	1.20
16-431	7.0	1.2	D	13.5		.26	.22	1.90
17-432	7.0	1.19	C	10.6		.52	.29	1.50
18-433	7.0	1.2	A	8.1		.29	.12	1.61
19-434	7	1.21	F	8.0				

STRUCTURAL RESPONSE PROFILE

COMPILED BY _____

DATE 12-9-66 / 12-10-66

HOUSE PE-6

PHASE 2-A 12-9-66				DISPLACEMENT					
				FREE FIELD	7	8	9	10
PIN	N.S.	Horiz.	Vert.					
20-435	7.0	1.2	A	8.1				
21-436	7.0	1.2	F	10.0				
22-437	7.0	1.17	D	7.7				
23-438	7.0	1.18	E	10.8				

Structural Response Rapoll

Compiled By _____

Date 12-9-64 & 12-16-64
House PF-6

Phase 2-A				Displacement				
12-10-64				From Cold	7	8	9	10
Run	Alt	Level	Var	Amb				
1-445	6.5	13	A					
2-446	6.5	12	F					
3-445	6.9	115	C					
4-446	6.5	12	F					
5-447	6.5	118	C					
6-448	6.5	114	D					
7-449	6.5	119	A					
8-450	6.9	118	D					
9-451	6.5	12	E					
10-452	6.5	111	A					
11-453	6.5	111	E					
12-454	6.5	111	F					
13-455	6.5	11	A					
14-456	6.5	11	F					
15-457	6.5	116	C					
16-458	6.5	110	D					
17-459	6.9	115	C					
18-460	8.0	12	A					
19-461	6.5	11	F					

Structural Response Rapoll

Compiled By _____

Date 12-9-64 & 12-16-64
House PF-6

Phase 2-A				Displacement				
12-10-64				From Cold	7	8	9	10
Run	Alt	Level	Var	Amb				
20-462	6.9	111	A					
21-463	6.5	11	E					
22-464	6.5	11	D					
23-465	6.5	11	E					

Structural Response Program

Compiled By ______

Date 12-9-68 / 12-15-68

House PE-1

Phase 2-A 12-14-6?				Displacement				
Run	W.E	Chg	Loc	Free Field	7	8	9	10
1-556	12	128	A		70	.21	09	78
2-557	12	128	F		91	.34	18	60
3-558	119	128	A		.72	.21	09	76
4-559	12	1.25	B		48	.57	.27	64
5-560	12	127	E		65	57	46	80
6-561	12	128	B		55	72	.39	76
7-562	12	1.3	C		115	48	18	.72
8-563	12	1.3	F	9c	96	32	.05	56
9-564	12	13	C	2.3	—	—	—	—
10-565	12	125	D	4.0	55	95	20	.66
11-566	11.8	125	H	3.0	.48	82	44	.26
12-567	11.3	125	D	3.1	.48	.8c	51	60
13-568	12.1	1.3	E	25	—	—	—	—
14-569	12	13	B	36	—	—	—	—
15-570	12	13	E	3.4	—	—	—	—
16-571	12	124	F	42	1.05	32		70
17-572	12	124	A	3.0	.72	14	.15	60
18-573	12	125	F	3.3	.89	25	07	.60
19-574	12	13	H	31	91	72	.51	40

Structural Response Program

Compiled By ______

Date 12-9-68 / 12-15-68

House PE-1

Phase 2-A 12-14-69				Displacement				
Run	W.E	Chg	Loc	Free Field	7	8	9	10
20-575	12	128	D	32	43	76	46	60
21-576	12	1.3	H	32	34	72	44	54
22-577	12	13	A	33	.96	.19	09	78
23-578	12	13	F	3.2	.96	3?		96
24-579	12	1.3	A	19	70	.19	05	.7?
25-580	11.5	122	B	36	.55	57	25	80
26-581	12	125	E	31	.53	.55	.40	80
27-582	12	13	B	36	6?	.57	29	90
28-583	12	124	C	28	48	44	21	.56
29-584	12	125	F	32	103	.36	12	70
30-585	12	126	C	.29	84	30	12	52
31-586	118	126	D	31	[illegible]	70	51	.66
32-587	118	126	H	3.4	48	82	51	.56
33-588	12	126	D	3.1	48	72	[illegible]	.60
34-589	12	1.26	E	2.9	50	.57	.41	.7?
35-590	12	127	B	2.9	.48	.57	25	.76
36-591	12	130	E	3.0	.67	.57	44	.80

Structural Response Program

Compiled By ______

Date 12-9-69 12-15-69
House PE-6

Phase 2-A 12-15-69				Displacement				
				Free Field	7	8	9	10
Run	M.C.		Loc.	AV.				
1-592	12	115	F		.78	.30	0.2	.31
2-593	12	117	A		.55	.36	.12	.95
3-594	11.5	150	F		1.00	.36	.09	.63
4-595	10.5	1.30	D		.75	.95	.74	1.30
5-596	10.5	130	H		.60	.75	1.04	.99
6-597	10.5	130	D		.68	.45	.47	.63
7-598	10.5	121	A	4.5	.75	.38	.23	1.05
8-599	10.5	123	F	3.0	1.07	.36	.32	.67
9-600	10.5	126	A	3.6	.90	.17	.23	1.03
10-601	12	122	B	2.8	.50	.75	.27	.80
11-602	10.5	120	E	3.6	.83	.67	.58	1.05
12-603	10.5	120	B	4.	.73	.91	.46	.91
13-604	10.5	120	C	3.6	1.00	.60	.18	.62
14-605	10.5	120	F	3.7	1.00	.34	.21	.67
15-606	10.5	121	C	4.2	1.00	.38	.21	.67
16-607	10.5	115	D	4.2	.65	.75	.53	.59
17-608	10.5	116	H	[illegible]	.35	.95	.46	.48
18-609	10.5	126	D	4.0	.53	.86	.51	.80
19-610	10.5	127	E		–	–	–	–

Structural Response Program

Compiled By ______

Date 12-9-69 12-15-69
House EE-6

Phase 2-A 12-15-69				Displacement				
				Free Field	7	8	9	10
Run	M.C.		Loc.	AV.				
20-611	10.5	125	B	4.5	–	–	–	–
21-612	10.5	125	E	4.3	–	–	–	–
22-613	10.5	125	F	3.7	1.05	.39	.13	.80
23-614	10.5	1.20	A	5.0	.75	.38	.23	.97
24-615	10.5	121	F	3.4	1.18	.36	.12	.80

Structural Response Program

Compiled By ______

Date [illegible]
House PF-6

Phase 2-A 1-15-65					Displacement (10⁻² in)					
Run	A.F.	[illegible]	Vec	AK (Freq.)	7	8	9	10	11	12
1-1	12	1.2	A		-	.143	.015	.078	-	-
2-2	12.	1.25	E		-	.078	.117	.268	-	-
3-3	21	1.26	A		-	.143	.015	.242	-	-
4-4	12.	1.25	[illegible]		.027	.143	.235	.134	1.051	.354
5-5	11.5	1.25	5		.041	.143	.250	.293	1.278	.923
6-6	12.	1.26	C		.027	.130	.176	.183	1.231	.308
7-7	12.	1.26	C		.068	.117	.271	.268	1.102	.600
8-8	12.	1.26	G		.082	.026	.309	.298	1.029	1.078
9-9	12.	1.28	C		.027	.039	.279	.244	-	.385
10-10	12.	1.11	D		.082	.117	.368	.207	-	.462
11-11	12	1.23	H		.027	.104	.353	.256	-	.385
12-12	12.	1.20	D		.109	.117	.412	.244	-	.432
13-13	11.9	1.21	E	57	.041	.130	.279	.232	1.590	1.000
14-14	11.9	1.24	F	66	.027	.091	.162	.122	1.196	.276
15-15	12	1.26	E	85	.027	.117	.176	.244	1.208	.968
16-16	12.	1.26	F	6.1	.010	.091	.088	.244	.511	1.201
17-17	12	1.25	A	56	.014	.130	.029	.232	.289	.462
18-18	12	1.25	F	67	.027	.065	.074	.220	.383	1.079
19-19	12.	1.26	G	50	.027	.013	.323	.342	1.509	.570

Structural Response Program

Compiled By ______

Date [illegible]
House PF-6

Phase 2-B 1-15-65					Displacement					
Run	A.F.	[illegible]	Vec	AK	7	8	9	10	11	12
20-20	12	1.25	C	6.3	.027	.091	.279	.244	-	.462
21-21	12.	1.26	G	6.1	.041	.026	.368	.293	-	1.386
22-22	11.5	1.26	H	6.3	.027	.104	.309	.329	2.326	.308
23-23	11.9	1.26	D	5.6	.109	.091	.397	.159	-	.359
24-24	12.	1.28	H	9.3	.123	.234	.426	.317	-	.524
25-25	12.	1.25	A	5.1	.014	.104	.059	.147	1.825	.462
26-26	12.5	1.25	E	5.0	.041	.104	.029	.220	-	1.370
27-27	11.8	1.26	A	8.1	.014	.117	.074	.159	-	.539
28-28	12.	1.25	C	5.5	.027	.104	.059	.110	-	.369
29-29	12.	1.2	C	6.5	.014	.078	.147	.159	-	.695
30-30	12.	1.23	B							
End.										

Structural Response Program

Compiled By ______

Date [illegible]
House PF-6

Phase 2-A				Displacement (10^{-2} m)							
1-16-65				Free Field	7	8	9	10	11	12	
Run	Wt	Horiz	Vec	AV							
1-31	11.5	1.31	C		-	-	-	-	-	-	
2-32	11.8	1.33	G	6.1	.129	.079	.229	.113	-	1.365	
3-33	11.5	1.36	C	6.0	.029	.157	.158	.227	-	.626	
4-34	12.	1.35	D	6.0	.129	.100	.401	.151	-	.589	
5-35	12.	1.25	H	6.0	.086	.157	.458	.202	-	.605	
6-36	12.	1.26	D	6.5	.143	.121	.329	.126	-	.481	
7-37	11.7	1.20	E	6.5	.272	.262	.286	.227	-	.970	
8-38	12.	1.31	B	5.6	.029	.144	.272	.126	-	1.079	
9-39	12.	1.31	E	6.2	.115	.262	.329	.240	-	1.085	
10-40	11.7	1.24	F	6.8	.029	.262	.143	.391	-	1.659	
11-41	11.6	1.26	A	9.0	.129	.236	.143	.252	-	.837	
12-42	12.	1.26	F	5.6	.014	.262	.129	.366	-	2.899	
13-43	12.	1.28	G	7.6	.086	.121	.915	.403	-	1.079	
14-44	12.	1.37	[illegible]	7.3	.029	.121	.286	.240	-	.698	
15-45	25.	1.35	F	0.0	[illegible]	[illegible]	[illegible]	[illegible]	NK	[illegible]	13-58
16-46	25.	1.35	E	5.1	[illegible]	[illegible]	[illegible]	[illegible]	NK	[illegible]	13-54
17-47	25.	1.35	F	9.5	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]
18-48	25.	1.35	F	4.0	[illegible]	[illegible]	[illegible]	[illegible]	NK	[illegible]	13-58
19-49	25.	1.35	F	2.9	[illegible]	[illegible]	[illegible]	[illegible]	NK	[illegible]	[illegible]

Structural Response Program

Compiled By ______

Date [illegible]
House PF-6

Phase 2-A				Displacement (10^{-2} m)						
1-16-65				Free Field	7	8	9	10	11	12
Run	Wt	Horiz	Vec	AV						
20-50	12.	1.26	H	5.5	.029	.105	.286	.139	-	.465
21-51	11.9	1.33	D	8.7	.129	.116	.315	.113	-	.481
22-52	12.	1.36	H	0.6	.029	.052	.172	.105	-	.391
23-53	12.	1.33	A	5.5	.014	.121	.057	.126	-	.620
24-54	12.	1.26	E	6.0	.044	.157	.086	.328	-	1.625
25-55	12.	1.24	A	8.6	.010	.116	.129	.126	-	.620
26-56	12.	1.26	[illegible]	5.0	.014	.144	.143	.139	-	.791
27-57	12.	1.37	C	8.3	.125	.209	.272	.225	-	1.085
28-58	12.	[illegible]	[illegible]	5.8	.014	.183	.157	.189	-	.946
29-59	12.	1.27	C	6.2	.029	.121	[illegible]	.256	-	.714
30-60	12.	[illegible]	[illegible]	5.8	.100	.116	.353	.325	-	1.085
31-61	12.	1.30	C	6.2	.014	.121	.219	.202	-	.467
32-62	12.	1.25	D	6.0	.115	.092	.315	.139	-	.543
33-63	11.8	1.37	[illegible]	6.6	.029	.116	.258	.176	-	1.805
34-64	11.6	1.36	[illegible]	7.6	.143	.105	.315	.240	-	.651
End										

STRUCTURAL RESPONSE PROGRAM

COMPILED BY _____ DATE: 1-17-65

HOUSE PF-6

PHASE 2-A				DISPLACEMENT. (10^{-2} in.)						
1-17-65				FREE FIELD	7	8	9	10	11	12
RUN	R.F.	HYPO	VEL.	AVE						
1-65	11.9	1.20	E	4.7	-	.210	.301	232	1.022	789
2-66	12.	1.19	E	4.8	-	.262	.286	142	1.999	672
3-67	12.3	1.20	E	6.0	-	.236	.226	.245	.976	.584
4-68	12.	1.22	F	7.0	-	.289	.127	.374	.702	.779
5-69	12.	1.18	A	7.6		.289	.029	.245	1.460	.438
6-70	12.	1.23	F	6.9		.236	.127	.258	.759	1.139
7-71	11.9	1.26	G	8.1		.066	.301	.142	1.252	1.008
8-72	12.	1.26	C	6.6		.131	.286	.129	1.099	.730
9-73	12.	1.24	G	6.8		.026	.429	.236	.701	.541
10-74	11.9	1.25	H	7.5		.131	.043	.245	1.694	.526
11-75	12.	1.22	D	5.6		.079	.429	.116	1.635	.307
12-76	12.	1.24	H	5.8		.118	.415	.168	2.681	.278
13-77	11.8	1.21	A	5.3		.157	.100	.206	1.621	.669
14-78	11.9	1.20	E	7.3		.118	.043	.206	1.129	1.193
15-79	12.	1.23	A	4.8		.131	.029	.142	1.549	.345
16-80	12.	1.24	B	5.2		.170	.258	.129	1.146	.380
17-81	12.	1.24	E	7.0		.157	.172	.190	.468	.702
18-82	12.	1.2.	B	6.8		.184	.243	.121	1.650	.423
19-83	12.	1.21	C	7.8		.105	.286	.129	1.578	.619

STRUCTURAL RESPONSE PROGRAM

COMPILED BY _____ DATE: 1-17-65

HOUSE PF-6

PHASE 2-A				DISPLACEMENT. (10^{-2} in.)						
1-17-65				FREE FIELD	7	8	9	10	11	12
RUN	R.F.	HYPO	VEL.	AVE						
20-84	12.	1.24	G	5.7	-	.066	.429	.245	1.241	.702
21-85	11.9	1.24	C	6.6	-	.105	.286	.129	1.201	.609
22-86	11.9	1.21	D	3.2		.039	.272	.026	.891	.175
23-87	12.0	1.24	H	5.2		.131	.529	.362	.292	.423
24-88	12.0	1.24	D	8.5		.066	.015	.129	1.860	.423
25-89	11.9	1.25	E	5.5		.236	.301	.245	1.270	.876
26-90	11.7	1.25	B	6.2		.197	.158	.142	1.373	.482
27-91	12.	1.26	C	6.9		.170	.286	.258	.978	.457
28-92	12.	1.20	E	6.9		.223	.127	.374	.906	1.300
29-93	12.	1.20	A	8.6		.157	.043	.155	2.335	.488
30-94	12.	1.20	E	7.1		.104	.072	.258	.891	1.339
End										

STRUCTURAL RESPONSE PROFILE

COMPILED BY _____

DATE: 1-18-65
HOUSE PE-6

PHASE 2-B — DISPLACEMENT (10⁻² in)

1-18-65

PIN	REF	Horiz	Vert	PEAK FREE FIELD	7	8	9	10	11	12
1-95	12.	1.24	G	5.3	.076	.057	.260	.195	.145	.616
2-96	12.	1.28	C	5.6	.130	.128	.168	.139	2.142	.916
3-97	12.2	1.25	G	2.9	—	—	—	—	—	—
4-98	12.	1.35	H	6.6	.005	.099	.291	.125	1.730	.978
5-99	12.	1.33	D	5.6						
6-100	11.9	1.35	H	5.1						
7-101	12.	1.34	A	5.6						
8-102	12.1	1.32	F	5.8	.005	.128	.138	.195	.903	1.069
9-103	12.	1.25	A	6.3	.050	.102	.122	.139	1.836	.329
10-104	11.9	1.21	B	4.8	.030	.128	.137	.125	2.197	.324
11-105	12.	1.23	F	5.1	.091	.179	.138	.139	9.18	.720
12-106	12.	1.25	B	5.3	.030	.102	.153	.125	2.295	.370
13-107	12.	1.25	C	5.6	.030	.057	.245	.167	2.295	.359
14-108	12.	1.35	G	4.5	.091	.005	.306	.195	1.836	6.m
15-109	12.	1.28	C	6.7	.030	.071	.168	.195	1.699	.978
16-110	12.	1.26	H	5.1	.060	.128	.306	.139	1.990	.997
17-111	12.	1.25	D	5.9	.167	.109	.306	.195	2.06	.932
18-112	12.	1.29	H	5.1	.106	.128	.666	.250	2.154	.693
19-113	11.8	1.30	E	4.5	.176	.162	.163	.264	1.020	.796

STRUCTURAL RESPONSE PROFILE

COMPILED BY _____

DATE: 1-18-65
HOUSE PE-6

PHASE 2-B — DISPLACEMENT (10⁻² in)

1-18-65

PIN	REF	Horiz	Vert	PEAK FREE FIELD	7	8	9	10	11	12
20-114	11.7	1.30	B	6.6	.005	.170	.153	.153	2.02	.770
21-115	12.	1.20	E	8.7	.060	.227	.153	.306	1.255	.926
22-116	12.	1.31	F	5.2	.030	.102	.107	.278	.597	.460
23-117	12.1	1.25	A	6.6	.015	.156	.077	.167	1.850	.586
24-118	12.	1.25	F	6.2	.045	.261	.199	.417	1.070	.468
25-119	12.	1.28	G	6.6	.121	.071	.367	.285	.630	.862
26-120	11.9	1.34	C	6.2	.060	.162	.291	.167	2.002	.770
27-121	12.1	1.31	G	5.1	.136	.063	.291	.131	1.101	.432
28-122	11.8	1.32	D	8.0	.136	.128	.337	.264	1.516	.600
29-123	12.	1.21	H	5.7	.121	.128	.337	.125	2.002	.368
30-124	12.	1.24	A	6.2	.136	.099	.306	.139	1.684	.962
End										

STRUCTURAL RESPONSE PROGRAM

COMPILED By ______

DATE [illegible]
HOUSE PF-6

PHASE 2-B				DISPLACEMENT (10⁻² in)							
Run	Act.	Head	Vic	AV	7	8	9	10	11	12	
1-125	12.	1.25	E	6.6	.043	.157	.112	.230	.550	.871	
2-126	25.0	1.62	F	2.9	.016	.013	.016	.092	.170	.280	
3-127	20.	1.45	A	2.2		.013	.016	.023	.031	.167	
4-128	12.	1.26	B	6.1	.028	.109	.154	.115	.1965	.462	
5-129	12.	1.25	E	4.8	.057	.157	.160	.230	.917	.240	
6-130	11.	1.25	[illegible]	5.2	.010	.144	.140	.115	.1979	.477	
7-131	12.	1.25	C	6.2	.057	.131	.210	.232	.2097	.672	
8-132	12.	1.26	G	6.0	.043	.118	.167	.232	.2290	.810	
9-133	12.	1.29	C	8.1							
10-134	12.4	1.25	D	6.9	.128	.118	.294	.173	.1965	.616	
11-135	11.9	1.27	H	5.0	.015	.118	.308	.115	.1441	.620	
12-136	11.8	1.24	D	6.5	.113	.131	.280	.173	.2019	.672	
13-137	25.	1.37	E	5.7	[illegible]	[illegible]	.140	.316	1.024	.714	12:58
14-138	25.	1.29	F	3.9	.036	[illegible]	.126	.184	[illegible]	.6[illegible]	12:58
15-139	11.6	1.24	G	10.8	.094	.118	.182	.253	.1245	.1120	
16-140	25.	1.25	E	3.7	[illegible]	[illegible]	[illegible]	.218	[illegible]	[illegible]	12:[illegible]
17-141	12.	1.25	B	5.1	.028	.131	.154	.115	[illegible]	.434	
18-142	25.	1.35	E	3.1	.028	[illegible]	.12[illegible]	[illegible]	[illegible]	.552	[illegible]
19-143	12.	1.22	[illegible]	6.0	[illegible]	.183	.150	.230	.866	.990	

STRUCTURAL RESPONSE PROGRAM

COMPILED By ______

DATE [illegible]
HOUSE PF-6

PHASE 2-B				DISPLACEMENT (10⁻² in)							
Run	Act.	Head	Vic	AV	7	8	9	10	11	12	
20-144	25.	1.35	E	3.5	[illegible]	[illegible]	.126	.330	1.04[illegible]	.702	12:56
21-145	30.	1.40	F	2.0	.016	.013	.016	.066	.328	.280	
22-146	30.	1.3	F	1.6	.016	.026	.010	.066	.310	.620	
23-147	30.	1.4	E	2.2	-	.013	.010	.035	.275	.268	
24-148	12.	1.26	A	5.6	.010	.100	.056	.115	.1441	.546	
25-149	11.9	1.21	[illegible]	5.1							
26-150	12.1	1.21	[illegible]	5.9							
27-151	12.7	1.22	[illegible]	6.7	.156	.105	.626	.330	.1611	.196	
28-152	12.	1.27	H	6.9	.028	.204	.268	.109	.1312	.210	
29-153	12.	1.25	D	6.6	.202	.118	.280	.173	.2051	.687	
30-154	12.	1.22	H	5.6	.057	.118	.290	.115	.1965	.342	
31-155	12.	1.20	A	5.7	.010	.131	.028	.12	.1965	.607	
32-156	12.	1.25	E	7.6	.185	.131	.140	.207	.721	.1331	
33-157	12.	1.25	A	6.4	.010	.157	.028	.173	.1335	.465	
End											

STRUCTURAL RESPONSE PROFILE

COMPILED BY _____

DATE 8/31/1965

HOUSE DE-6

PHASE 2-A — 1-20-65 — DISPLACEMENT (10⁻² in)

RUN	ELEV	AZIM	VEC	PEAK ACC	7	8	9	10	11	12
1-176	12.	1.28	D	5.2	.110	.269	.227	.125	.2826	.220
2-177	12.	1.28	C	6.0	.070	.262	.230	.375	.2311	.880
3-180	12.	1.28	G	7.4	.252	.140	.626	.262	.2118	.250
4-181	12.	1.28	—	5.3	.028	.196	.284	.187	.1876	.560
5-182	28.	1.44	E	2.0	.015	.076	.019	.560	.282	.241
[illegible]	30.	1.28	F	1.6	.014	.013	.010	.013	.003	.007
[illegible]	46.	1.44	F	0.9	.110	.237	.014	.007	.353	.420
8-185	11.9	1.28	—	6.5	.042	.105	.238	.125	.1470	.630
[illegible]	[illegible]	[illegible]	[illegible]	7.8	.042	.168	.235	.185	.1061	.229
[illegible]	12.	1.28	—	6.2	.126	.140	.526	.225	.1677	.516
11-188	11.9	1.28	—	12.3	.166	.262	.376	.300	.1831	.1245
[illegible]	12.	1.28	—	8.1	.098	.236	.199	.200	.1481	.952
13-190	11.8	1.28	E	4.1	.056	.121	.299	.125	.714	.476
14-191	12.	1.28	E	4.2	.111	.222	.142	.375	.84[illegible]	.669
[illegible]	12.	1.28	A	3.5	.042	.[illegible]6	.142	.250	.2539	.560
16-193	11.7	1.28	E	4.2	.098	.236	.142	.375	.2[illegible]	.210
17-194	12.	1.28	G	5.5	.140	.131	.369	.375	.[illegible]	.350
18-195	12.	1.28	G	5.6	.140	.131	.112	.250	.1881	.[illegible]
[illegible]	[illegible]	[illegible]	G	7.8	.140	.097	.126	.375	.210	.[illegible]

STRUCTURAL RESPONSE PROFILE

COMPILED BY _____

DATE 8/31/1965

HOUSE DE-6

PHASE 2-A — 1-21-65 — DISPLACEMENT (10⁻² in)

RUN	ELEV	AZIM	VEC	PEAK ACC	7	8	9	10	11	12
1-177	12.	1.30	H	5.2	.112	.236	.620	.129	.2125	.290
2-178	12.	1.28	D	6.1	.112	.131	.299	.129	.1782	.653
3-179	12.	1.28	H	6.8	.126	.238	.620	.248	.1230	.551
4-180	12.	1.28	H	6.7	.056	.249	.098	.248	.2395	.580
5-181	12.	1.31	E	6.6	.098	.275	.196	.372	.1044	.232
6-182	12.	1.30	D	6.6	.028	.160	.070	.236	.2182	.551
7-183	12.	1.30	B	5.3	.028	.236	.266	.186	.993	.812
8-184	11.9	1.30	E	6.8	.098	.249	.250	.236	.941	.812
9-185	12.	1.31	B	6.3	.028	.170	.280	.260	.2262	.711
10-186	12.	1.28	C	5.6	.070	.186	.350	.248	.2450	.841
11-187	12.	1.28	G	6.2	.182	.118	.378	.359	.1450	.1131
12-188	12.	1.28	G	[illegible]	.070	.262	.620	.397	.2610	.841
13-189	25.	1.30	E	2.5	.168	.131	.140	.015	.725	.669
14-190	12.	1.28	D	6.3	.112	.186	.462	.248	.1361	.661
15-191	25.	1.30	A	2.7	.070	.118	.462	.170	.2171	.5811
16-192	12.	1.31	H	3.5	.042	.118	.620	.161	.1941	.1135
17-193	25.	1.30	E	[illegible]	.042	.118	.140	.294	.125	.653
18-194	12.	1.30	D	6.5	[illegible]					
19-195	25.	1.26	H	2.5	.210	.131	[illegible]	.137	.[illegible]	.363

Structural Response Program

Compiled By ______

Date [illegible]
House PF-6

Phase 2-B				Displacement (10⁻¹ in.)						
1-21-65					7	8	9	10	11	12
Run	Alt.	Mach	Vec.	ΔV						
20-196	25	1.31	F	2.6	014	[illegible]	[illegible]	23[illegible]	813	5[illegible]0
21-197	25	1.25	A	2.5	014	131	023	124	2681	606
22-198	25	1.36	F	3.2	[illegible]	131	160	[illegible]	725	580
23-199	12.1	1.31	E	4.8	.042	302	280	389	1102	1015
24-200	12	1.30	A	4.9	.028	275	.406	322	2755	608
25-201	12.	1.30	E	5.3	.126	.262	.406	.248	1450	.740
26-202	25.	1.35	F	4.6	.042	249	154	372	1030	943
27-203	12.1	1.30	D	4.5	.070	.186	.462	.372	1585	667
28-204	25.	1.32	A							
29-205	12	1.30	E	3.7	.056	.157	420	.223	1930	449
30-206	25.	1.33	F	2.8	014	118	098	248	725	.540
31-207	26.5	1.33	A	3.8	01[illegible]	066	056	087	2560	435
32-208	25.5	1.52	F		.014	210	140	071	1088	1088
33-209	26.5	1.32	H	2.6	014	026	028	112	1545	218
34-210	12.	1.23	H	8.5	.266	.186	644	.273	3025	.580
35-211	25.5	1.36	E	5.1	042	.170	140	372	812	927
36-212	12.	1.28	D	7.6	.126	.197	.560	236	2118	.725
37-213	25	1.34	A	2.9	.014	.118	.028	.112	1931	.319
38-215	25.	1.32	E		.028	.131	.140	.248	960	986

Structural Response Program

Compiled By ______

Date [illegible]
House PF-6

Phase 2-B				Displacement.						
1-21-65					7	8	9	10	11	12
Run	Alt.	Mach	Vec.	ΔV						
60-216	12	1.30	G.	6.0	.140	.059	.348	.484	1505	.608
61-217	11.9	1.28	C	5.2	.238	.236	.280	.248	2463	.463
62-218	12.	1.31	G	5.2	.140	105	420	.324	1407	.550
63-219	12	1.31	H	7.9	.112	.244	.560	.245	3194	[illegible]3
64-220	11.9	1.30	D	4.8	.126	.197	.420	.136	1181	.551
65-221	11.7	1.31	H	5.7	.042	.249	.448	.248	2321	.435

STRUCTURAL RESPONSE PROGRAM

COMPILED BY ______

DATE [illegible]

HOUSE PF-6

PHASE 2-B					DISPLACEMENT (10⁻² in)					
1-22-65					7	8	9	10	11	12
Run	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]
1-222	12.	1.32	A		[illegible]	371	[illegible]	307	3117	[illegible]
2-223	12.	130	E	3.5	[illegible]	[illegible]	15[illegible]	37[illegible]	[illegible]	[illegible]
3-224	12	132	A	4.6	[illegible]	[illegible]	143	[illegible]	[illegible]	1.31
4-225	12.	127	B	10.7	072	[illegible]	[illegible]	131	214[illegible]	[illegible]
5-226	12	126	E	16.9	130	615	572	[illegible]	1334	393
6-227	12	127	B	21	[illegible]	3.[illegible]	24[illegible]	[illegible]	[illegible]	526
7-228	11.9	12	C	4.3	101	320	200	671	3331	738
8-229	12.	131	G	3.7	144	664	25[illegible]	26[illegible]	1150	55[illegible]
9-230	121	133	C	71	029	179	186	30[illegible]	1701	355
10-231	[illegible]	[illegible]	E	16	[illegible]	[illegible]	057	126	035	426
11-232	[illegible]	[illegible]	A	16	[illegible]	15	114	113	1610	860
12-233	[illegible]	[illegible]	E	22	014	026	063	[illegible]	303	026
13-234	[illegible]	[illegible]	A	59	029	171	103	252	2022	[illegible]
14-235	11.9	132	E	4.5	055	353	301	267	[illegible]	224
15-236	11.[illegible]	132	B	5.9	115	44[illegible]	624	353	55[illegible]	710
16-237	12.4	131.	E	4.8	[illegible]	158	163	181	72[illegible]	557
17-238	12.	129	F	6.2	144	254	721	278	27[illegible]	[illegible]
18-239	10	130	A	39	[illegible]	243	057	252	275	710
19-240	11.	125.	F	7.3	104	410	315	550	1653	317

STRUCTURAL RESPONSE PROGRAM

COMPILED BY ______

DATE [illegible]

HOUSE PF-6

PHASE 2-B					DISPLACEMENT (10⁻² in)					
1-22-65					7	8	9	10	11	12
Run	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]
20-241	16.	1.91	G	31	130	[illegible]	[illegible]	265	183	554
21-242	16.5	1.91	C	14	014	026	[illegible]	103	131	238
22-243	20.	1.2	G	09	014	015	[illegible]	113	240	284
23-244	30.2	1.6	F	26	010	[illegible]	[illegible]	126	[illegible]	454
24-245	30.20	1.6	A	21	010	210	035	176	103	358
25-246	30.25	1.6	F	46	014	604	[illegible]	126	456	355
26-247	30.25	1.6	A	1.5		128	224	113	5[illegible]	284
27-248	25.	1.91	A	1.5	010	115	[illegible]	0[illegible]	725	270
28-249	25.	1.6	F	24	021	011	[illegible]	126	425	526
29-250	25	1.6	A	16	014	125	021	050	718	180
30-251	29	1.6	E	23	[illegible]	[illegible]	[illegible]	[illegible]	305	[illegible]
31-252	25.	1.5	B	66	010	013	121	[illegible]	[illegible]	113
32-253	25.	1.6	E	16	014	013	014	013	377	316
33-250	25	1.5	B		014	115	114	[illegible]	[illegible]	170

STRUCTURAL RESPONSE PROFILE

COMPILED BY _____ DATE: 1/25/1965

HOUSE PF-6

PHASE 2-A 1-23-65					DISPLACEMENT. (10^{-2} in)						
					PEAK DISPL.	7	8	9	10	11	12
RUN	ALT.	VEL.	VEC.								
1-255	11.9	1.25	C			.089	.414	.298	.677	.2778	.755
2-256	11.9	1.25	G		6.9	.149	.124	.283	.299	1200	.915
3-257	11.95	1.29	C		6.6	.030	.262	.259	.381	1800	.592
4-258	11.3	1.30	D		6.7	.149	.262	.313	.150	2160	.829
5-259	12.	1.29	H		6.6	.149	.138	.067	.136	2340	.659
6-260	12.	1.30	D		3.1	.149	.345	.067	.136	2085	.579
7-261	12.	1.28	E		6.7	.119	.552	.067	.530	1050	.918
8-262	12.	1.27	A		6.3	.060	.603	.388	.350	2563	.760
9-263	12.	1.28	E		2.9	.149	.290	.283	.326	.870	.681
10-264	12.	1.30	A		3.7	.030	.249	.268	.177		.459
11-265	11.9	1.30	F		4.9	.119	.410	.313	.500	1069	
12-266	11.9	1.31	A		6.0	.030	.360	.030	.390	2790	.760
13-267	11.8	1.30	F		3.1	.180	.193	.149	.272	.765	.977
14-268	25.	1.36	F		2.8	.045	.083	.089	.150	.750	.598
15-269	12.	1.29	G		3.1	.149	.120	.298	.381	.765	.696
16-270	25.	1.35	A			.045	.276	.030	.360	2850	.532
17-271	12.1	1.29	C		3.8	.149	.331	.388	.530	2625	.760
18-272	25.	1.36	F		6.1	.075	.207	.149	.381	1094	.888
19-273	12.	1.26	G		5.7	.259	.193	.067	.530	1650	.859

STRUCTURAL RESPONSE PROFILE

COMPILED BY _____ DATE: 1/25/1965

HOUSE PF-6

PHASE 2-A 1-23-65					DISPLACEMENT. (10^{-2} in)						
					PEAK DISPL.	7	8	9	10	11	12
RUN	ALT.	VEL.	VEC.								
20-274	25.	1.39	A		2.7	.015	.138	.030	.136	1650	.296
21-275	26	1.35	F		2.8	.030	.138	.149	.350	.915	.740
22-276	25	1.36	A		2.6	.015	.138	.015	.150	1800	.326
23-277	25	1.36	F		2.3	.015	.041	.045	.136	.705	.566
24-278	24.6	1.35	A		3.1	.015	.138	.015	.123	1905	.311
25-279	12.	1.26	H		5.2	.149	.138	.692	.259	2877	.888
26-280	12.	1.31	D		3.2	.104	.124	.283	.109	1425	.444
27-281	12.	1.28	H		7.1	.149	.262	.477	.218	3660	.816
28-282	12.	1.28	D		12.1	.298	.373	.596	.368	2925	.988
29-283	25.	1.36	F		2.9	.030	.041	.130	.196	.885	.607
30-284	25.	1.36	A		2.1	.015	.055	.030	.123	1025	.266
31-285	12.	1.29	B		3.3	.060	.359	.313	.272	2550	.533
32-286	26	1.36	F		2.6	.030	.055	.045	.268	.915	.636
33-287	12.05	1.29	E		6.6	.119	.538	.603	.569	1650	1.036
34-288	25	1.37	A		2.1	.015	.110	.015	.068	.900	.296
35-289	12	1.29	B		6.2	.030	.538	.462	.368	2799	.710
36-290	25	1.37	F		2.9	.015	.027	.030	.123	.435	.666
37-291	25	1.37	A		6.6	.015	.166	.030	.258	1875	.666
38-292	25	1.36	F		3.1	.075	.138	.149	.350	1.2	.99

STRUCTURAL RESPONSE PROFILE

COMPILED BY _____ DATE 1/25/1965

HOUSE PF-6

PHASE 2-A — 1-23-65 — DISPLACEMENT, X 10^{-2}

RUN	REF	HORZ	VERT	PEAK FIELD	7	8	9	10	11	12
				AW						
39-293	12.	125	C	5.5	119	278	313	381	724	796
40-294	25.	137	A	0.9	015	221	830	252	2129	473
41-295	12.	130	G	3.7	030	016	610	095	735	666
42-296	25.	137	F	2.3	030	097	119	273	680	592
43-297	12.	125	C	7.2	130	600	632	608	2550	760
44-298	12.	120	G	7.3	067	248	894	806	3300	1430
45-299	12.	126	H	2.7	194	514	611	245	3310	678
46-300	12	125	D	2.8	065	138	298	010	1274	370
47-301	12.	124	H	3.1	119	120	667	258	2022	370
48-302	12.	129	E	4.2	015	248	298	252	970	629
49-303	12.	130	A	6.7	030	396	313	284	2350	859
50-304	12.	130	E	6.8	130	662	667	422	1215	888

STRUCTURAL RESPONSE PROFILE

COMPILED BY _____ DATE 1/25/1965

HOUSE PF-6

PHASE 2-A — 1-24-65 — DISPLACEMENT, (10^{-2} in.)

RUN	REF	HORZ	VERT	PEAK FIELD	7	8	9	10	11	12
				AW						
1-305	12.	122	F	6.6	110	376	145	391	362	918
2-306	12.	123	A	6.6	072	312	145	254	2569	693
3-307	12.	120	F	6.2	036	266	188	381	725	987
4-308	25	125	A	3.8	043	284	116	263	2245	423
5-309	12.2	122	G	6.9	163	039	290	229	3376	663
6-310	12.	122	C	6.6	072	260	290	318	2175	536
7-311	12.	120	G	6.5	172	104	300	254	1450	747
8-312	12.	120	C	6.6	110	260	188	292	2505	536
9-313	12.	125	H	6.8	043	260	609	140	2630	296
10-314	12.	126	D	5.0	157	275	290	160	1481	560
11-315	12.	125	H	6.2	129	275	609	127	3070	268
12-316	12.	125	D	6.5	163	284	1121	216	1812	677
13-317	12.	126	A	6.6	089	275	145	282	2850	560
14-318	12.	124	F	5.3	086	377	246	470	812	1128
15-319	12.	126	A	3.6	027	260	145	250	2630	564
16-320	12.	121	B	6.1	129	390	635	355	2260	846
17-321	12.1	120	E	5.7	129	417	635	348	1305	715
18-322	11.95	120	A	6.1	043	284	367	714	2175	564
19-323	12.	122	E	3.9	072	417	635	669	1521	705

STRUCTURAL RESPONSE PROGRAM

Compiled By ______

Date 1-25-1-26-65
House PE-6

Phase 2-B				Displacement (10⁻² in)						
1-26-65				Free Fall	7	8	9	10	11	12
Run	Act	Nom	Vc	OK						
20-324	12	1.23	C	6.1	043	417	435	363	2755	733
21-325	12.	1.23	G	5.9	003	390	435	381	1082	719
22-326	12.	1.29	C		029	226	290	242	2017	423
23-327	12.	1.29	G	6.3	072	377	377	354	1160	691
24-328	12	1.20	H	7.9	218	221	870	368	3680	464
25-329	12.	1.21	D	4.6	129	260	435	368	1775	493
26-330	12.	1.21	H		143	207	638	216	2435	423
27-331	12	1.20	D	65	143	260	435	254	1815	620
28-332	12.	1.21	E	4.6	072	403	435	381	1319	705
29-333	12.	1.29	B	3.8	043	260	319	178	3130	437
30-334	12.	1.23	E	8.1	057	390	350	361	1607	.665
31-335	12.	1.25	B	4.1	014	195	261	127	1581	206
32-336	11.9	1.20	F	4.2	003	351	159	381	630	787
33-337	12.	1.2	H							
34-338	12.	1.21	F		029	103	145	.207	501	532
35-339	12.	1.21	J	2.9	010	207	116	.242	1305	560
36-340	12.	1.21	G	3.0	.143	.065	290	250	1480	.569
37-341	12.	1.20	C	4.9	057	247	203	254	2597	1395
38-342	12.	1.22	G	44	143	117	.443	381	2245	.733
39-343	12.	1.22	C	3.9	029	208	131	242	2219	.394

STRUCTURAL RESPONSE PROGRAM

Compiled By ______

Ceiling
200# static load deflects s.g. 0.008 in

Date 1-21-65
House PE-6

Phase 2-B					Deflections (in)			Actual Pressure (psf)		
					Down	Up	Total	Datacraft	Boeing	
Run	Act	Nom	Vc	AV						
1-177	12.	1.30	H		.045	.045	.086	5.3	5.7	
2-178	12.	1.30	D		.030	.040	.070	4.1	5.0	
3-179	12.	1.30	H		.045	.060	.105	6.8	6.1	
4-180	12.	1.30	A		.030	.030	.060	6.4	5.2	
5-181	12.	1.31	F		.045	.045	.090	4.6	5.3	
6-182	12.	1.30	A		.030	.035	.065	4.4	4.9	
7-183	12.1	1.30	G		.030	.045	.075	5.3	4.7	
8-184	12.1	1.30	E		.045	.045	.090	4.8	4.5	
9-185	12.1	1.31	B		.050	.052	.100	4.3	5.5	
10-186	12.	1.30	C		.040	.050	.090	5.6	5.7	
11-187	12.	1.30	G		.040	.050	.090	4.2	5.5	
12-189	12.	1.30	C		.025	.035	.060	—	5.4	
13-189	25.	1.36	E		.015	.020	.035	2.5	2.9	13 56
14-190	12.	1.39	D		.015	.020	.035	5.2	—	
15-191	25.	1.30	A		.022	.030	.050	2.9	3.5	13 56
16-192	12.	1.31	H		.025	.025	.050	2.5	5.0	
17-193	25.	1.30	F		.020	.025	.045	—	—	13 56
18-194	12.	1.30	D		.024	.035	.055	4.8	—	
19-195	25.	1.36	A		.025	.025	.050	2.6	2.4	13 56

Structural Response Record

Compiled By _____

Ceiling

200# static load deflects 3.9. .008 in.

Date 1-21-65

House PE-6

Phase 2-B	Deflections (in)			Actual Pressure (psf)		
	Down	Up	Total	Datacraft	Boeing	
Pin Ref Horiz Vert Ax						
25-20 12. 1.30 E	.040	.045	.085	53	47	
26-20 2.5 1.35 F	.020	.025	.045	46	—	B-5B
27-20 12.1 1.30 D	.025	.30	.055	44	—	
32-20 2.5 1.35 F	.025	.030	.055	—	40	B-5B
33-20 2.5 1.35 A	.015	.020	.035	2.6	2.7	B-5B
34-21 12. 1.35 H	.030	.040	.070	85	49	
35-21 2.5 1.36 E	.035	.040	.075	31	30	B-5B

Structural Response Record

Compiled By _____

.0060" with ~.200# push at center of wall

North Wall

Date 1-21-65

House PE-6

Phase 2-B	Top Frame (in)			Middle Wall (in)			Actual Pressure (psf)		
	In	Out	Ttl	In	Out	Ttl	Datacraft		
Pin Ref Horiz Vert Ax									
2-178 12. 1.28 D	.005	.005	.010	.005	.020	.025	41		
3-179 12. 1.30 H	.010	.010	.020	.020	.040	.060	68		
4-180 12 1.30 A	.015	.015	.020	.025	.025	.050	64		
5-181 12. 1.31 E			.010	.005	.010	.015	46		
6-182 12. 1.28 A			.015	.025	.030	.055	44		
7-183 12.1 1.30 B			.015	.020	.020	.040	53		
8-184 12.1 1.30 E			.005	.010	.010	.020	48		
9-185 12.1 1.31 B			.015	.020	.025	.045	43		
10-186 12. 1.29 C			.010	.025	.025	.050	56		
11-187 12 1.30 G			.005	.025	.025	.050	42		
12-188 12. 1.30 C			.020	.030	.025	.055	54		
13-189 2.5 1.36 F			—	.004	.004	.008	2.5	B-5B	
14-190 12. 1.29 D			—						
15-191 2.5 1.30 A			—					B-5B	

Structural Response Program

Compiled By ______

Date 1-25-65; 1-28-65
House PF-6

Phase 2-B 1-25-65 Run	Alt	Hum	Vc	Free Field AV	P1	P2	P3	P4	P5	P6	P7	P8	P9	P10	P11	P12	P13		D1	D2	D3	D4	D5	D7	D8	D9	D10	D11	D12
1-244	12	130	H	–	NR	NR	NR	NR	NR	NR	(No		Record	)															
2-245	12	130	D	–																									
3-246	12	130	H	–																									
4-347	12.0	126	A	–		2.2	4.4	0.8		2.2	1.6	1.6	1.9	NR	NR	NR	NR												
5-348	12.0	133	F	–		2.9	4.8	5.2		2.4	2.5	1.9	2.5																
6-349	12.	131	A	–		2.2	1.7	1.0		0.3	1.3	0.6	3.2																
7-350	12	132	B	–		2.9	2.8	2.9		0.5	0.6	0.6	5.2	5.5	8.2	8.9	4.9		1245	1318	966			.028	.600	.623	.260	1835	.372
8-351	12	130	E	32		4.8	5.0	2.4		2.6	2.6	1.3	2.9	1.8	5.2	3.0	2.5		.673	2075	2180			.028	.370	.282	.286	987	.552
9-352	11.8	126	B	93		5.0	5.4	5.7		1.3	1.6	1.6	2.2	10.8	14.8	2.1	2.2		3538	1955	1380		1200	.127	.632	.589	.990	3820	.786
10-353	12.5	13	C	32		3.5	5.6	2.9		0.6	0.3	0.9	6.4	5.1	4.9	4.3	4.6		572	1100	1665			.056	.162	.161	.237	1622	.345
11-354	121	131	G	89		4.2	3.2	5.1		0.4	0.9	1.6	4.9	2.6	1.9	1.6	5.1		2345	2750	1932			.268	.162	.522	.662	1257	.621
12-355	12	130	C	3.7		3.5	5.9	3.5		1.2	0.3	1.4	9.0	6.4	4.1	4.6	6.4		862	1865	2916			.127	.338	.250	.390	2655	.483
13-356	12.	125	D	2.9		4.8	5.0	2.7		0.6	0.3	1.2	4.5	2.6	1.9	4.6	3.1		572	1220	2185			.113	.129	.260	.163	1835	.616
14-357	11.	115	H	2.9		2.4	6.2	5.9		2.5	1.1	4.7	5.4	3.0	1.0	2.0	2.5		1090	2199	2372	.296		.282	.503	.870	.325	1565	.428
15-358	16.	1.46	D	2.5		4.4	5.0	2.6		0.9	0.3	1.6	3.2	2.4	7.6	2.2	2.1		730	1428	4810			.141	.338	.608	.260	2540	.538
16-359	13	130	E	–		2.9	4.6	2.1	2.1	0.9	0.9	1.6	2.9	2.3	1.5	2.6	2.2		530	2810	1180			.062	.691	.423	.681	945	.304
17-360	11.9	135	B	4.1		2.5	5.1	3.1	3.1	1.2	0.6	0.9	4.9	1.6	2.1	4.9	4.6		2000	1392	828			.062	.271	.311	.221	1622	.276
18-361	12.9	133	E	2.9		5.2	4.7	2.4	2.4	0.6	0.9	1.6	2.9	1.8	1.9	2.3	2.5		600	2430	2483			.028	.370	.282	.273	1114	.469
19-362	12.	126	F	3.0		4.4	1.9	3.9	2.8	0.6	0.6	0.6	2.9	1.6	1.5	2.2	1.8		701	1852	718			.062	.206	.161	.286	.817	.621
	* Changed to ¢ of attic, 1-28-65																												

Structural Response Program

Compiled By ______

Date 1-25-65; 1-28-65
House PF-6

Phase 2-B 1-25-65 Run	Alt	Hum	Vc	Free Field AV	P1	P2	P3	P4	P5	P6	P7	P8	P9	P10	P11	P12	P13		D1	D2	D3	D4	D5	D7	D8	D9	D10	D11	D12
20-363	12	133	A	32		3.1	4.0	4.7	5.5	1.3	0.6	0.6	8.1	5.5	4.5	2.9	2.3		1030	2575	1793			.028	.348	.127	.273	2937	.621
21-364	12	132	F	3.5		4.8	4.0	2.4	3.1	0.6	1.3	0.9	1.3	1.6	1.5	2.0	4.0		1030	2282	352			.127	.245	.169	.364	1015	.538
22-365	12	130	G	55		6.5	3.6	2.1	2.8	1.3	1.2	0.9	4.2	3.3	1.9	3.3	3.4		2561	2260	1590			.183	.129	.423	.390	1298	.621
23-366	12	129	C	37		3.5	4.3	3.0	2.1	0.6	0.6	1.3	3.9	3.6	3.4	3.9	4.6		610	753	2112			.071	.232	.141	.260	1623	.345
24-367	14.9	134	G	25		2.2	1.6	1.2	1.4	0.6	0.6	0.5	1.6	1.5	1.1	1.3	1.5		572	1135	718			.042	.038	.169	.156	.560	.276
25-368	16	135	C	3.3		1.7	3.7	2.0	2.1	0.6	0.3	1.6	4.9	2.4	.6	4.6	3.1		915	1160	1622			.028	.065	.141	.234	1481	.304
26-369	12	135	H	2.6		6.1	4.7	4.7	5.2	1.6	0.6	0.9	5.6	4.0	3.4	3.9	3.6		3862	1564	1905			.113	.206	.451	.234	2285	.412
27-370	12.2	130	D	6.9		5.2	5.5	5.5	4.1	0.9	0.9	1.9	5.6	4.0	3.7	5.9	5.1		1288	2016	5320	.218	.903	.197	1097	.579	.247	2610	.497
28-371	12	126	H	–		2.5	2.8	2.4	2.8	1.2	0.3	0.9	3.4	2.2	1.9	2.3	2.8		1372	672	1643			.141	.168	.423	.130	1805	.276
29-372	12.9	135	F	3.0		5.2	4.7	3.9	3.8	0.9	1.3	0.9	2.2	2.1	1.9	2.0	2.1												
30-373	12.85	121	A	53		5.6	5.0	4.7	4.5	1.9	1.5	0.6	12	2.6	5.2	4.1	7.7		1450	1575	2070			.127	.613	.169	.403	3670	.428
End																													
	* Changed to ¢ of attic, 1-28-65																												

Pressure psf. Displacement (10⁻² in).

Structural Response Program

Compiled By ______

Date [illegible]

House PF-6

Phase 2-B 1-26-65 Run	A.F.	Hum	Vec	Face Field AW	Pressure psi 1	2	3	4	5	6	7	8	9	10	11	12	13	Displacement (10⁻² in) 1	2	3	4	5	7	8	9	10	11	12
1-374	12	132	B	–		(	No				Record	)																
2-375	12.5	126	E	4.8	4.1	9.2	2.5	3.7	4.4	1.5	1.2	1.6	2.1	2.8	2.8	3.2	3.3	.677	2600	4350			.012	.516	.409	.492	.124	.734
3-376	12	133	B	41	4.9	2.6	3.4	2.9	41	1.5	0.6	1.1	6.7	5.1	6.1	7.3	6.1	2065	1580	1066			.056	.361	.310	.368	1760	.310
4-377	12	131	C	5.0	3.2	3.6	2.5	4.0	4.7	1.2	0.6	1.1	7.0	5.7	6.2	7.3	6.5	677	1425	3735			.140	.322	.282	.379	2500	.490
5-378	12	132	G	–	2.2	8.2	4.4	2.9	5.4	1.5	0.8	1.1	4.7	3.6	1.9	3.6	3.6	2320	2460	2235	145		.168	.129	.423	.368	1480	.522
6-379	12	132	C	–	3.4	3.2	2.5	2.9	4.4	1.2	0.8	1.6	7.0	6.0	3.4	2.3	5.7	.805	.880	4135	.261		.126	.258	.282	.379	2181	.524
7-380	12.5	132	D	45	3.1	5.4	9.4	3.7	5.7	0.9	0.8	1.1	4.4	3.4	3.4	4.5	4.0	.983	.900	5510			.140	.129	.438	.126	2279	.409
8-381	11.95	130	H	70	2.5	4.3	4.1	3.2	4.4	1.5	1.1	1.9	5.3	4.1	3.3	4.2	4.5	2225	.626	2350			.140	.219	.536	.227	1960	.310
9-382	11.95	131	D	48	(	No		Record		)	0.9	1.6	4.7	3.9	2.6	4.1	4.5	.821	.721	5290			.140	.258	.438	.227	2345	.479
10-383	12	130	H	25							0.8	1.2	3.7	2.6	2.5	3.4	3.3	1982	.583	1.723			.070	.129	.423	.126	1739	.296
11-384	12	130	E	81	3.7	9.0	8.1	4.4	5.7	0.9	0.9	1.7	4.4	2.8	2.8	4.4	3.4	.729	2550	2865	.342		.140	.245	.310	.277	1241	.663
12-385	12	130	B	69	6.4	4.3	3.7	4.4	6.3	1.2	0.8	1.2	7.0	5.1	5.1	7.8	6.3	2225	1990	.970			.070	.310	.338	.353	1276	.423
13-386	12	130	E	5.0	2.7	7.5	6.6	3.3	3.5	0.9	1.3	1.7	4.4	2.3	2.1	4.2	3.3	.805	2060	4270			.126	.374	.296	.379	1241	.832
14-387	12	125	B	–	6.9	3.2	3.7	2.9	4.7	0.9	0.5	0.6	6.2	5.0	4.4	6.2	4.9	1920	1825	.960			.002	.258	.282	.227	1861	.324
13-38 15-388	25	136	F	3.8	4.4	5.4	3.1	2.2	3.2	2.8	2.3	1.7	2.8	2.0	1.9	2.6	3.1	1160	3600	1352			.002	.129	.141	.368	.828	.719
13-38 16-389	25	137	A	3.9	4.1	3.2	3.4	2.9	3.2	1.2	0.6	1.2	4.5	3.2	2.5	2.1	3.7	.397	1670	.913			.014	.129	.014	.126	1392	.423
17-390	12	131	G	55	5.6	4.5	3.1	2.2	3.9	1.2	1.7	1.9	2.4	2.8	1.2	1.9	2.8	1616	.743	1175			.140	.129	.310	.200	1311	.607
B-38 18-391	25	137	E	46	5.6	5.0	3.1	2.2	3.2	1.2	1.6	0.8	3.0	2.3	2.3	3.6	2.1	1030	3600	.598			.056	.129	.155	.290	.966	.635
19-392	12	136	C	–	5.3	5.0	5.6	5.2	4.7	2.1	0.8	1.6	7.8	6.4	4.4	7.3	6.3	1270	1590	3530	.290		.112	.387	.296	.567	4270	.719
	*	changed	to	¢	of attic	, 1-28-65																						

Structural Response Program

Compiled By ______

Date [illegible]

House PF-6

Phase 2-B 1-26-65 Run	A.F.	Hum	Vec	Face Field AW	Pressure psf 1	2	3	4	5	6	7	8	9	10	11	12	13	Displacement (10⁻² in) 1	2	3	4	5	7	8	9	10	11	12
A-38 20-393	25	137	A	4.9	4.7	3.6	3.4	2.6	1.8	1.8	1.1	6.4	3.4	4.8	5.8	6.0	5.4	2048	1822	.897			.014	.129	.028	.151	2830	.564
21-394	12	136	G	3.7	4.2	5.7	3.1	2.9	2.5	1.2	1.2	0.9	3.7	2.0	1.4	3.2	3.1	1805	2.600	1175			.160	.116	.409	.290	1681	.550
B-38 22-395	25	134	F	2.2	2.8	3.6	1.9	1.8	2.2	2.5	1.2	1.2	1.9	1.4	1.1	1.9	2.1	.563	2165	.456			.014	.106	.113	.252	.704	.423
23-396	12	130	C	4.7	3.1	2.9	4.4	2.9	3.2	1.5	1.1	1.7	6.2	3.9	3.4	5.0	3.9	.742	4.801	1.102			.028	.129	.155	.239	2000	.451
A-38 24-397	25	138	A	3.5	3.7	3.2	3.4	2.9	3.2	4.0	1.9	1.9	3.4	3.2	2.6	3.6	3.3	.628	2165	.780			.014	.129	.028	.126	2082	.423
A-38 25-398	25	138	F	6.7	4.7	5.0	2.6	2.9	4.1	1.2	1.6	0.8	3.8	2.3	2.6	3.4	3.3	.885	3415	.598			.002	.155	.141	.368	.758	.635
A-38 26-399	25	138	A	21	2.5	2.2	2.2	2.6	2.5	1.2	1.5	0.5	3.1	3.0	3.4	3.1	2.8	.483	1380	.573			.014	.077	.028	.126	2000	.423
27-400	12	134	H	36	4.2	4.3	3.1	3.3	4.4	1.2	0.5	0.6	4.4	3.2	3.1	4.1	3.7	1772	2035	1765			.126	.155	.409	.227	2239	.451
28-401	11.9	125	D	3.0	2.8	3.3	5.0	3.6	3.2	0.9	0.8	1.7	3.3	2.5	2.3	3.6	3.0	.660	1.325	1368			.070	.106	.292	.125	1599	.310
29-402	11.95	131	H	–	3.7	5.4	3.8	2.9	5.1	1.5	0.5	0.8	6.1	4.4	2.8	4.9	4.5	1579	.580	1220			.126	.129	.310	.202	2000	.353
30-403	12	132	D	71	3.7	7.2	10.9	2.4	5.4	1.5	1.1	1.9	5.8	3.6	4.4	5.8	5.1	1616	2120	4290			.154	.219	.368	.164	[illegible]	.351
13-38 31-404	25	137	F	26	2.5	3.2	2.4	1.5	1.9	1.6	1.2	0.6	2.0	1.8	1.6	2.4	2.2	.467	2281	.661			.028	.065	.085	.214	.825	.423
13-38 32-405	25	138	A	4.7	5.0	3.9	3.4	2.9	5.1	1.5	1.7	1.1	5.8	4.6	4.4	5.8	5.4	.967	2190	.735			.014	.129	.028	.137	2476	.635
13-38 33-406	25	138	F	3.1	4.4	4.3	2.5	2.6	2.2	1.5	1.6	0.8	2.5	2.1	1.7	3.4	3.0	.805	3155	.598			.028	.129	.140	.278	1690	.564
34-407	12	133	G	3.8	5.5	4.3	3.1	2.6	2.2	1.2	0.9	0.8	3.0	2.5	1.4	2.9	2.5	[illegible]	[illegible]	1470			.140	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]
13-38 35-408	25	138	A	36	3.4	3.6	3.4	2.9	2.8	1.6	1.9	0.6	4.1	3.2	2.3	3.9	4.0	[illegible]	[illegible]	.413			.014	.129	[illegible]	.151	[illegible]	
13-38 36-409	12	133	C	4.5	2.1	2.5	4.4	7.9	3.6	1.2	0.6	1.6	9.6	3.6	3.0	4.9	4.6	[illegible]	[illegible]	[illegible]			[illegible]	[illegible]	.197	.277	[illegible]	.423
37-410	25	137	F	58	5.0	5.7	2.5	3.3	3.8	1.2	1.4	6.2	2.5	2.1	1.9	3.6	3.0	[illegible]	[illegible]	.595			[illegible]	[illegible]	.151	.252	1630	.575
38-411	11.9	135	G	7.3	10.0	8.0	4.1	4.6	6.3	1.2	1.2	0.9	5.1	3.7	2.8	4.9	4.2	[illegible]	[illegible]	[illegible]	.435		.165	[illegible]	[illegible]	[illegible]	[illegible]	[illegible]
	*	changed	to	¢	of attic	, 1-28-65																						

STRUCTURAL RESPONSE PROGRAM

COMPILED
By ______

DATE: 1-25-65; 1-28-65
HOUSE PF-6

PHASE 2-A — 1-26-65

Run	AT	Hum	Vel	AV	P 1	P 2	P 3	P 4	P 5	P 6	P 7	P 8*	P 9	P 10	P 11	P 12	P 13	D 1	D 2	D 3	D 4	D 5	D 7	D 8	D 9	D 10	D 11	D 12
					PRESSURE psf													**DISPLACEMENT X 10⁻²**										
39-413	25	137	A	2.8	3.1	2.2	2.5	2.2	2.5	0.9		.6	3.1	2.7	2.3	3.4	3.1	.628	1225	.598			.014	.052	.014	.113	2220	.469
40-412	25	137	F	25	3.4	2.2	2.5	1.8	1.9	1.2	1.1	0.8	2.1	1.8	1.7	2.6	2.4	483	2118	461			.014	.116	.085	239	800	.409
41-414	25	138	A	—	3.4	3.6	3.1	2.6	2.2	1.4	2.0	0.8	4.4	3.9	3.3	4.1	4.5	1015	1778	.897			.014	.129	.028	.126	2565	.508
42-415	25	138	F	3.7	4.4	5.4	3.4	2.9	2.2	1.8	1.7	0.8	3.1	2.8	2.3	3.6	2.6	965	4565	.820			.042	232	.161	.379	1090	.705
43-416	25	141	A	25	3.4	2.9	2.8	4.5	2.2	2.2	1.4	0.9	2.3	1.8	1.3	2.4	2.2	.483	1410	.603				106	.014	.101	1270	.198
44-417	12.	128	H	6.0	10.9	5.0	3.7	5.5	8.9	1.5	0.8	1.4	9.7	6.0	4.4	9.6	7.5	3600	2018	1779	435		126	.232	.438	.239	2330	.423
45-418	12	125	H	4.2	6.2	2.6	2.1	1.8	[illegible]	1.2	0.3	0.8	3.4	2.8	2.3	3.2	3.3	1432	1155	1250			.084	129	.282	.126	1589	.338
46-419	12.	120	D	3.5	3.1	3.6	5.6	2.6	3.2	1.5	0.8	1.7	4.2	3.0	2.8	4.5	3.2	.493	1.910	2810			.080	.129	.409	139	1519	.310
47-420	12.	131	G	4.0	4.6	5.0	2.5	2.2	2.2	1.2	0.6	0.9	2.6	2.1	1.3	2.7	2.5	1531	1.910	2350			126	.039	.141	.126	.939	.310
48-421	12.	131	C	3.7	2.5	2.5	3.1	2.2	1.9	0.9	1.1	1.1	2.5	2.7	2.8	3.2	3.0	.669	1.695	1.295			.010	106	113	252	2345	381
49-422	12	133	G	7.6	9.4	7.5	3.4	2.9	6.0	1.5	1.1	1.2	4.8	4.4	3.4	3.7	4.0	2125	3300	1515			.160	.116	.923	379	1931	.677
50-423	12.	126	H	7.2	10.9	6.8	4.7	5.5	8.2	1.8	1.1	1.9	9.4	7.3	5.8	NR	7.6	3675	1570	2250	.305		.100	.348	.719	.252	3590	.494
51-424	12.2	13	D	3.6	3.4	5.7	6.6	3.3	2.8	1.2	0.9	1.7	3.3	2.1	2.6	4.2	3.2	.661	1.695	2235			.112	.116	.169	.113	2070	.494
52-425	12.2	13	H	5.2	7.5	5.0	3.4	3.3	4.7	2.1	1.1	1.4	6.1	5.0	4.7	6.2	6.0	2105	1910	2618			.140	.387	.677	252	2840	.409
End																												

* CHANGED TO ℄ OF ATTIC, 1-28-65

STRUCTURAL RESPONSE PROGRAM

COMPILED
By ______

DATE: 1-25-65; 1-28-65
HOUSE PF-6

PHASE 2-A — 1-27-65

Run	AT	Hum	Vel	AV	P 1	P 2	P 3	P 4	P 5	P 6	P 7	P 8*	P 9	P 10	P 11	P 12	P 13	D 1	D 2	D 3	D 4	D 5	D 7	D 8	D 9	D 10	D 11	D 12
					PRESSURE psf													**DISPLACEMENT (10⁻² in)**										
1-426	12.	126	D	7.9	(No Record)						1.1	1.7	5.6	4.2	4.2	6.2	5.1	1592	2.110	4630	612		298	.422	.609	.270	1618	.618
2-427	11.95	123	H	5.7							0.6	1.9	5.5	4.7	3.1	4.5	4.1	2505	1470	1899			149	.244	.453	149	1980	.367
3-428	11.95	123	D	—							1.2	1.9	5.8	4.7	4.3	6.4	6.0	1915	2260	6600	.628		268	.409	.573	.270	.250	.661
4-429	12.	1.25	H	3.9							0.6	1.7	4.0	3.5	3.1	3.7	3.2	2720	1720	2.058			.199	.200	.453	.243	1675	.514
5-430	11.95	125	E	4.6							1.2	1.7	4.3	3.3	2.5	3.3	3.7	.895	2880	3970			.119	.518	.468	.405	1.190	.867
6-431	11.95	126	B	5.4							0.5	1.4	6.4	5.2	4.9	6.1	6.0	3205	.621	.957	.153		.149	.409	.393	270	1925	.441
7-432	12.	1.30	E	4.5							1.7	2.5	3.5	3.0	2.6	3.5	4.0	.910	1469	4960			.075	.409	.153	322	1455	832
8-433	12.	1.30	A	4.2							0.6	1.3	4.3	3.1	3.4	3.5	3.8	1809	1409	.785			.075	.368	.317	.257	1960	.456
9-434	12.	126	F	9.3							1.9	1.9	4.6	3.5	5.2	6.4	6.5	1239	3270	2619			.045	.394	.211	.436	.867	1.072
10-435	11.8	120	A	4.6							1.6	1.3	5.2	2.8	3.4	5.1	6.5	1319	2050	1899			.030	.177	.906	.270	2.697	.661
11-436	12.	1.21	F	—							2.8	3.1	5.2	2.5	4.3	5.1	5.9	2023	4520	4198	168		.005	.394	.196	.513	1250	.425
12-437	12	120	A	—							1.6	1.6	5.8	4.2	4.6	5.7	5.9	.170	1679	1789			.015	.272	.151	.270	[illegible]	.735
13-438	11.5	120	F	3.3							3.1	3.1	6.1	3.5	2.1	4.8	5.9	1830	1049	2162			.030	.254	.166	.351	1250	.162
14-439	12.	122	A	6.1							1.2	1.6	5.8	5.6	[illegible]	6.0	6.5	1906	1985	1318			.030	.272	.176	.257	2353	.720
15-440	12	122	G	7.0	2.1	6.6	3.1	2.6	3.8	0.9	1.6	2.8	3.6	3.5	3.1	5.1	3.2	2419	2239	1601			.160	.169	.302	[illegible]	1102	.691
16-441	12.	1.25	C	6.8	3.1	2.6	6.5	4.4	3.2	1.2	0.9	1.6	4.9	5.2	4.3	6.1	[illegible]	[illegible]	1595	[illegible]			.045	.136	[illegible]	[illegible]	[illegible]	.514
17-442	11.85	120	G	4.5	8.3	9.7	4.6	6.6	6.4	4.5	1.9	1.9	5.2	4.6	5.7	5.7	4.4	[illegible]	[illegible]	[illegible]			253	.136	.183	[illegible]	.62	970
18-443	12.	125	C	5.0	3.4	3.5	6.2	4.0	3.5	0.9	1.7	1.6	5.8	5.6	4.3	7.0	5.6	[illegible]	1675	2550			[illegible]	.231	.302	.405	[illegible]	[illegible]
19-444	12.	125	G	6.5	6.5	5.2	3.4	3.7	4.5	1.2	1.6	1.6	4.0	3.5	3.1	5.4	4.7	[illegible]	2254	1410			.149	[illegible]	[illegible]	[illegible]	[illegible]	.779

* changed to ℄ of attic, 1-28-65

STRUCTURAL RESPONSE PROGRAM

COMPILED BY _____

DATE: 25-65: 1-28-65

HOUSE PE-6

RUNS 2-B — 1-27-65

RUN	SEC	VIEW	VEL	FILE TAPE	PRESSURES p.s.f. 1	2	3	4	5	6	7	8*	9	10	11	12	13	DISPLACEMENT (10⁻² in.) 1	2	3	4	5	7	8	9	10	11	12
20-448	12	125	H	—	7.4	4.5	3.4	2.9	4.8	2.1			NO	RECORD				903	1635	2355			.109	.214	.453	.216	.310	.514
21-448	12	125	D	37	2.8	3.8	5.5	2.6	2.9	1.7								1073	1690	3920			.090	.150	.348	.108	.870	.991
22-447	12	127	H	57	7.1	4.5	3.4	2.3	4.5	2.1								1510	1242	2060			.119	.218	.438	.135	.285	.397
23-448	12	127	D	55	4.0	6.6	9.2	6.2	4.5	6.5								1953	2550	6250			.140	.272	.664	.135	.220	.514
24-449	12	125	H	54	8.3	5.2	3.4	5.5	6.4	2.1								2795	1221	2180			.109	.254	.453	.135	.295	.612
25-450	12	122	D	114	5.2	8.0	12.6	10.2	5.4	6.5								1970	2900	8275	489		.285	.272	.710	.162	.399	.588
26-451	12	120	F	66			C		NO				RECORD					1790	1035	769			.045	.218	.136	.270	.088	.172
27-452	12	124	H	38														931	935	785			.015	.272	.136	.216	.985	.514
28-453	12	12	F	153														1720	1925	1760			.090	.609	.225	.392	.102	.172
29-454	12	115	H	56														1271	655	982			.030	.272	.151	.243	.220	.720
30-455	12	12	F	5.0														1668	2335	2670			.090	.531	.302	.132	.974	.1146
End																												

* CHANGED TO ℄ OF ATTIC, 1-28-65

STRUCTURAL RESPONSE PROGRAM

COMPILED BY _____

DATE: 25-65: 1-28-65

HOUSE PE-6

RUNS 2-B — 1-28-65

RUN	SEC	VIEW	VEL	FILE TAPE	PRESSURES p.s.f. 1	2	3	4	5	6	7	8*	9	10	11	12	13	DISPLACEMENT (10⁻² in.) 1	2	3	4	5	7	8	9	10	11	12
1-456	12.	120	B	55	8.3	4.4	3.4	4.2	5.4	2.4	1.9	2.5	6.2	6.3	4.7	5.1	5.9											
2-457	12.	123	E	57	3.7	9.2	6.2	4.2	5.4	3.0	2.1	4.1	6.9	3.8	3.2	4.8	6.2											
3-458	12	127	B	48	7.4	3.7	3.4	5.0	5.7	2.7	1.9	3.2	6.9	6.7	4.4	5.1	6.2											
4-459	195	12	C	—	4.3	4.4	9.2	5.9	2.2	1.5	1.6	2.8	7.2	7.0	7.6	8.5	7.4											
5-460	205	125	G	92	6.3	5.8	3.4	2.9	6.8	2.1	2.5	2.8	4.4	3.5	3.2	6.4	4.7											
6-461	12	12	C	68	4.0	3.4	7.7	5.9	5.0	1.2	1.3	1.9	6.6	5.2	5.2	6.4	6.5											
7-462	12	129	G	99	7.4	7.1	3.4	5.9	5.7	1.8	1.2	2.8	5.0	3.8	3.8	6.7	5.9											
8-463	12	123	G	39	6.2	4.4	2.1	2.5	4.3	2.1	2.5	1.9	4.1	3.1	3.2	4.8	5.3											
9-464	12	122	C	52	4.0	3.4	6.5	4.2	5.4	1.5	1.6	1.3	6.2	5.2	5.4	6.1	6.2											
10-465	12	120	G	51	8.0	6.5	3.4	2.8	5.7	2.1	2.8	1.9	4.7	3.5	3.5	6.7	5.5											
11-466	12	122	C	52	4.0	3.4	6.8	4.6	4.7	1.2	1.6	1.6	6.2	5.2	5.2	5.8	5.9											
12-467	12	126	G	46	7.2	5.4	3.7	3.4	5.4	2.1	2.8	1.9	5.0	3.8	3.5	6.4	5.9											
13-468	12	125	C	50	5.4	3.4	6.6	6.3	4.7	1.5	1.3	1.6	6.2	5.9	6.0	7.0	6.2											
14-469	12	126	G	49	7.1	5.8	3.4	2.5	5.0	2.1	2.5	1.9	4.7	3.5	3.4	6.1	5.0											
15-470	12.	126	C	67	3.4	3.7	9.2	4.6	5.4	1.5	1.6	1.6	4.4	5.9	6.3	7.4	6.2											
16-471	12	126	G	—	4.6	4.1	2.1	2.5	3.6	1.4	2.5	1.6	2.7	2.1	2.2	4.3	4.4											
17-472	12.	126	C	121	3.1	3.4	6.6	4.2	3.6	1.5	1.3	1.6	5.6	4.9	4.7	6.4	5.9											
18-473	195	126	G	33	5.2	4.1	2.6	2.5	3.6	1.4	1.4	1.1	1.1	2.8	1.9	3.6	4.1											
19-474	12	126	G	51	8.0	6.8	3.7	4.0	5.0	2.4	2.6	1.9	5.0	3.5	3.5	6.4	5.7											

* Changed to ℄ of attic, 1-28-65

Structural Response Program

Compiled By ______

Date 1-28-65

House PF-6

Phase 2-B 1-28-65 Run	Alt	Head	Vic	Free Field AV	Pressure p.s.f. 1	2	3	4	5	6	7	8*	9	10	11	12	13	Displacement (10⁻² in) 1	2	3	4	5	7	8	9	10	11	12
20-475	12.	122	G	4.3	6.2	4.1	2.8	2.5	2.4	3.1	1.5	1.6	4.1	3.1	2.2	4.8	1.1											
21-476	12	125	C	3.5	4.0	3.1	5.9	4.2	2.9	1.5	1.3	1.6	6.2	2.5	3.2	4.8	5.3											
22-477	12	125	G	5.0	2.4	5.8	3.4	3.4	3.6	2.7	2.8	1.6	4.7	2.5	2.8	6.1	5.6											
23-478	12.	1.22	C	6.8	3.1	3.1	5.5	2.9	2.5	1.2	1.3	1.3	4.7	3.5	3.8	3.8	4.4											
24-479	12	121	D	—	3.7	5.8	8.0	2.8	2.6	1.2	1.6	1.6	5.3	3.8	3.2	5.1	4.7											
25-480	12	1.20	H	6.2	9.2	5.1	3.7	2.9	6.8	1.8	1.6	1.9	6.9	5.2	3.5	5.4	5.9											
26-481	12.	121	D	—	3.1	4.4	6.2	2.9	3.2	1.5	1.3	1.6	4.7	3.5	2.8	4.2	4.4											
27-482	12.1	120	H	6.5	7.1	4.1	3.4	2.5	5.4	1.8	1.3	1.6	5.9	3.8	2.8	4.8	4.7											
28-483	12	125	D	4.9	3.1	4.4	6.8	3.8	3.6	1.2	1.3	1.6	4.4	3.5	3.2	4.5	NR											
29-484	12.5	1.27	F	4.9	4.6	6.8	3.7	4.2	5.4	1.2	1.6	1.9	4.7	2.4	3.2	5.1	4.4											
30-485	12.	1.28	A	5.1	4.6	3.7	3.7	5.5	5.4	1.5	1.3	1.6	8.1	5.2	3.2	6.1	5.6											
31-486	12.	129	F	4.7	6.8	8.5	4.3	5.5	4.2	1.5	2.2	1.9	6.9	5.1	4.4	6.4	5.9											
32-487	12.	1.28	F	5.6	5.5	6.8	3.4	4.2	4.3	1.5	1.6	1.9	5.0	3.1	3.2	5.4	4.7											
33-488	12	1.2	B	3.1	3.7	2.0	2.2	1.7	3.2	1.5	0.9	1.6	3.1	2.4	2.5	3.2	2.9											
34-489	12.	122	E	3.8	3.1	2.1	5.9	3.4	3.6	0.9	1.6	1.6	5.0	3.1	1.6	3.2	4.7											
35-490	12.	1.20	B	4.7	8.0	3.7	3.4	5.0	5.0	1.8	1.6	2.8	6.6	4.9	4.7	6.4	6.5											
36-491	12.	1.22	F	—	4.2	8.5	5.9	8.4	5.4	1.2	2.2	1.9	2.2	3.5	3.2	6.4	5.9											
37-492	12.	1.20	A	3.3	4.6	4.1	4.3	4.2	4.7	1.5	1.6	1.6	5.9	3.5	2.8	5.1	4.7											
38-493	12.5	1.25	F	3.6	4.3	6.5	4.0	3.8	2.9	1.2	1.9	1.9	4.4	2.1	1.9	4.5	4.1											
39-494	12.5	1.20	A	3.8	4.3	3.7	4.0	4.2	2.5	1.8	1.3	1.6	4.7	2.8	2.8	4.8	3.3											
End		Changed to E of attic, 1-28-65																										

STRUCTURAL RESPONSE PROGRAM

COMPILED BY ______

SCRATCH GAUGE

DATE 1-23-65
HOUSE Storefront

PHASE				PRESSURE (Boeing)							PANE E (in)			PANE B (in)			
Run	A.F.	Hmax	Veh	AV.	1 Inside	2 Tripod	3 Gnd	4 Gnd	5 Gnd	6	IN	OUT	TTL	IN	OUT	TTL	
1-255	11.9	1.25	C	4.67	1.50	1.80	5.25	4.25	4.50	6.25			.70				
2-256	11.9	1.25	G	5.44	2.00	1.80	5.75	6.00	4.25	3.50			.44				
3-257	11.9	1.29	C	2.92	.88	1.10	3.00	5.00	2.75	3.75			.56				
4-258	11.3	1.30	D	3.00	1.50	1.50	2.75	3.25	3.00	3.00			.38				
5-259	12.	1.29	H	5.00	2.00	1.80	5.25	4.75	5.00	3.25			.30				
6-260	12.	1.30	D	5.42	1.88	1.80	5.25	6.00	5.00	5.25			.48				
7-261	12.	1.28	E	7.25	2.13	1.90	7.50	8.00	6.25	5.25			.42				
8-262	12.	1.27	C	4.90	1.50	1.50	4.75	4.25	4.75	6.00			.46				
9-263	12.	1.28	E	4.92	1.75	1.60	5.00	5.25	4.50	2.20			.40				
10-264	12.	1.30	B	3.25	1.13	1.70	3.00	3.25	2.50	3.25			.48				
25-279	12.	1.26	H	4.25	2.00	2.00	4.00	4.50	4.25	4.75			.32				
30-284	25	1.36	A	6.67	.63	1.90	6.50	6.25	7.25	5.50			1.40				B-58
31-285	12.	1.29	B	6.50	.88	1.90	6.00	7.00	6.50	6.25			.64				
32-286	25	1.36	F	2.42	1.50	1.60	2.50	2.25	2.50	1.75			.88				B-58
33-287	12.5	1.29	E	2.83	1.38	1.40	2.75	3.75	2.00	2.00			.42				
34-288	25	1.32	A	3.04	.88	1.30	2.75	3.00	3.25	2.25			1.38				B-58
35-289	12.	1.29	B	5.75	2.00	2.00	5.75	5.25	6.25	6.25			.70				
36-290	25	1.37	F	2.00	1.50	1.40	1.75	2.25	2.00	1.50			.88				B-58
37-291	25	1.37	A	3.0	1.13	1.60	3.00	3.25	3.25	3.25			1.28				B-58
38-292	25	1.34	F										1.22				B-58

STRUCTURAL RESPONSE PROGRAM

COMPILED BY ______

SCRATCH GAUGE

DATE 1-24-65
HOUSE Storefront

PHASE				PRESSURE (Boeing)							PANE E (in)			PANE B (in)		
Run	A.F.	Hmax	Veh	AV.	1 Inside	2 Tripod	3 Gnd	4 Gnd	5 Gnd	6	IN	OUT	TTL	IN	OUT	TTL
13-317	12.	1.29	A	4.00	1.25	1.40	4.00	4.00	[illegible]	5.25			.76			
14-318	12.	1.29	F	4.50	1.25	1.70	4.00	5.25	4.25	6.25			.48			
15-319	12.	1.26	A	5.00	1.13	1.10	5.25	5.00	4.75	5.00			.49			
16-320	12.	1.21	B	4.50	1.50	1.60	4.50	4.25	4.25	5.75			.44			
12-321	12.1	1.20	E	4.52	2.00	1.60	5.00	4.75	4.00	5.00			.44			
21-325	12.	1.23	G	4.17	1.26	1.70	4.25	4.25	4.00	2.50			.38			
22-326	12.	1.29	C	6.00	1.63	1.40	6.25	6.25	5.50	5.75			.62			
23-327	12	1.29	G	3.75	1.63	1.30	3.50	4.00	3.75	2.75			.40			
36-340	12	1.21	G	3.92	1.63	1.60	3.75	5.00	4.00	2.00			.62			
37-341	12.	1.24	C	4.92	2.00	1.30	4.75	4.50	4.50	6.50			.74			
38-342	12.	1.22	G	5.42	2.25	2.20	5.50	5.50	5.25	5.25			.46			
39-343	12.	1.22	C	5.75	1.13	1.20	5.00	6.50	5.75	6.00			.70			

STRUCTURAL RESPONSE PROBE II

COMPILED BY _____

SCRATCH GAUGE

DATE 1-25-65

HOUSE SIDEMOUNT

RUN	ALT	MACH	VEC	PHASE	PRESSURE (BOOM) AM	1	2	3 (TOP)	4	5	6	DAMAGE E (in) IN	OUT	TTL	DAMAGE B (in) IN	OUT	TTL
19-367	12.	1.24	E		5.28	4.13	3.90	3.50	3.50	3.50	4.50			.34			
20-368	12	1.33	A		5.83	—	2.10	4.75	5.75	6.00	4.50			.52			
21-369	12.	1.32	F		2.83	.75	1.70	2.75	2.75	3.00	4.50			.28			
26-369	12.	1.35	H		4.58	4.63	3.00	5.25	4.75	3.50	4.25			.46			
27-370	12.2	1.30	G		5.33	2.00	1.50	5.00	4.50	4.50	6.00			.50			
28-371	11.7	1.26	H		5.83	2.88	4.20	5.75	4.50	5.25	2.75			.36			

STRUCTURAL RESPONSE PROBE II

COMPILED BY _____

SCRATCH GAUGE

DATE 1-26-65

HOUSE SIDEMOUNT

RUN	ALT	MACH	VEC	PHASE	PRESSURE (BOOM) AM	1	2	3 (TOP)	4	5	6	DAMAGE E (in) IN	OUT	TTL	DAMAGE B (in) IN	OUT	TTL
1-376	12.	1.32	B		5.58	5.00	3.60	5.25	6.00	5.50	5.25	.30	.28	.58			
2-375	12.5	1.36	E		4.17	4.25	3.90	4.25	4.25	4.00	2.75	.18	.18	.36			
3-376	12.	1.33	B		4.83	3.38	3.00	4.75	5.00	4.75	4.00	.24	.24	.48			
4-377	12.	1.31	C		4.92	4.63	4.40	4.75	5.25	4.25	5.50	.2	.2	.72			
5-378	12	1.32	G		4.58	4.88	2.80	4.25	5.00	4.50	2.75	.20	.16	.36			
6-379	12	1.32	C		5.75	4.50	4.30	5.00	4.75	5.00	5.00	.38	.32	.70			
7-380	12.5	1.30	D		5.00	4.25	4.30	—	4.25	4.75	4.50	.24	.22	.46			
8-381	11.95	1.30	H		4.92	4.25	3.10	4.25	4.25	4.25	5.50	.16	.14	.30			
9-382	11.95	1.31	D		5.17	4.38	4.10	4.50	5.00	5.00	6.00	.26	.26	.52			
10-383	12	1.30	H		4.92	2.75	2.60	4.25	4.25	4.25	2.75	.14	.14	.28			
11-384	12	1.30	C		3.67	4.38	4.10	3.25	4.00	3.75	3.00	.18	.20	.38			
13-385	12	1.30	B		5.58	4.13	3.80	5.00	4.75	5.75	4.50	.30	.26	.56			
13-386	12	1.30	C		4.25	4.38	4.25	3.25	5.00	4.00	3.00	.30	.26	.56			
14-387	12	1.25	B		3.92	2.63	2.90	3.50	2.75	3.25	4.25	.28	.28	.56			
15-388	25.	1.26	F		3.33	4.88	3.40	3.00	3.75	3.25	2.00	.46	.46	.92			
16-389	25.	1.27	A		4.42	4.50	2.90	3.25	5.50	4.00	3.50	.26	.28	.58			
17-390	12	1.31	G		3.75	3.25	4.10	2.75	2.75	3.25	2.00	.20	.16	.36			
18-391	25.	1.27	F		3.08	4.88	1.90	3.25	4.50	3.00	2.50	.32	.32	.64			
19-392	12.1	1.26	C		3.75	3.25	4.10	3.50	4.00	3.25	2.25	.36	.38	.74			

STRUCTURAL RESPONSE PROGRAM

COUPLED
By _____

SCRATCH GAUGE

DATE 1-26-65
HOUSE SUPPLEMENT

PHASE					PRESSURE (Bars)						PANE E (in)			PANE B (in)			
					1	2 (P3)	3	4	5	6							
RUN	SEC	HOUR	SEC		AM						IN	OUT	TTL	IN	OUT	TTL	
20-393	2	1		A	3.50	1.67	2.30	3.50	3.25	3.50	4.50	.44	.86	1.70			B 5B
21-394	12	1.30		G	6.25	3.13	2.70	6.25	7.00	7.00	2.25	.20	.14	.34			
22-395	25	1.34		F	8.25	4.50	4.70	8.00	7.25	7.50	1.25	.42	.40	.82			B 5B
23-396	12	1.36		C	5.75	2.88	2.70	4.25	5.75	5.25	6.00	.42	.34	.76			
24-397	25	1.38		A	3.50	1.38	1.40	3.25	2.50	2.75	2.25	.28	.28	.56			B 5B
25-398	25	1.38		F	8.25	4.00	4.00	8.25	8.50	8.25	2.00	.44	.44	.88			B 5B
26-399	25	1.38		A	4.25	1.62	1.70	4.25	4.25	5.00	4.50	.62	.64	1.26			B 5B
27-400	12	1.39		H	4.25	2.00	2.60	4.00	4.75	4.00	3.00	.12	.18	.30			
28-401	19	1.25		D	6.25	3.00	2.60	5.75	6.50	6.75	5.50	.28	.26	.54			
29-402	195	1.31		H	3.75	2.38	2.30	3.50	3.75	4.00	2.25	.14	.14	.28			
30-403	12	1.32		D	5.33	1.50	1.70	5.50	6.00	6.00	3.75	.24	.22	.46			
31-404	25	1.37		F	NR			(N G)				.44	.42	.86			B 5B
32-405	25	1.38		A	3.50	1.38	1.80	3.25	3.25	3.50	3.00	.60	.58	1.18			B 5B
33-406	25	1.38		F	8.75	2.13	2.10	8.25	8.25	8.75	2.75	.44	.46	.90			B 5B
34-407	12	1.33		G	4.00	2.25	2.20	3.25	4.25	4.25	2.25	.20	.18	.38			
35-408	25	1.38		A	3.17	1.38	1.80	3.00	3.25	3.25	3.25	.28	.30	.58			B 5B
36-409	12	1.33		C	2.25	1.00	.90	2.00	2.25	2.50	2.25	.34	.28	.62			
37-410	25	1.37		F	4.00	2.25	2.10	3.75	4.25	3.75	2.75	.44	.44	.88			B 5B
38-411	19	1.35		G	4.50	2.25	2.30	4.25	5.00	4.25	2.75	.20	.16	.36			

STRUCTURAL RESPONSE PROGRAM

COUPLED
By _____

SCRATCH GAUGE

DATE 1-26-65
HOUSE SUPPLEMENT

PHASE					PRESSURE (Bars)						PANE E (in)			PANE B (in)			
					1	2 (P3)	3	4	5	6							
RUN	SEC	HOUR	SEC		AM						IN	OUT	TTL	IN	OUT	TTL	
39-412	25	1.30		A	2.50	1.50	1.80	3.00	3.25	3.25	3.50	.66	.26	.92			B 5B
40-413	25	1.37		F	2.25	1.50	1.50	2.25	2.25	2.25	1.75	.42	.38	.80			B 5B
41-414	25	1.38		A	2.88	1.25	1.60	2.75	3.00	2.75	3.00	.30	.26	.56			B 5B
42-415	25	1.38		F	8.25	2.13	2.10	3.50	4.00	3.50	2.75	.44	.46	.90			B 5B
43-416	25	1.41		A	3.50	1.25	1.70	2.25	4.25	3.25	2.75	.24	.24	.48			B 5B
44-417	12	1.28		H	4.00	2.13	2.60	3.75	4.25	4.25	2.75	.20	.16	.36			
45-418	12	1.25		H	5.33	2.38	2.50	5.00	3.75	3.25	2.25	.18	.16	.34			
46-419	12	1.20		D	4.00	1.50	1.10	3.50	4.25	4.50	4.25	.60	.68	1.28			
47-420	12	1.31		G	3.00	2.13	1.80	2.75	3.50	3.00	1.75	.38	.30	.68			
48-421	12	1.31		C	2.50	.69	1.10	2.25	2.50	4.00	2.00			.30			
49-422	12	1.33		G	4.50	2.00	1.90	4.50	4.25	4.75	1.75			.30			
50-423	121	1.26		H	10.17	4.88	4.94	9.25	11.00	11.13	4.25	.20	.20	.40			
51-424	122	1.3		D	4.92	1.38	1.00	4.00	5.25	5.25	1.15	.22	.24	.46			
52-425	122	13		H	5.50		2.70	4.50	6.75	6.75	4.00	.28	.18	.46			

STRUCTURAL RESPONSE PROGRAM

COMPILED BY _____ SCRATCH GAUGE DATE 1-31-65 HOUSE SHELTER #2

PHASE					PRESSURE (BOOMS)						DANG E (in)			DANG B (in)		
					1	2	3 (OBS)	4	5	6	IN	OUT	TTL	IN	OUT	TTL
PIN	HT	WDTH	LOC	AV												
1-563	12	126	F	4.2	6.0	7.1	7.9	4.8	6.9	5.2			.84			
2-564	12	125	A	4.6	2.9	2.0	2.6	4.0	2.6	1.9			.84			
3-565	12.5	126	F	3.9	6.2	6.0	6.4	3.7	5.4	5.1			.84			
4-566	12	120	G	4.1	5.2	4.6	8.0	6.1	5.6	5.0			.32			
5-567	12	122	C	5.0	2.4	2.4	2.5	5.0	2.3	2.4			.24			
6-568	12	123	G	5.0	4.9	5.0	5.5	5.0	4.2	4.2			.28			
7-569	12	123	H	4.8	4.1	4.6	4.9	4.8	4.3	4.0			.24			
8-570	12	123	F	4.4	6.5	4.5	9.1	4.4	5.7	6.8			.36			
9-571	12	123	D	5.3	2.7	2.7	4.2	5.3	2.1	2.6			.42			
10-572	12	125	A	3.3	2.5	1.8	4.3	2.3	2.4	2.0			.26			
11-573	12	122	I-1	5.5	4.6	5.6	5.8	5.5	5.-	5.6			.24			
12-574	12	124	F	4.3	7.6	7.1	7.6	4.2	6.0	5.5			.32			
13-575	12	125	A	5.6	4.2	4.2	2.8	5.6	2.8	2.1			.28			
14-576	12	124	F	3.9	5.3	5.1	5.7	3.9	4.6	4.3			.20			
15-577	12	124	A	5.5	2.9	2.1	3.2	5.5	2.7	2.3			.44			
16-578	12	124	D	3.6	2.5	2.4	2.0	3.6	2.1	1.6			.54			
17-579	12	124	G	6.2	4.2	9.5	7.4	6.2	6.5	5.2			.33			
18-580	12	124	C	5.0	3.3	2.5	2.4	5.0	3.0	2.0			.36			
19-581	12	122	C	4.4	2.2	2.0	2.7	4.4	1.8	2.4			.20			

STRUCTURAL RESPONSE PROGRAM

COMPILED BY _____ SCRATCH GAUGE DATE 1-31-65 HOUSE SHELTER #2

PHASE					PRESSURE (BOOMS)						DANG E (in)			DANG B (in)		
					1	2	3 (OBS)	4	5	6	IN	OUT	TTL	IN	OUT	TTL
PIN	HT	WDTH	LOC	AV												
20-582	12	123	G	3.8	4.4	5.2	5.5	2.6	4.0	3.9			.20			
21-583	12	122	C	4.9	2.4	2.5	3.1	4.9	2.3	2.5			.24			
22-584	12	124	D	3.0	2.4	2.5	2.7	3.0	2.6	2.1			.24			
23-585	12	124	H	7.0	4.4	4.2	4.0	7.0	4.4	4.0			.36			
24-586	12	124	D	4.4	2.9	3.0	3.2	4.4	2.3	2.3			.44			
25-587	12	122	C	5.8	6.6	5.1	7.8	5.8	4.8	4.7			.44			
26-588	12	124	B	4.0	3.8	2.7	3.0	4.0	4.1	2.2			.68			
27-589	12	124	C	7.5	8.9	9.1	10.2	7.5	8.4	7.4			.46			

STRUCTURAL RESPONSE PROGRAM

COMPILED BY _____

SCRATCH GAUGE

DATE 2-3-65

HOUSE SUPPLEMENT

PHASE				PRESSURE (BOOMS)						PANEL E (in)			PANEL B (in)		
				1	2	3	4	5	6	IN	OUT	TTL	IN	OUT	TTL
RUN				AV											
6-656	R	125	F	43	46	48	45	42	48	42		.40			.16
7-657	1195	125	C	41	37	44	39	41	41	42		.58			.58
8-658	12	125	E	52	43	44	41	52	40	38		.42			.18
9-659	12	122	F	42	—	—	—	42	—	—		.42			.30
10-660	12	125	B	49	—	—	—	49	—	—		.56			.54
11-661	12	120	A	45	27	41	35	45	36	37		.96			.92
12-662	11	115	F	43	38	25	35	43	36	25		.104			.78
13-663	12	121	A	NR	(	W	R	)				.82			.80
14-664	12	121	F	48	48	37	41	48	40	37		.52			.40
15-665	12	125	G	41	41	28	36	41	40	38		.38			.34
16-666	12	120	H	35	21	32	24	35	37	32		.34			.50
17-667	1195	126	C	40	46	38	43	40	37	46		.66			.52
18-668	12	121	D	36	33	30	29	36	30	36		.24			.40
19-669	12	125	G	55	25	33	34	55	42	28		.38			.34
20-670	12	123	H	53	25	31	36	53	54	44		.28			.42
21-671	1195	122	G	45	24	21	33	45	33	32		.24			.42
22-672	1205	120	D	36	45	45	45	36	29	35		.56			.22
23-673	119	120	B	27	20	29	22	27	27	24		.48			.50
24-674	1205	123	A	40	29	29	24	40	19	22		.26			.20

STRUCTURAL RESPONSE PROGRAM

COMPILED BY _____

SCRATCH GAUGE

DATE 2-3-65

HOUSE SUPPLEMENT

PHASE				PRESSURE (BOOMS)						PANEL E (in)			PANEL B (in)		
				1	2	3	4	5	6	IN	OUT	TTL	IN	OUT	TTL
RUN				AV											
25-675	12	121	E	53	47	42	46	53	41	42		.50			.28
26-676	12	123	F	39	—	33	46	39	35	25		.48			.34
27-677	12	124	B	66	33	40	36	66	41	41		.26			.76
28-678	12	125	A	54	41	41	64	54	23	58		.24			.82
29-679	12	125	E	32	21	19	20	32	26	22		.40			.18
30-680	12	124	F	56	64	50	69	56	47	37		.58			.46

STRUCTURAL RESPONSE PROGRAM

COUPLED BY ——— SCRATCH GAUGE DATE 2-4-65 HOUSE SIDEWALL

PHASE				PRESSURE PSF (BOEING)							DANCE IN.				DANCE IN.			
					1	2	3	4	5	6	III	OUT	III		IN	OUT	III	
RUN	PSF	M.P.H.	DIR	AV														
1-681	97	120	C	6.6	2.55	–	6.9	6.9	6.2	6.5			.96				76	
2-682	97	118	SW	6.5	2.0	–	6.6	6.8	5.8	6.6			.70				36	
3-683	97	121	G	6.4	2.85	–	6.1	6.7	5.8	6.2			.54				34	
4-684	97	120	W	6.1	2.25	–	6.1	6.3	5.7	6.3			.36				42	
5-685	97	121	C	5.9	2.62	–	6.0	6.4	5.6	5.9			.90				74	
6-686	97	120	SW	6.4	2.15	–	6.5	6.9	6.0	6.2			.64				32	
7-687	97	120	W	6.1	2.10	–	5.8	6.6	5.9	6.1			.56				38	
8-688	99	119	W	NR	2.15	–	–	–	–	–			.54				28	
9-689	97	120	A	6.3	2.10	–	6.0	6.6	6.2	6.0			1.00				90	
10-690	97	120	C	6.0	2.20	–	6.1	6.3	5.7	6.2			.78				74	
11-691	97	120	W	6.0	2.00	–	5.9	6.3	5.8	5.8			.52				38	
12-692	97	121	W	NR	1.90	–	–	–					.54				26	
13-693	97	119	G	7.1	1.95	–	7.8	7.2	7.0	6.3			.38				40	
14-694	97	120	W	5.7	2.15	–	5.6	5.8	6.1	5.5			.40				56	
15-695	97	121	C	6.1	2.40	–	6.2	6.7	5.8	5.7			.90				72	
16-696	97	119	SW	5.8	2.70	–	5.4	5.8	6.6	5.6			.72				36	
17-697	97	120	G	5.1	1.65	–	5.2	5.2	5.0	4.9			.36				34	
18-698	97	121	W	5.0	2.05	–	5.1	5.5	4.7	4.7			.34				50	
19-699	97	118	G	6.6	2.40	–	6.9	5.8	7.3	6.5			.82				82	

STRUCTURAL RESPONSE PROGRAM

COUPLED BY ——— SCRATCH GAUGE DATE 2-4-65 HOUSE SIDEWALL

PHASE				PRESSURE PSF (BOEING)							DANCE IN.				DANCE IN.			
					1	2	3	4	5	6	IN	OUT	III		IN	OUT	III	
RUN	PSF	M.P.H.	DIR	AV														
20-700	97	119	A	8.2	2.20	–	8.5	7.8	8.3	8.2			1.04				1.02	
21-701	97	120	SW	6.6	1.90	–	6.6	6.6	6.1	6.1			.50				25	
22-702	97	120	W	6.5	1.95	–	7.1	6.3	5.9	6.8			.50				38	
23-703	97	120	W	5.1	2.70	–	5.0	5.2	5.1	4.5			.94				84	
24-704	97.5	119	A	6.4	2.21	–	7.1	6.3	5.9	6.2			.98				96	
25-705	97	120	C	5.9	2.50	–	5.6	5.7	6.2	5.8			–				–	
26-706	97	120	SW	5.7	2.30	–	6.1	5.9	5.5	5.2			.70				36	
27-707	95	120	G	2.5	1.15	–	2.8	2.7	3.4	2.2			.36				36	
28-708	97	120	W	5.6	2.10	–	5.3	5.2	6.2	5.6			.36				50	
29-709	97	120	G	5.3	1.95	–	5.2	5.4	6.0	4.5			.42				32	
30-710	97	119	W	6.3	2.20	–	6.6	6.5	6.1	5.6			.38				58	

STRUCTURAL RESPONSE PROGRAM

COMPILED
BY ______

SCRATCH GAUGE

DATE 2-5-65
HOUSE STOREFRONT

PHASE				PRESSURE PSF (BOEING)							PANE E IN.			PANE B IN.		
					1	2	3	4	5	6	IN	OUT	TTL	IN	OUT	TTL
RUN	ALT	MACH	VEC	AV	[illegible]		[illegible]	[illegible]	[illegible]	[illegible]						
3-713	8.0	1.2	C	9.3	[illegible]	–	9.6	9.5	9.3	8.9			1.00			.90
4-714	8.0	1.21	A	8.6	2.50	–	9.3	8.8	8.4	8.1			1.16			1.00
5-715	8.0	1.21	E	8.6	2.10	–	8.9	8.5	8.6	9.5			.56			.56
6-716	8.0	1.19	F	9.1	2.45	–	9.9	9.0	8.7	9.0			.66			.44
7-717	8.0	1.20	G	8.7	2.70	–	8.9	8.9	8.9	9.0			.46			.40
8-718	8.0	1.20	H	8.6	2.90	–	8.6	8.5	8.7	8.3			.42			.62
9-719	8.0	1.2	C	9.6	3.00	–	10	8.7	9.7	10.9			1.10			.90
10-720	8.0	1.20	D	9.0	2.65	–	9.2	8.6	9.4	8.8			.70			.38
11-721	8.0	1.2	G	8.0	2.75	–	7.8	8.2	7.5	7.3			.52			.42
12-722	8.0	1.21	H	9.3	2.00	–	10.1	8.8	8.4	8.8			.46			.66
13-723	7.95	1.19	A	8.3	2.40	–	8.6	8.5	8.6	7.3			1.20			.92
14-724	7.9	1.21	B	10.2	1.95	–	9.5	9.1	11.0	10.3			1.04			.92
15-725	8.0	1.2	F	9.2	–	–	9.4	8.4	9.0	10.6			.60			.40
16-726	8.0	1.21	E	8.5	1.65	–	8.2	8.6	9.1	7.9			.56			.34
17-727	7.9	1.20	A	7.4	2.60	–	6.9	7.0	8.1	7.7			1.22			1.08
18-728	8.0	1.21	C	8.4	3.15	–	7.9	8.2	9.3	8.3			.96			.82
19-729	8.0	1.2	C	7.9	2.40	–	7.2	8.5	8.4	7.6			1.00			.98
20-730	8.0	1.2	D	7.5	2.30	–	7.1	7.7	7.7	7.6			.26			.36
21-731	8.1	1.2	G	7.2	1.55	–	7.0	7.4	7.7	6.8			.50			.40

STRUCTURAL RESPONSE PROGRAM

COMPILED
BY ______

SCRATCH GAUGE

DATE 2-5-65
HOUSE STOREFRONT

PHASE				PRESSURE PSF (BOEING)							PANE E IN			PANE B IN.		
					1	2	3	4	5	6	IN	OUT	TTL	IN	OUT	TTL
RUN	ALT	MACH	VEC	AV	[illegible]		[illegible]	[illegible]	[illegible]	[illegible]						
22-732	8.0	1.2	H	7.6	2.6	–	7.2	8.1	7.8	7.1			.46			.64
23-733	8.0	1.2	C	9.0	2.05	–	8.4	9.5	9.1	9.0			1.18			.96
24-734	8.0	1.2	D	9.2	2.55	–	8.8	9.1	10.2	8.8			.80			.32
25-735	8.0	1.19	F	7.0	2.7	–	7.2	6.4	7.1	6.9			.66			.46
26-736	8.0	1.19	E	10.4	2.4	–	8.5	11.2	12.6	9.1			.62			.42
27-737	8.0	1.2	H	9.2	2.45	–	8.9	9.2	10.1	8.5			1.12			1.00
28-738	7.95	1.2	C	7.1	2.9	–	7.4	7.1	6.6	7.5			.98			.82
29-739	8.0	1.19	E	8.2	2.45	–	8.6	8.1	7.9	8.2			.42			.38
30-740	8.0	1.20	F	7.8	2.15	–	7.7	8.0	7.9	7.8			.58			.42

STRUCTURAL RESPONSE PROGRAM

COMPILED BY _____

SCRATCH GAUGE

DATE 2-6-65
HOUSE STREET COURT

PHASE				PRESSURE PSF (BOEING)							PANE E IN			PANE B IN		
					1	2	3	4	5	6	IN	OUT	TTL	IN	OUT	TTL
RUN	AT	HOW	VEL	AM												
1-241	72	120	G	10.7	3.54	-	106	102	101	104			.44			.58
2-242	72	120	H	99	3.35	-	109	106	102	100			.48			.78
3-243	73	122	C	108	3.7	-	105	105	104	108			1.21			1.08
4-244	73	121	V	10.9	3.35	-	110	113	106	102			.98			1.62
5-245	73	120	G	10.2	3.05	-	102	110	94	102			.52			.54
6-246	73	120	H	10.1	3.40	-	106	106	88	104			.54			.76
7-247	73	121	C	10.2	3.35	-	94	107	107	107			1.22			1.00
8-248	73	12	V	10.6	3.30	-	103	110	102	111			.96			.60
9-249	73	119	G	10.6	3.45	-	99	107	110	110			1.07			1.08
10-250	72	119	E	9.3	3.05	-	91	96	102	100			.66			.60
11-251	73	119	E	11.4	3.75	-	108	108	113	123			.64			.46
12-252	73	12	A	10.6	-	-	-	112	99	106			1.38			1.20
13-253	73	12	G	10.1	3.65	-	103	106	95	103			1.08			1.00
14-254	73	119	E	10.3	3.6	-	101	105	111	115			.72			.46
15-255	73	119	E	10.1	-	-	101	106	107	105			.62			.42
16-256	73	12	A	11.6	4.25	-	112	97	120	108			1.44			1.24
17-257	73	12	C	12.3	4.50	-	128	130	116	114			1.96			1.00
18-258	73	119	V	11.7	4.40	-	120	108	123	106			.94			.60
19-259	73	120	G	9.2	2.9	-	91	94	91	91			.44			.58

STRUCTURAL RESPONSE PROGRAM

COMPILED BY _____

SCRATCH GAUGE

DATE 2-6-65
HOUSE STREET COURT

PHASE				PRESSURE PSF (BOEING)							PANE E IN.			PANE B IN		
					1	2	3	4	5	6	IN	OUT	TTL	IN	OUT	TTL
RUN	AT	HOW	VEL	AM												
20-260	73	119	E	9.4	3.05	-	89	70	87	72			.58			.76
21-261	73	12	C	11.9	3.71	-	127	108	118	125			1.22			1.00
22-262	73	121	V	11.0	3.4	-	96	105	93	105			.86			.56
23-263	73	12	G	9.4	2.9	-	81	76	86	91			.44			.56
24-264	73	117	E	9.7	3.01	-	95	96	97	99			.78			.86
25-265	73	12	E	10.9	3.7	-	115	105	109	108			.68			.44
26-266	73	12	E	9.5	2.95	-	96	91	102	94			.60			.36
27-267	73	12	A	NR	(					)			1.30			1.18
28-268	73	12	G	10.6	4.41	-	106	98	108	106			1.15			1.06
29-269	73	12	E	10.0	3.5	-	94	98	110	98			.60			.40
30-270		119	E	12.6	4.0	-	119	123	134	121			.48			.34

STRUCTURAL RESPONSE PROGRAM

COMPILED BY ______

DATE 2-7-65
HOUSE STOREFRONT

SCRATCH GAUGE

PHASE				PRESSURE PSI (BOEING)							PANE E (in)			PANE B (in)		
					1	2	3	4	5	6	IN	OUT	TTL	IN	OUT	TTL
RUN	ALT	HGT	VEH	AV												
1-771	68	12	F	12.3	3.15	–	12.8	12.8	11.8	11.6			.74			.40
2-772	[illegible]	[illegible]	F	14.0	3.65	–	14.2	13.6	14.2	14.0			.80			.48
3-773	68	11.2	[illegible]	11.3	3.05	–	11.2	10.6	11.6	11.4			.66			[illegible]
4-774	68	11.9	F	13.2	3.45	–	13.6	12.4	12.6	14.2			.78			.50
5-775	68	12	F	13.2	2.85	–	13.2	12.6	13.2	13.8			.62			.44
6-776	[illegible]	11.8	F	14.9	3.05	–	15.4	16.4	15.2	12.6			.90			.52
7-777	[illegible]	12	[illegible]	11.0	3.20	–	12.4	13.6	12.4	13.4			.70			.48
8-778	[illegible]	[illegible]	[illegible]	12.1	3.05	–	10.4	13.0	12.8	12.6			.68			.48
9-779	[illegible]	11.9	A				N	K	)				1.56			1.26
10-780	67.5	11.1	A	11.7	3.4	–	11.4	12.0	11.6	11.8			1.40			1.22
11-781	68	12	F	12.3	–	–	11.4	12.8	12.6	12.2			.70			.52
12-782	[illegible]	11.9	F	12.5	3.3	–	12.4	12.6	13.0	12.6			.70			.46
13-783	[illegible]	12	A	13.2	3.65	–	12.6	13.6	13.4	13.0			1.46			1.28
14-784	67.5	11.9	A	13.4	3.25	–	12.8	13.6	14.4	12.4			1.54			[illegible]
15-785	67	12	F	11.7	2.95	–	11.8	12.4	12.4	11.4			.72			.44
16-786	[illegible]	[illegible]	F	11.9	3.15	–	11.4	12.2	12.4	11.4			.80			.48
17-787	[illegible]	[illegible]	A	16.4	4.5	–	16.2	15.6	15.4	16.8			1.80			1.44
18-788	67.5	11.8	A	13.6	4.25	–	13.2	13.8	14.0	13.2			1.48			1.26
19-789	68	12	F	10.0	–	–	9.5	9.6	10.0	10.4			.64			.38

STRUCTURAL RESPONSE PROGRAM

COMPILED BY ______

DATE 2-7-65
HOUSE STOREFRONT

SCRATCH GAUGE

PHASE				PRESSURE (BOEING)							PANE E			PANE B		
					1	2	3	4	5	6	IN	OUT	TTL	IN	OUT	TTL
RUN	ALT	HGT	VEH	AV												
20-790	68	1.2	F	13.3	3.75	–	12.8	13.0	14.4	15.0			.82			.46
21-791	66	12	A	12.7	3.4	–	12.0	12.2	13.6	12.8			1.42			1.22
22-792	67.5	1.2	A	13.9	3.95	–	14.2	13.8	14.0	13.4			1.40			1.26

Structural Response Program

Compiled By ______

Date 2-9-65

Scratch Gauge

House Storefront

Phase				Pressure PSF (Boeing)							Pane E in			Pane B in.		
					1	2	3	4	5	6	In	Out	TTL	In	Out	TTL
Run	A.F.	[illegible]	[illegible]	AK	[illegible]		Grnd	Grnd	Grnd	Grnd						
1-79[illegible]	6.3	116	F	14.6	3.6	—	15.2	14.6	13.2	15.4			.92			.52
2-194	5.8	117	A	17.5	4.5	—	16.6	18.6	18.2	16.4			1.89			1.62
[illegible]	6.3	117	F	12.4	4.55	—	18.[illegible]	18.4	18.2	17.0			.86			.46
4-196	[illegible]	123	F	18.0	4.2	—	19.4	18.4	16.6	17.4			.44			.48
[illegible]-19[illegible]	6.6	12[illegible]	A	12.8	[illegible].9	—	12.6	12.4	10.4	[illegible]			1.53			1.34

Structural Response Program

Compiled By ______

Date 2-10-65

Scratch Gauge

House Storefront

Phase				Pressure PSF (Boeing)							Pane E (in)			Pane B (in)		
					1	2	3	4	5	6	In	Out	TTL	In	Out	TTL
Run	A.F.	[illegible]	[illegible]	AK	[illegible]		Grnd	Grnd	Grnd	Grnd						
1-798	5.7	115	F	19.2	4.2	—	23.2	19.0	18.0	18.6			1.06			.60
2-799	5.5	118	C	21.4	6.3	—	23.0	[illegible]	18.4	23.6			1.80			1.40
3-800	5.8	118	F	15.7	4.2	—	20.8	12.8	15.2	18.0			1.00			.60
4-801	5.7	11	F	17.4	5.2	—	19.8	16.6	12.6	12.6			1.22			.92
5-802	5.65	11	A	21.7	5.9	—	22.8	20.8	18.2	25.0			1.66			2.00
6-803	5.7	1.1	F	16.7	4.5	—	16.4	14.6	13.6	16.6			1.34			.80

John A. Blume & Associates, San Francisco, Calif.
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DESCRIPTORS

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Structural Response
Supersonic Aircraft
Noise
Damage
Overpressure
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The test area included 21 structures varying in design, construction and age. Furniture, mirrors, television sets and other home appliances, dishes, crystal, bric-a-brac and various other items were in the test structures.

The test site was exposed to 1494 sonic booms of overpressures ranging from 1.6 to 23.4 pounds per square foot (p.s.f.). Sonic booms and structural material reaction were measured.

To study the cumulative effects of repeated sonic booms, 680 successive flights at a scheduled overpressure of 5.0 p.s.f. were generated during one period of the study.

It is concluded that no previously undamaged material was identified during the accumulative effects portion of the study. Sonic boom overpressure levels at which incipient effects appear in structures and materials are presented.

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